



UNIVERSITY OF MINNESOTA

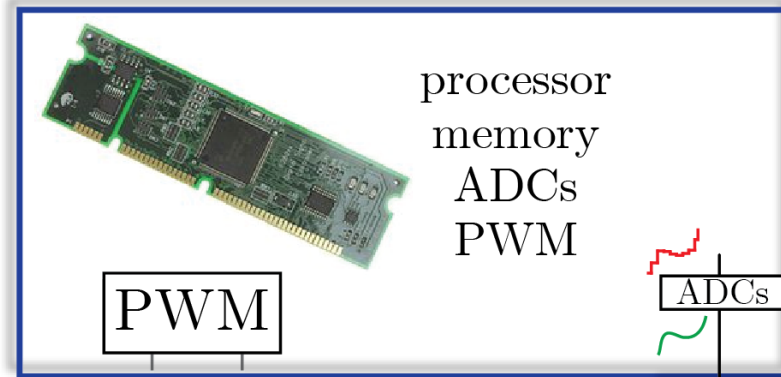
Grid-forming Power Electronics for Low-inertia Power Systems

Sairaj Dhople

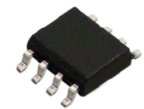
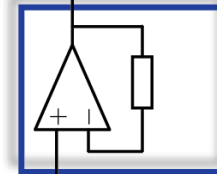
Associate Professor || Department of Electrical and Computer Engineering
sdhople@umn.edu || sairajdhople.umn.edu

