

Determination of Sandia Thermal Model Coefficients and ΔT for PV Modules with New Backsheet Types

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1. Introduction

- Sandia thermal model [1], one of the most extensively used models by the industry, predicts the cell temperature of a PV module using a few empirical coefficients and ΔT (temperature difference between cell and conventional backsheet).
- When the Sandia thermal model was developed before 2004, there were only a few types of polymer backsheet materials available in the marketplace and they were mainly Tedlar based backsheets.
- Due to \$/watt pressure in the current highly competitive market, many module manufacturers have started using non-Tedlar based backsheets.
- We present the empirical coefficients and ΔT for the PV modules containing new types of polymer backsheets and glass substrate.
- These backsheet-specific coefficients and ΔT provide more accurate predicted cell temperatures for the modules.

2. Experimental Setup

➤ Glass/Polymer Modules

- Glass/EVA/Cell/EVA/Backsheet
- 156mm x 156 mm monocrystalline Si cells
- Polymer backsheet types
 - Tedlar-PET-Tedlar (TPT)
 - PVDF-PET-EVA
 - PA-Aluminum-PET-PA

➤ Glass/Glass Modules

- Glass/EVA/Cell/EVA/Glass
- 156mm x 156 mm monocrystalline Si cells
- Glass types
 - 3.2 mm-thick Solite PV glass

➤ Module Dimensions

- 1-cell module: 8" x 11"
- 9-cell module: 20.5" x 22"

➤ Cell and Module temperature

- Cell temperature: T-type thermocouple was attached on the backside of solar cell before lamination. (9-cell module only)
- Module temperature: T-type thermocouple was attached on the backsheet.

➤ Module Installation and Data Acquisition

- Open rack installation
 - South facing
 - 45° fixed tilt
- Data acquisition system
 - Every 30s interval
 - Cell and module temperature
 - Weather data
 - POA irradiance, ambient temperature, wind speed, wind direction