Building Block

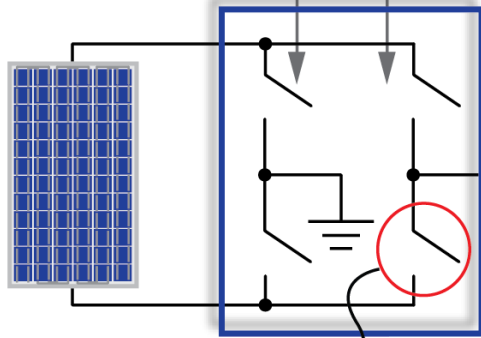
Microcontroller



Measurements



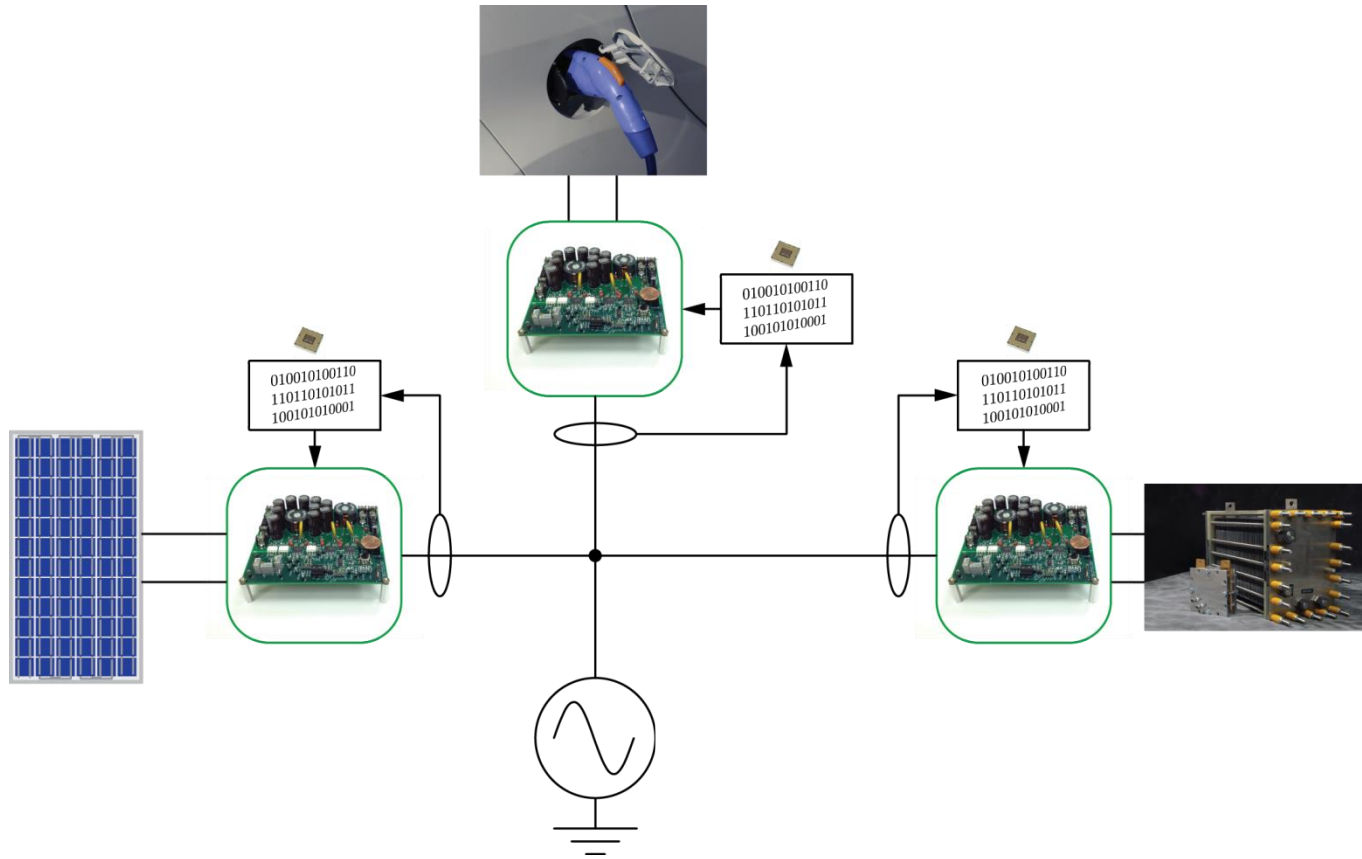
Filter Components



Power Semiconductors



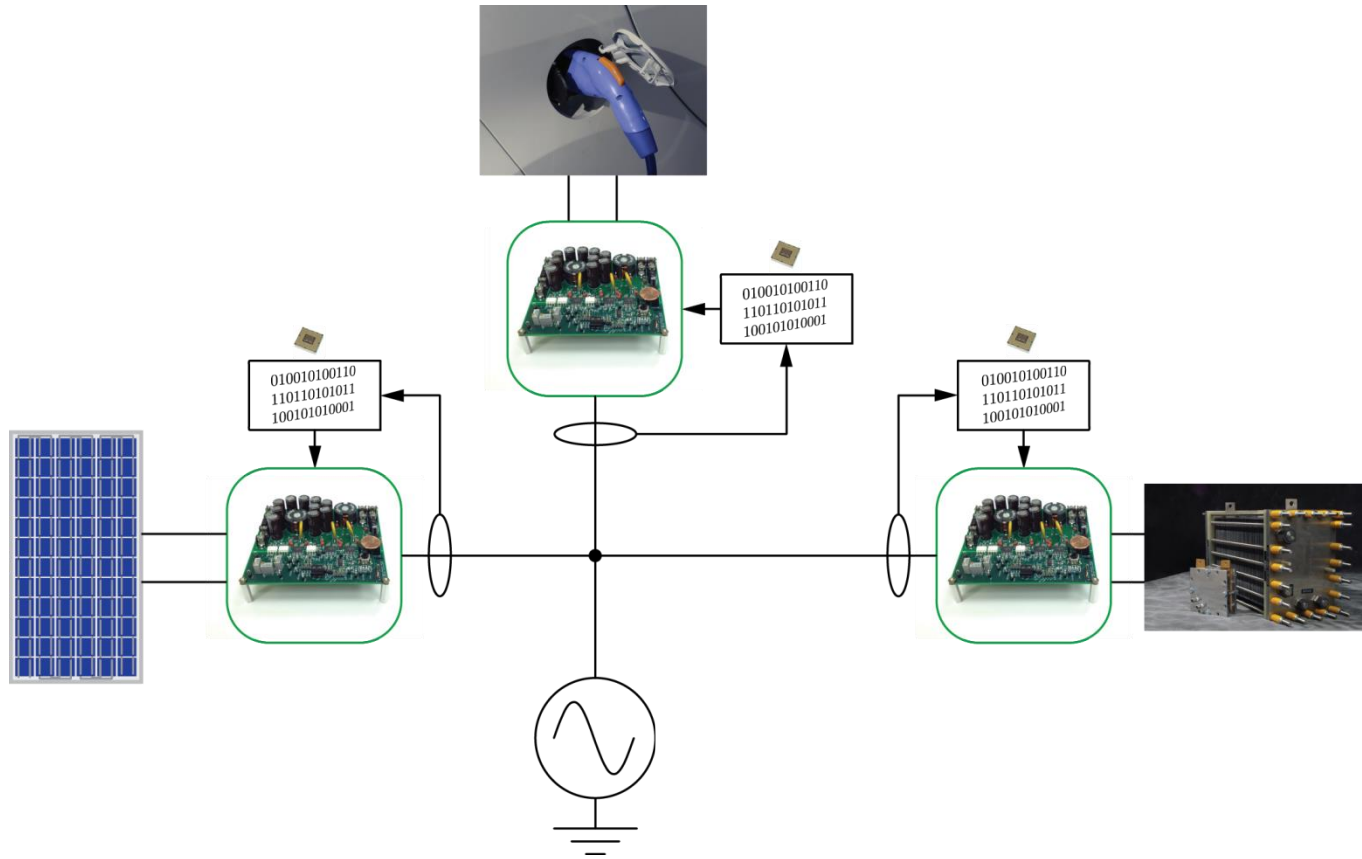
System Architecture



- Heterogeneous DC energy resources
- Semiconductor-based energy conversion
- High-bandwidth digital control



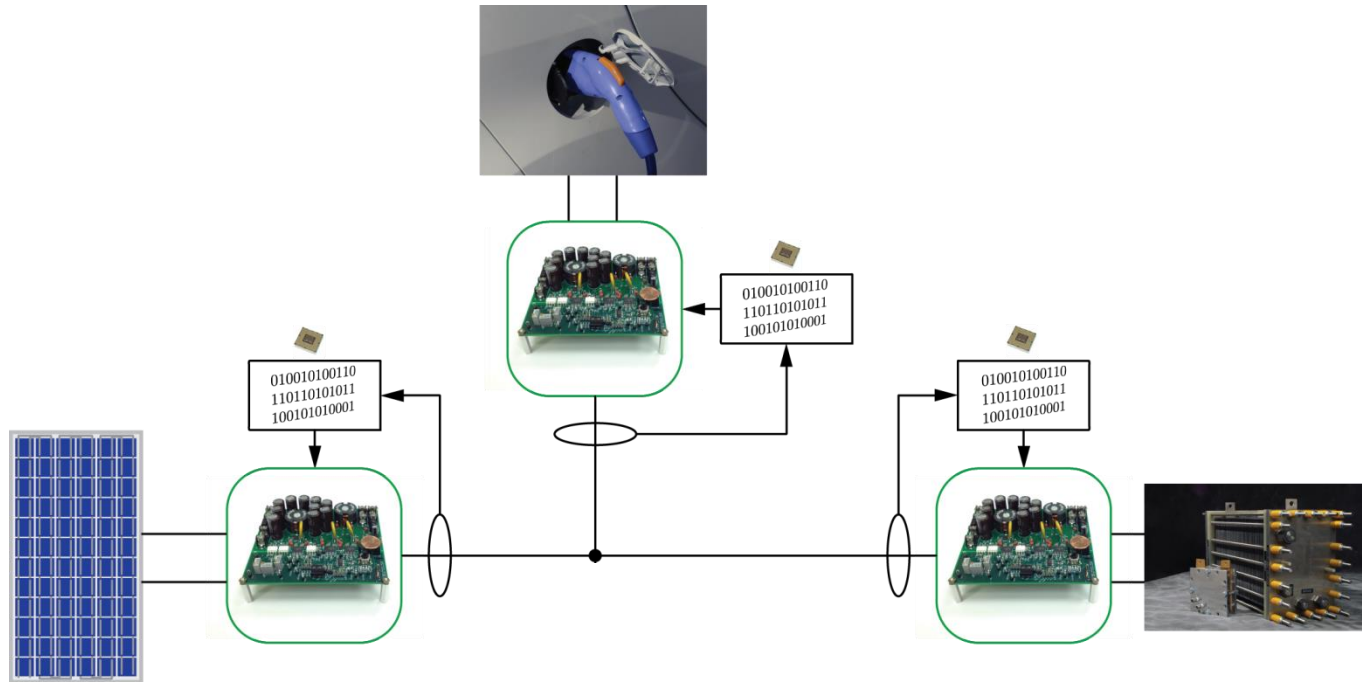
Challenges



- Variability, volatile dynamics
- Minimize communication, plug-and-play operation
- Low-to-no inertia



Challenges

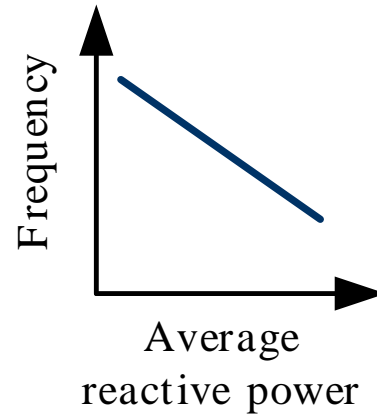
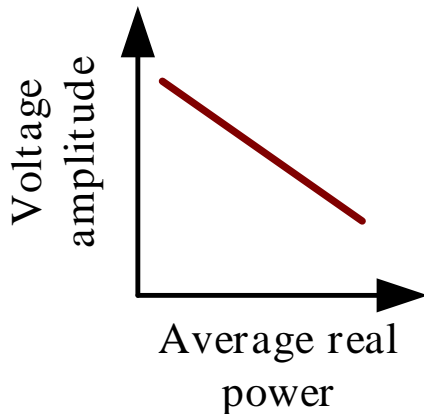
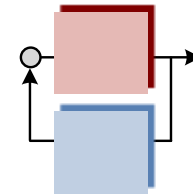


- Variability, volatile dynamics
- Minimize communication, plug-and-play operation
- Low-to-no inertia



State of the Art

- Droop Control^{[1]-[2]}
- Inverters mimic synchronous machines
- Limitations
 - Assumes sinusoidal steady state
 - Slow dynamics
 - Hierarchical control

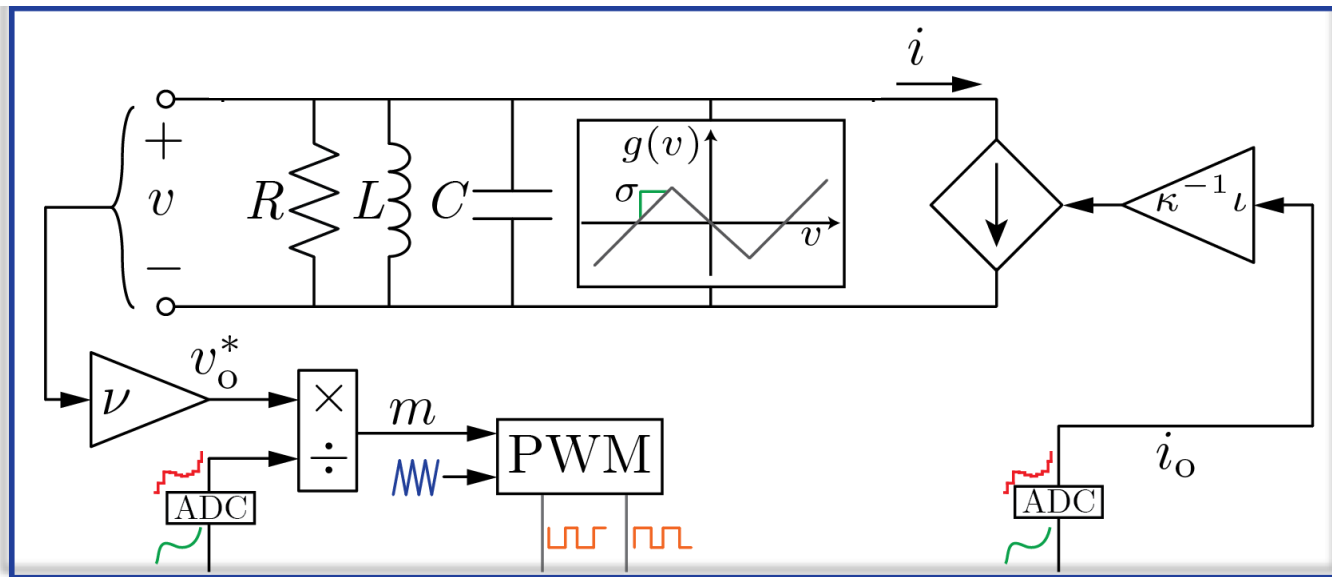


[1] M. Chandorkar, D. Divan, and R. Adapa, "Control of parallel connected inverters in standalone ac supply systems," *IEEE Transactions on Industrial Applications*, 1993.

[2] R. Lasseter, "Microgrids," *IEEE PES Winter Meeting*, 2002.



Time-domain Alternative

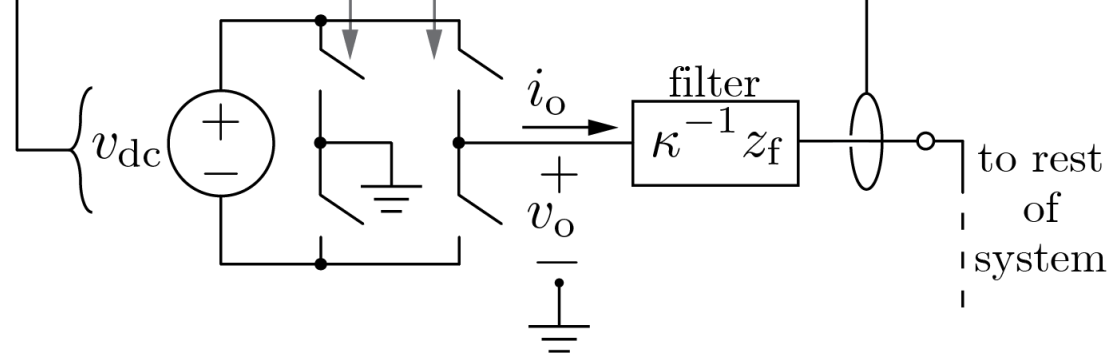


micro-
controller

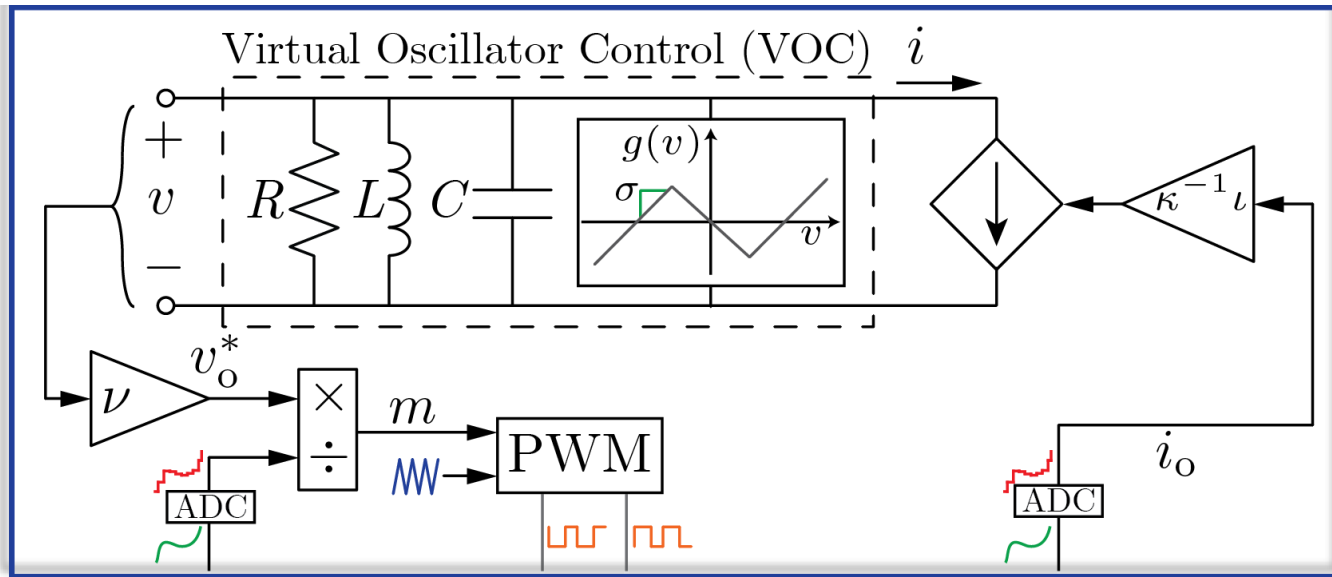


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110110101011
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power
electronics