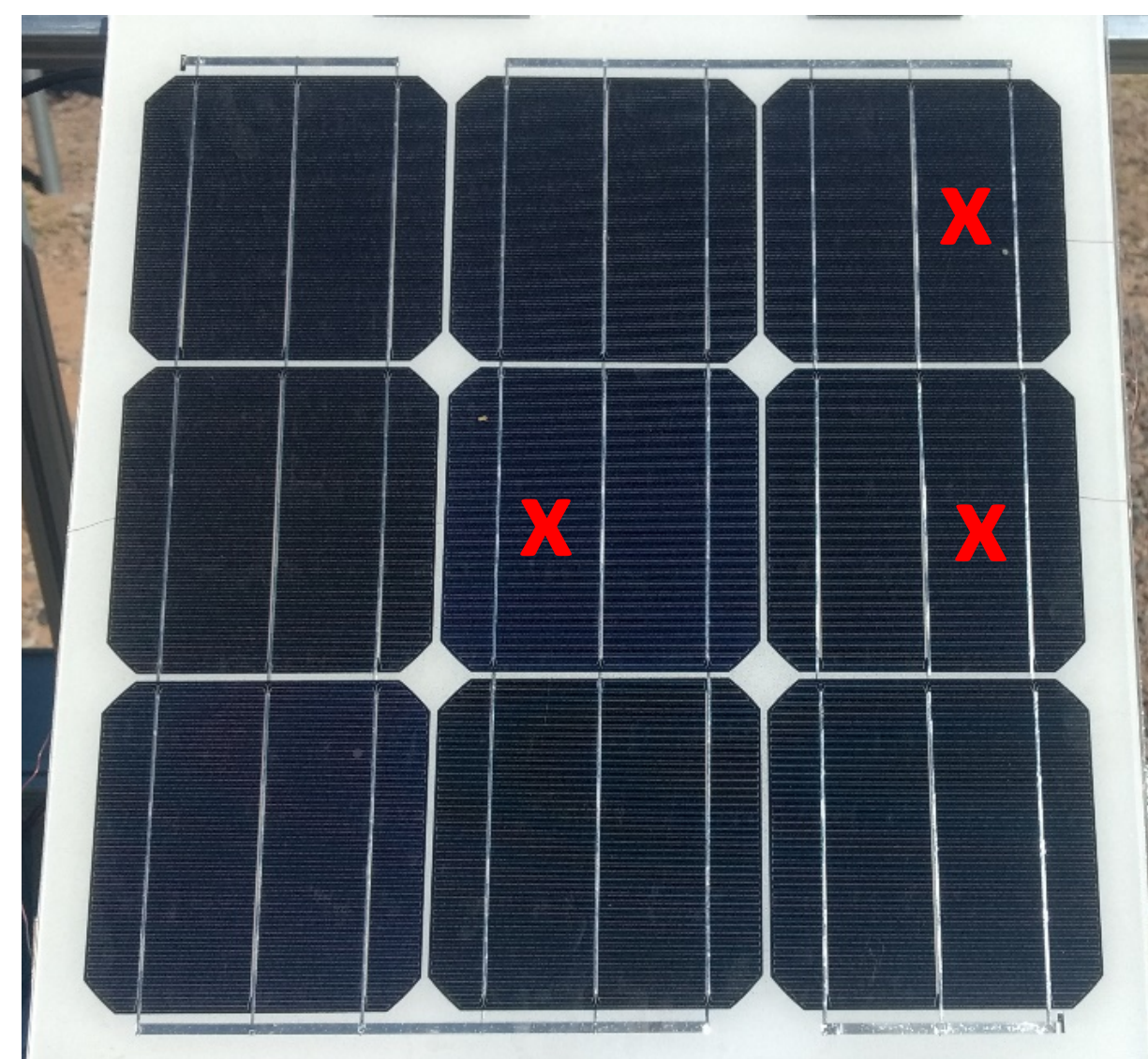


Fig. 1. 9-cell module. 'X' marks represent the placement of thermocouples on backside of the cells.



Fig. 2. A photo of 1-cell and 9-cell modules installed at open rack mount for thermal testing at Mesa, Arizona.

➤ Temperature coefficients

- Outdoor I-V tracer was used to take multiple I-V curves with respect to temperature.
- Test modules were stored in air-conditioned box ($<20^{\circ}\text{C}$) until I-V measurement.

3. Sandia Thermal Model Coefficients

- Overall, the coefficient 'a' of all the 1-cell modules obtained at ASU-PRL is practically similar to Sandia thermal model coefficient.
- No coefficient 'a' difference observed between the glass/polymer module and the glass/glass module while King *et al* [1], reported -3.47 as a coefficient 'a' for glass/glass module.
- For coefficient 'b', all the values obtained from the modules used in this study are higher (smaller) than Sandia reported values, which are -0.0750 and -0.0594 for glass/polymer module and glass/glass module, respectively.

Module Operating Temperature by Sandia Model

$$T_m = E \times (e^{a+b \times WS}) + T_{amb}$$

- T_m : module temperature (backsheet temperature) ($^{\circ}\text{C}$)
- E: plane of array irradiance (W/m^2)
- WS: wind speed (m/s)
- T_{amb} : ambient temperature ($^{\circ}\text{C}$)
- a: empirically-determined coefficient establishing the upper limit for module temperature at low wind speeds and high solar irradiance
- b: empirically-determined coefficient establishing the rate at which module temperature drops as wind speed increases