Virtual Oscillator Control: VOC

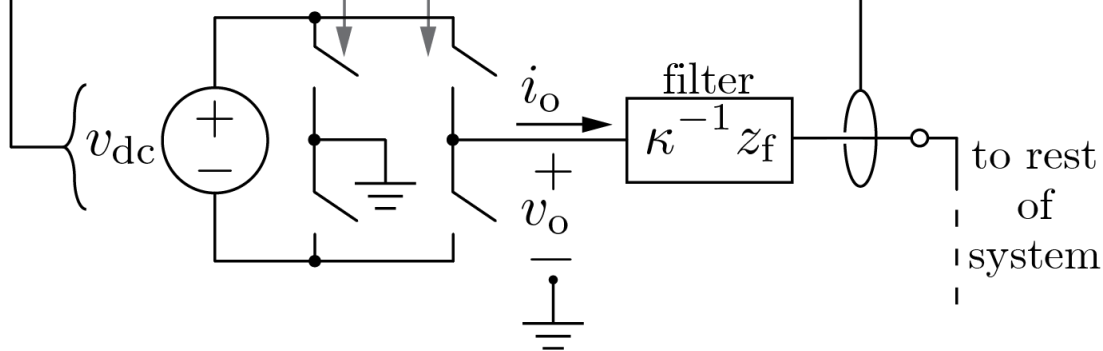


micro-
controller



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power
electronics



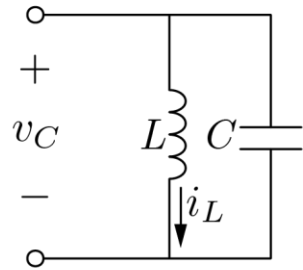
Features & Advantages



Features & Advantages

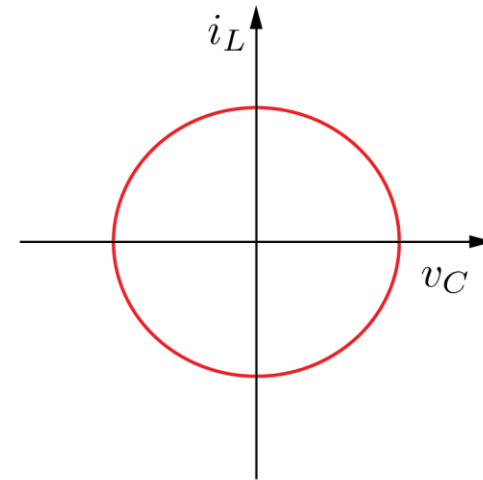
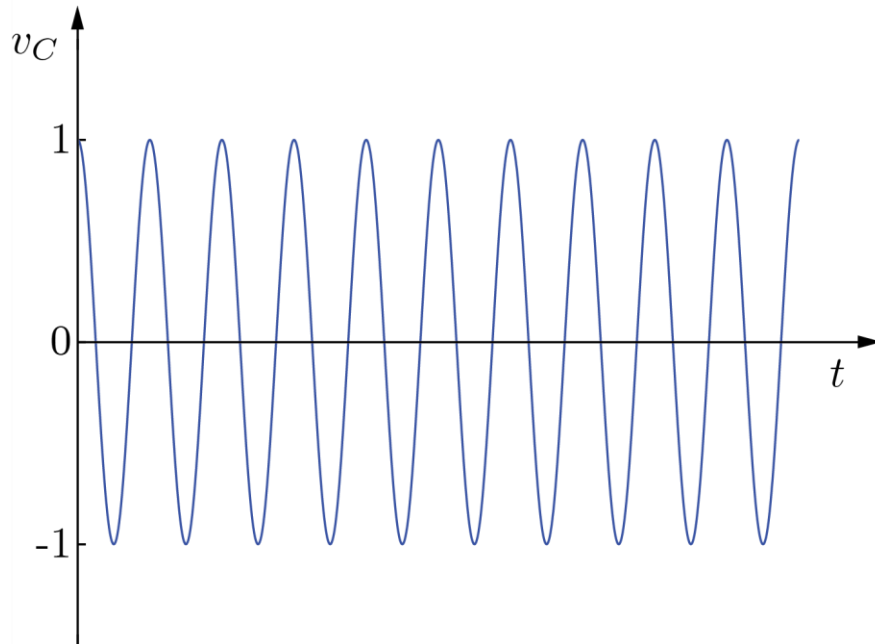


Harmonic Oscillator

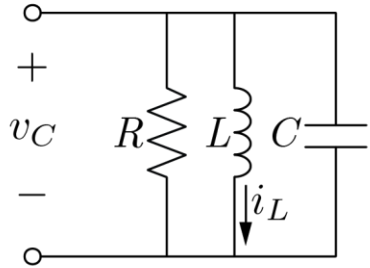


$$\ddot{v}_C + \frac{1}{LC}v_C = 0$$

$$\omega = \frac{1}{\sqrt{LC}}$$

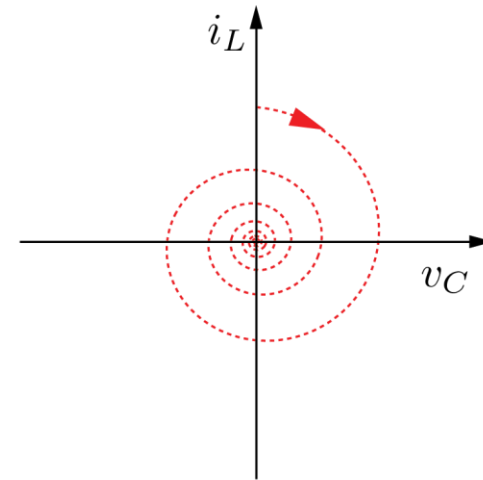
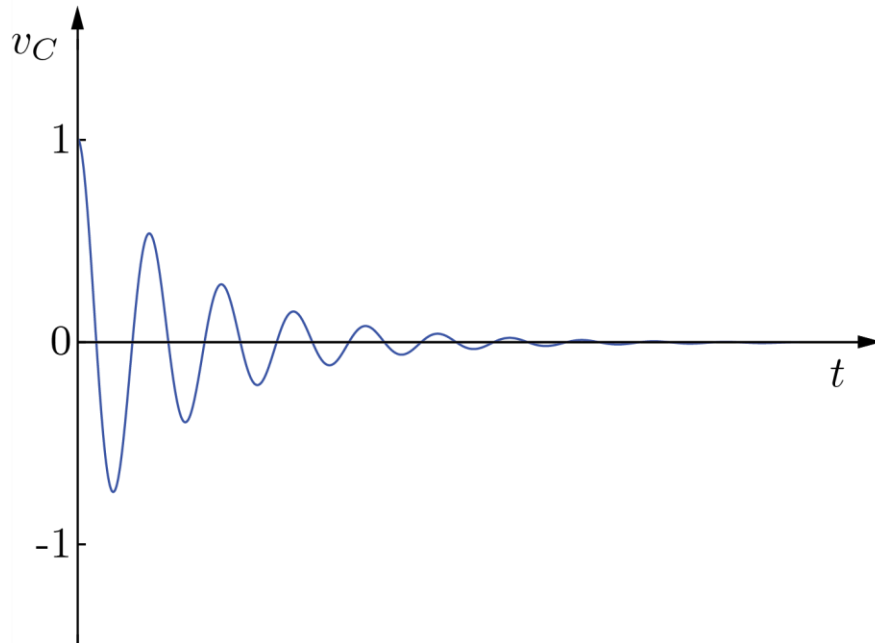


Damped Oscillator

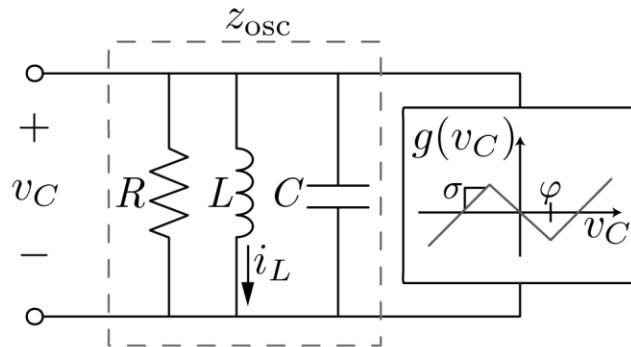


$$\ddot{v}_C + \frac{1}{RC}\dot{v}_C + \frac{1}{LC}v_C = 0$$

$$\omega = \frac{1}{\sqrt{LC}}$$



Dead-zone Oscillator



Yields self-sustaining
oscillations

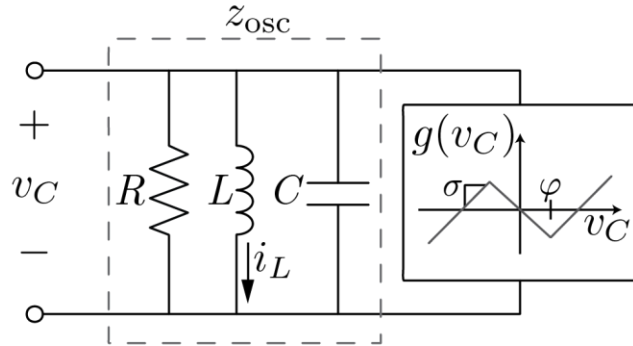
Parameter selection:

$$\omega = \frac{1}{\sqrt{LC}} \rightarrow \text{sets frequency}$$

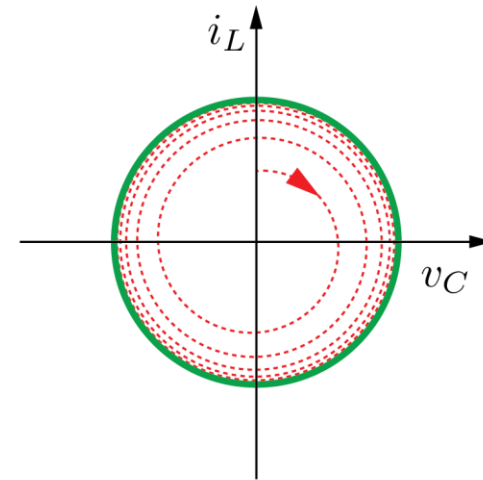
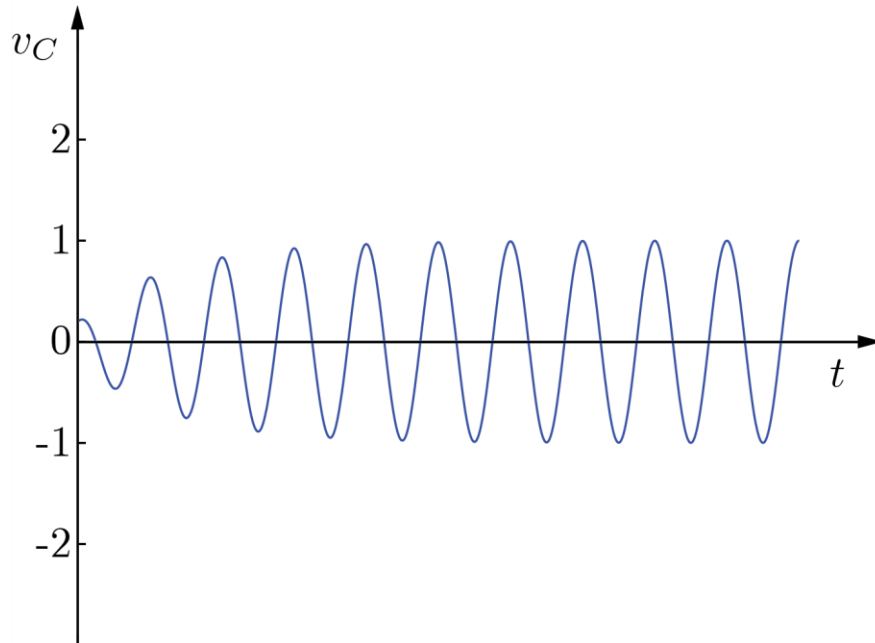
$$\left(\sigma - \frac{1}{R}\right) \text{ and } \varphi \rightarrow \text{set amplitude}$$



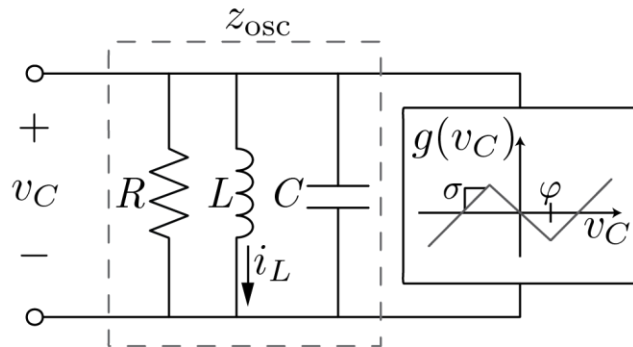
Dead-zone Oscillator



$$\ddot{v}_C + \frac{1}{C} \left(\frac{1}{R} + \frac{dg(v_C)}{dv_C} \right) \dot{v}_C + \frac{1}{LC} v_C = 0$$
$$\omega = \frac{1}{\sqrt{LC}}$$

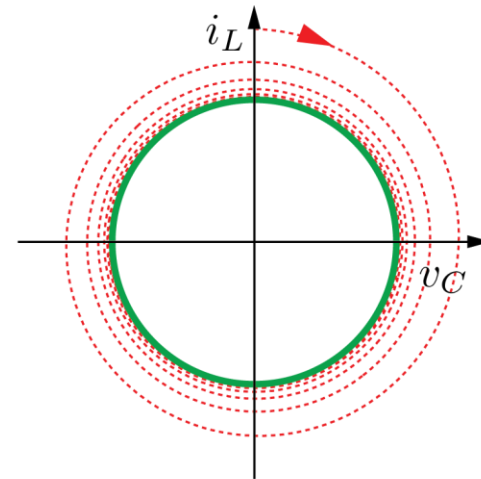
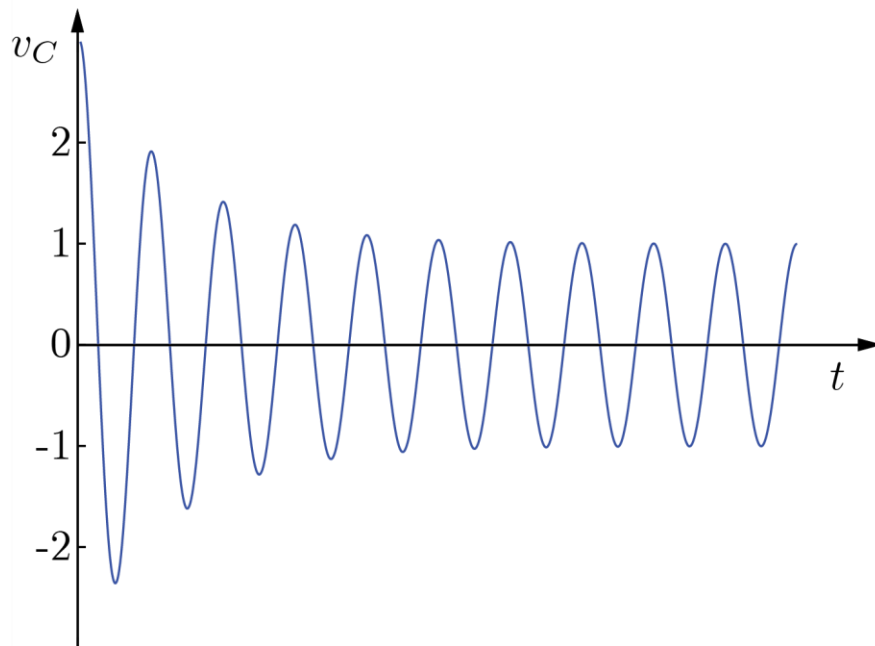