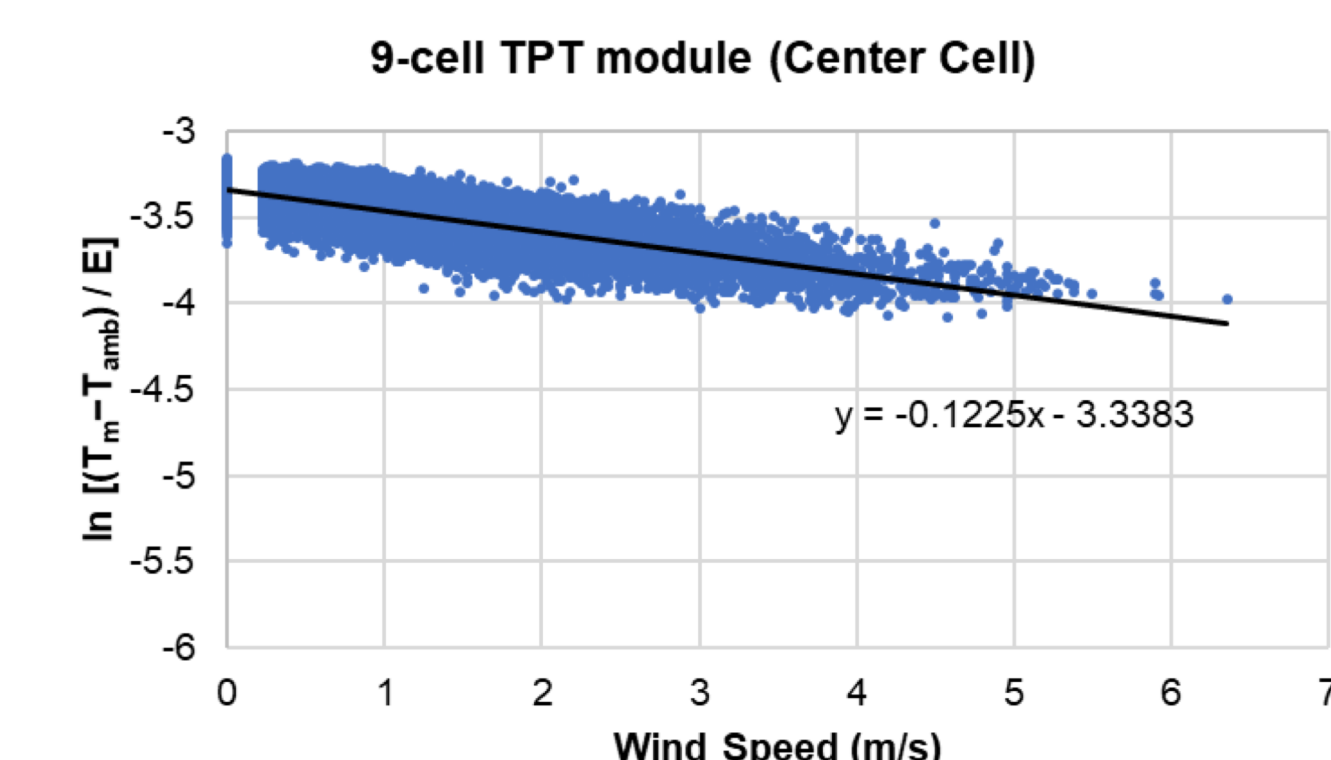


Fig. 3. Plotted empirical data to determine the coefficients (a, b). T_m was measured from center cell of nine-cell module.

Empirically determined coefficients for various type of backsheets and module configuration

Sample	Module Type	a	b
1-cell module	Glass/Polymer (PVDF-PET-EVA)	-3.60	-0.1101
	Glass/Polymer (PA-AI-PET-PA)	-3.58	-0.1080
	Glass/Polymer (TPT)	-3.52	-0.1154
	Glass/Glass	-3.53	-0.1037
9-cell module (center cell)	Glass/Polymer (PVDF-PET-EVA)	-3.38	-0.1033
	Glass/Polymer (PA-AI-PET-PA)	-3.29	-0.1125
	Glass/Polymer (TPT)	-3.34	-0.1225