Dead-zone Oscillator

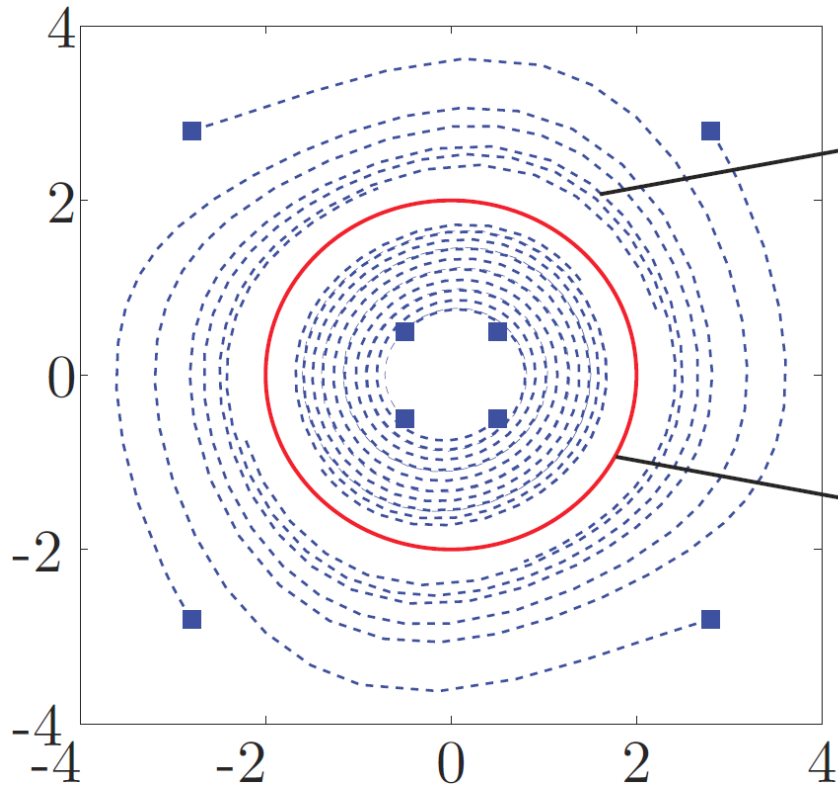


$$\ddot{v}_C + \frac{1}{C} \left(\frac{1}{R} + \frac{dg(v_C)}{dv_C} \right) \dot{v}_C + \frac{1}{LC} v_C = 0$$

$$\omega = \frac{1}{\sqrt{LC}}$$



Time-domain Control

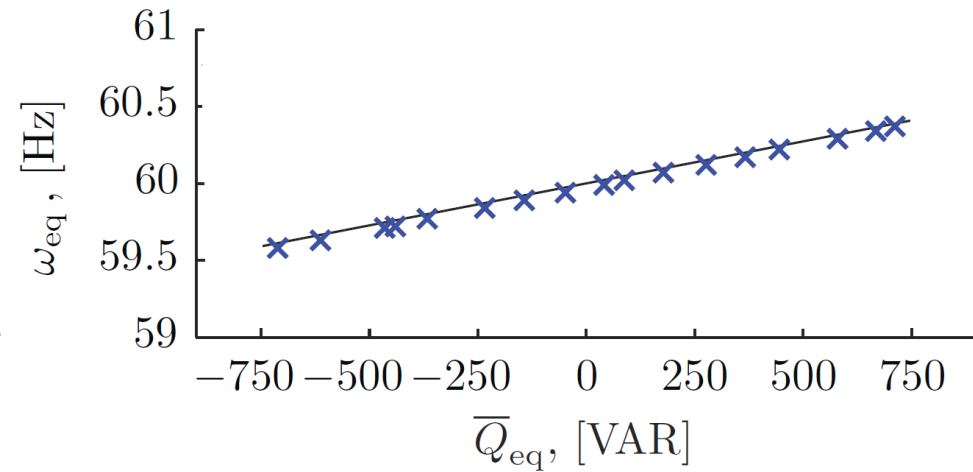
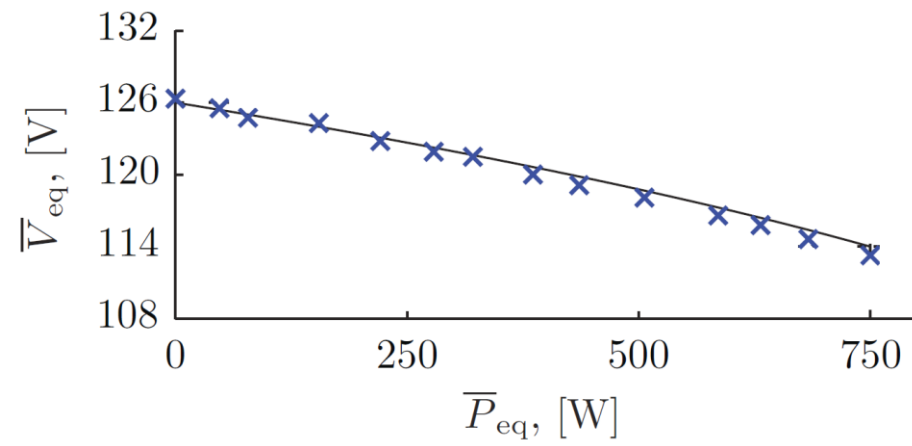


VOC stabilizes arbitrary waveforms to sinusoidal steady state

Droop control only acts on sinusoidal steady state



"Contains" Droop



× Experimental

— Analytical



Features & Advantages



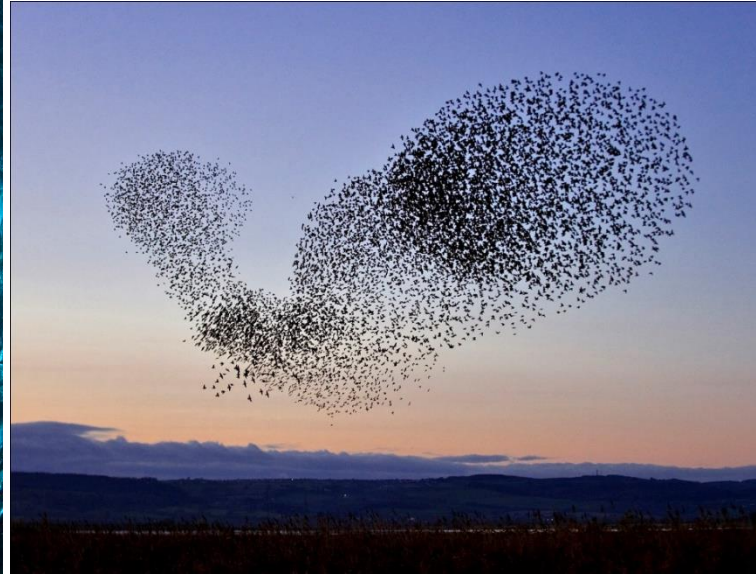
Features & Advantages



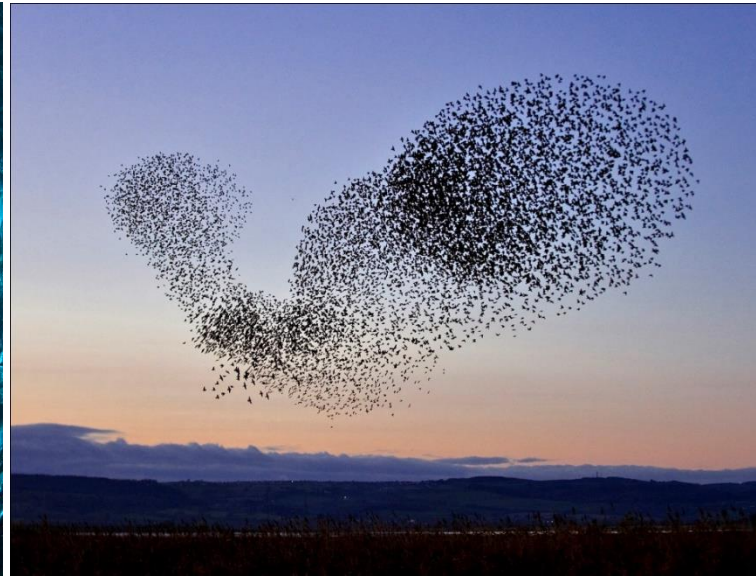
Synchronization in Nature



Synchronization in Nature

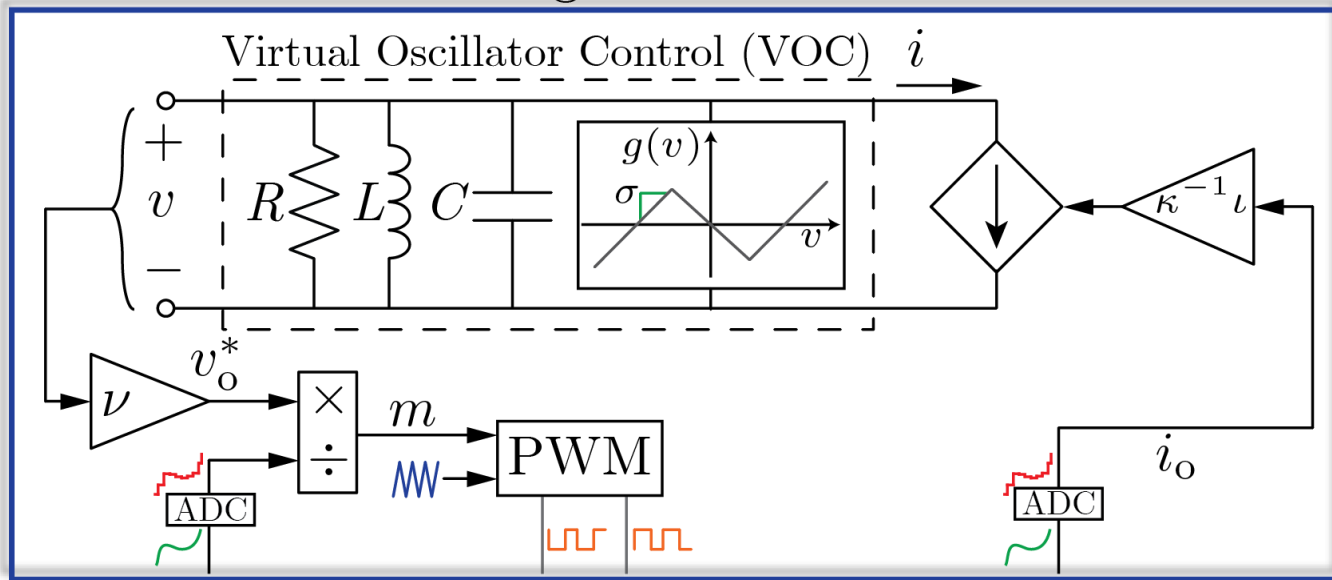


Synchronization in Nature