4. Temperature Difference between Cell and Backsheet (ΔT)

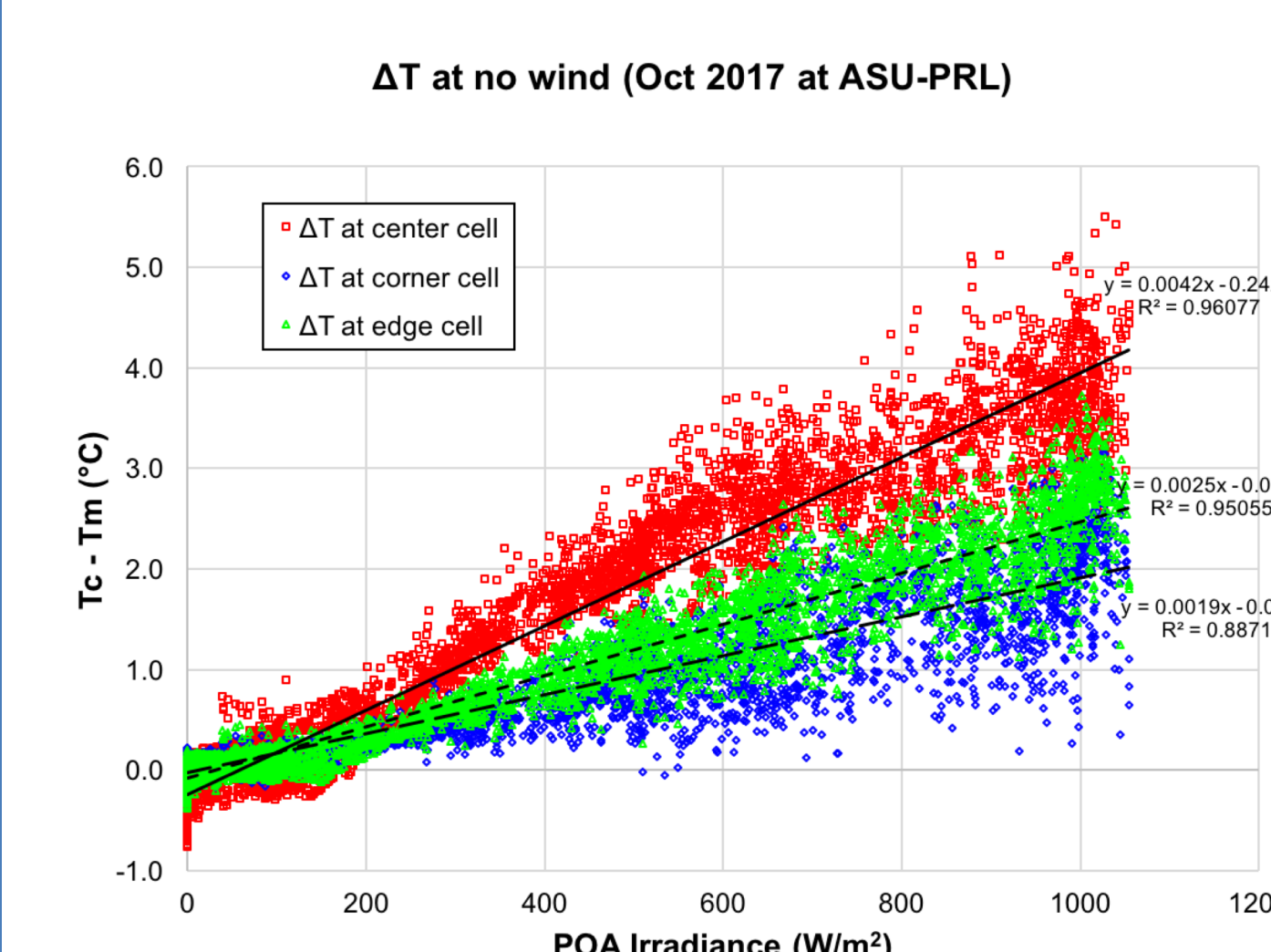


Fig. 4. ΔT with respect to irradiance for Glass/Polymer (TPT) 9-cell modules at 0 m/s wind speed

Sample	Module type	ΔT at 1057 \pm 3 W/m^2	
		ΔT at 0 m/s WS	ΔT at 1 m/s WS
1-cell module	Glass/Polymer (PVDF-PET-EVA)	2.6	3.3
	Glass/Polymer (PA-AI-PET-PA)	2.6	3.5
	Glass/Polymer (TPT)	2.7	3.4
	Glass/Glass	2.9	3.7
9-cell module	Glass/Polymer (PVDF-PET-EVA) Center cell	3.2	3.1
	Glass/Polymer (PVDF-PET-EVA) Corner cell	2.2	2.6
	Glass/Polymer (PVDF-PET-EVA) Edge cell	1.5	2.1
	Glass/Polymer (PA-AI-PET-PA) Center cell	2.5	2.5
	Glass/Polymer (PA-AI-PET-PA) Corner cell	1.9	2.3
	Glass/Polymer (PA-AI-PET-PA) Edge cell	2.1	2.5
	Glass/Polymer (TPT) Center cell	4.0	4.1
Glass/Polymer (TPT) Corner cell	1.9	2.4	
Glass/Polymer (TPT) Edge cell	2.4	2.8	

- ΔT provided by Sandia is $2\text{-}3^{\circ}\text{C}$ for open-rack mount.
- ΔT was center>edge>corner in 9-cell module, and it was as high as $5.5\text{-}5.8^{\circ}\text{C}$ at center cell.
- ΔT could be higher at 1 m/s wind speed than 0 m/s wind speed.
- Due to thermal equilibrium issue, P_{max} could be overestimated when $T_m + 2.5^{\circ}\text{C}$ was used rather than T_c as shown in Fig. 5.

Temperature coefficients of 9-cell module at 1000 W/m^2 irradiance

Temperature	I_{sc} ($\text{A}/^{\circ}\text{C}$)	V_{oc} ($\text{V}/^{\circ}\text{C}$)	I_{mp} ($\text{A}/^{\circ}\text{C}$)	V_{mp} ($\text{V}/^{\circ}\text{C}$)	FF ($\%/^{\circ}\text{C}$)	P_{max} ($\text{W}/^{\circ}\text{C}$)
$T_m + 2.5$	0.0063	-0.0206	-0.0006	-0.0232	-0.1812	-0.1825
T_c	0.0057	-0.0188	-0.0002	-0.0214	-0.1658	-0.1667

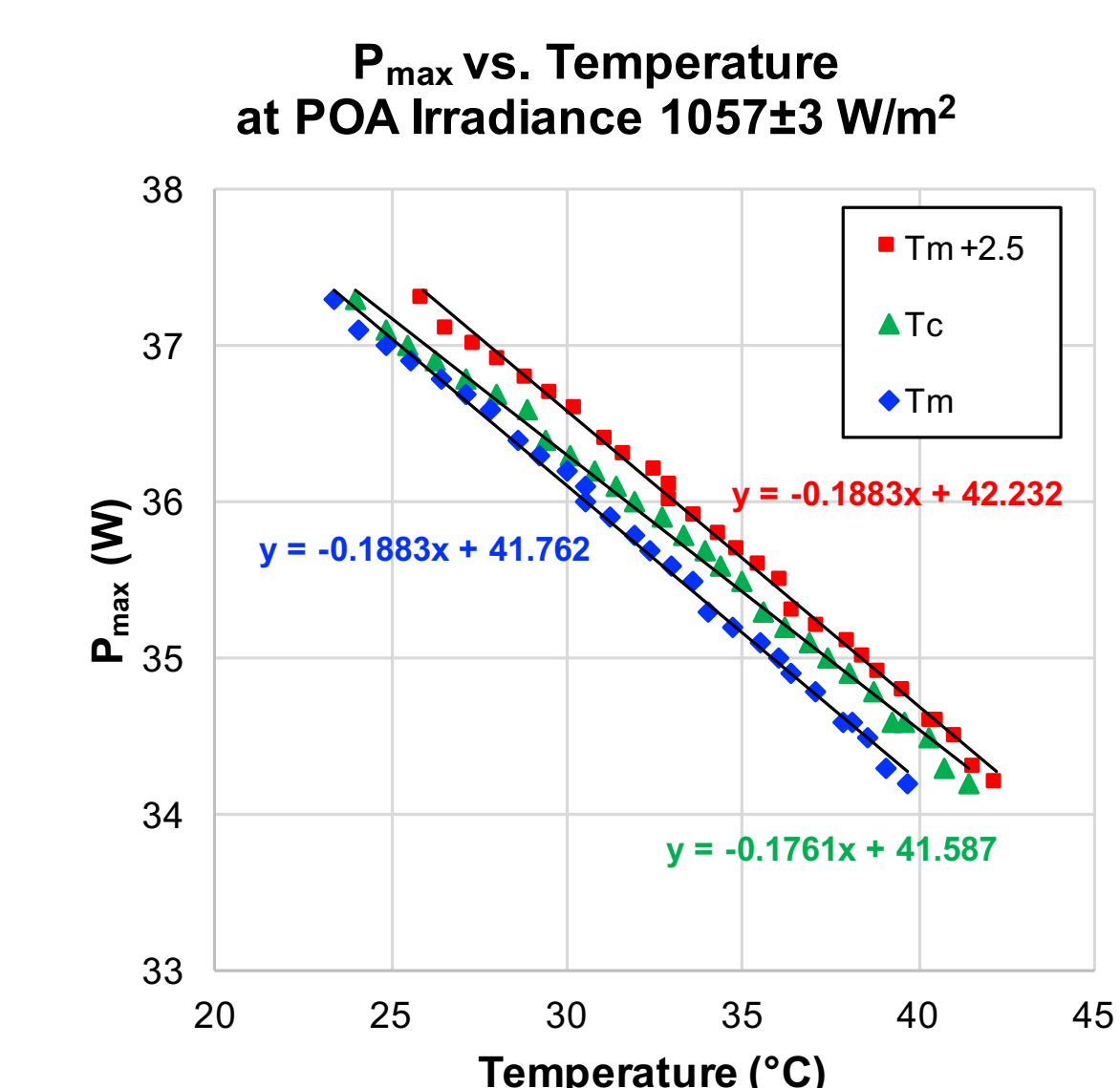


Fig. 5. P_{max} temperature coefficient using cell temperature, module temperature and converted cell temperature ($T_m + 2.5^{\circ}\text{C}$).