Recall the Controller

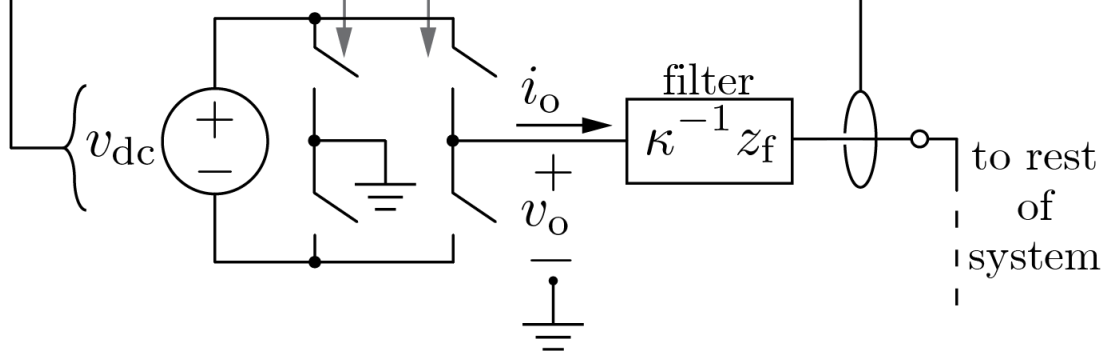
Digital Control



micro-
controller



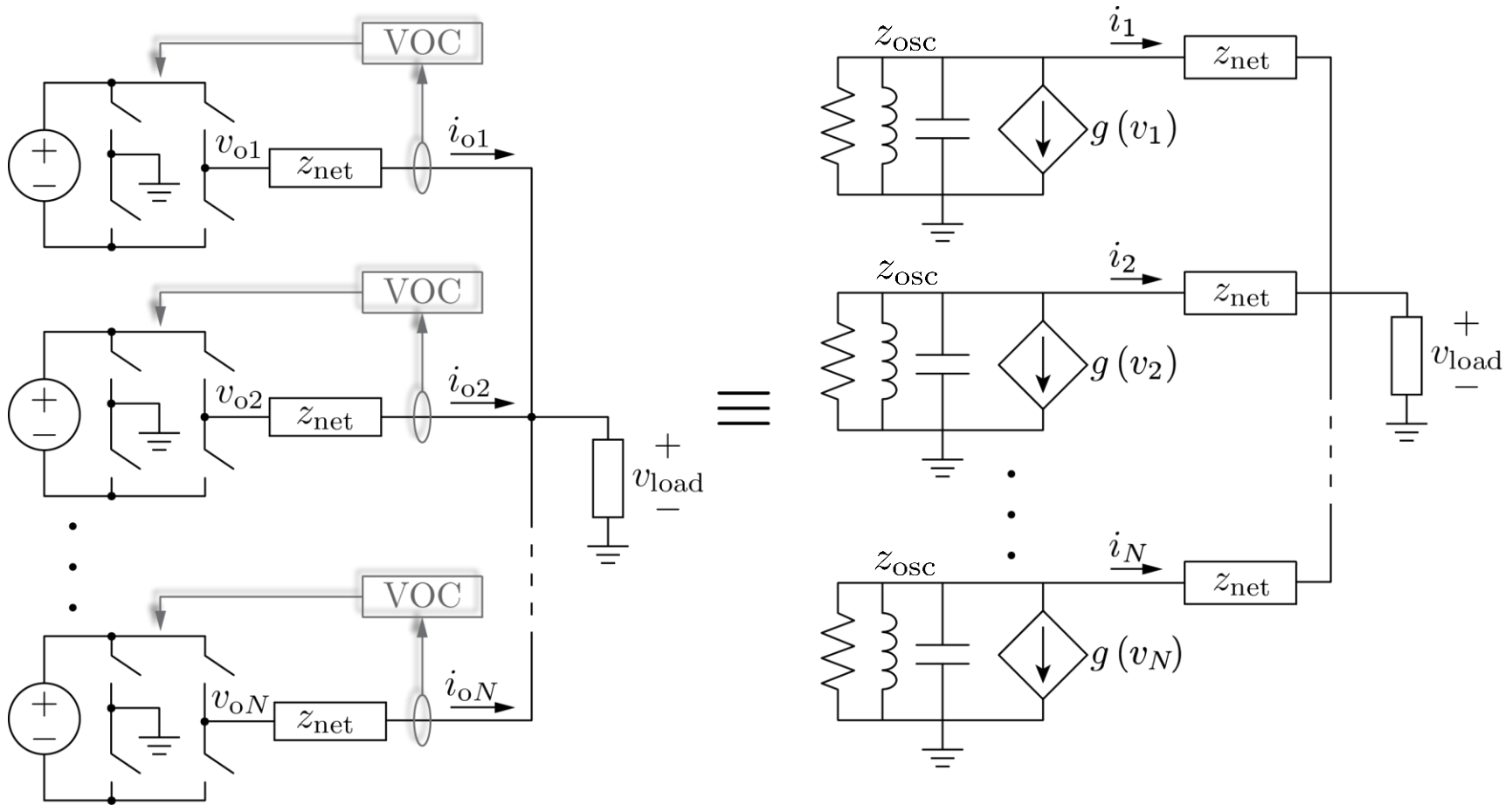
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power
electronics



System-level Behavior

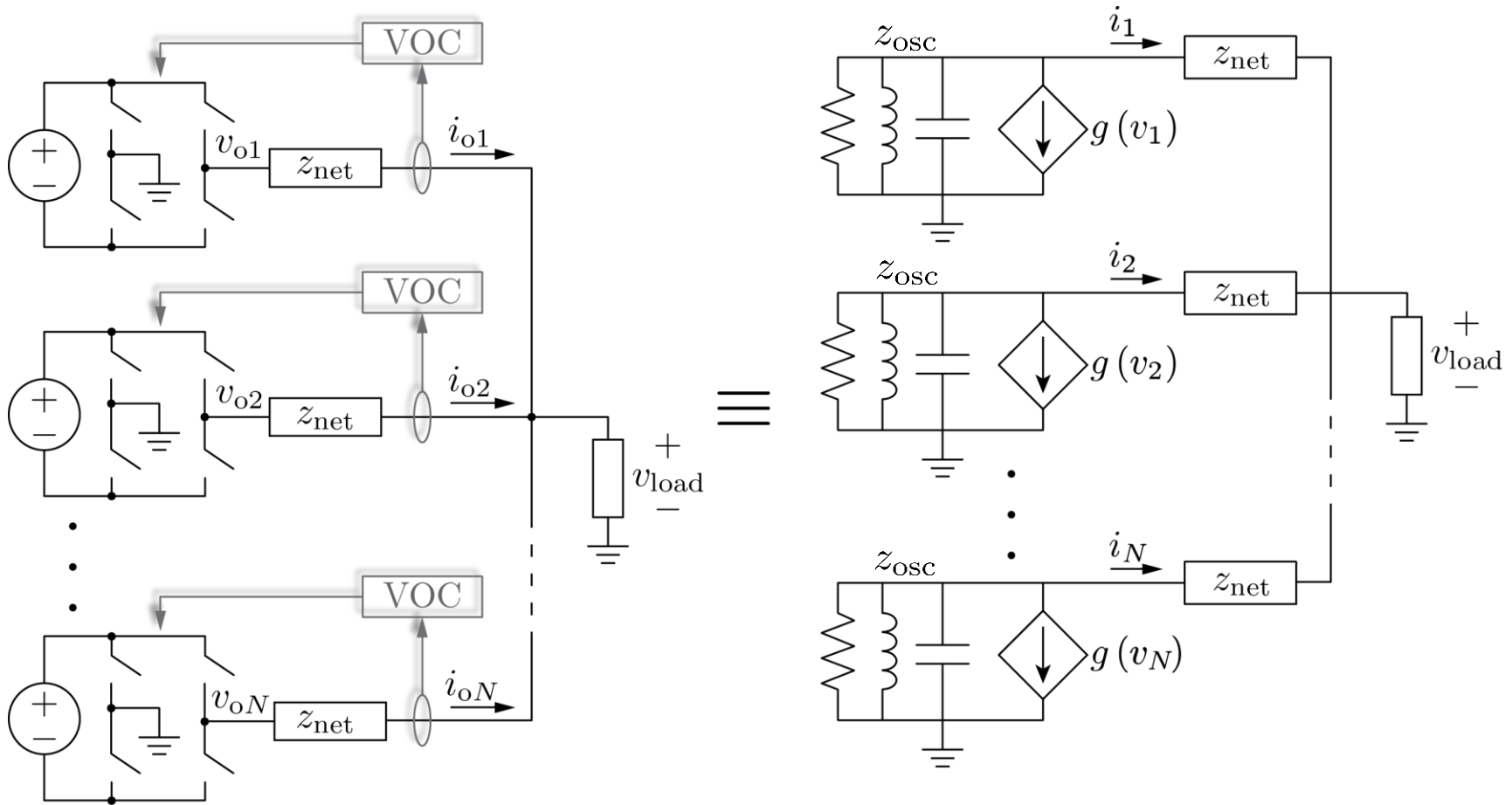


Global asymptotic synchronization

$$\lim_{t \rightarrow \infty} v_j(t) - v_k(t) = 0 \quad \forall j, k = 1, \dots, N$$



System-level Behavior

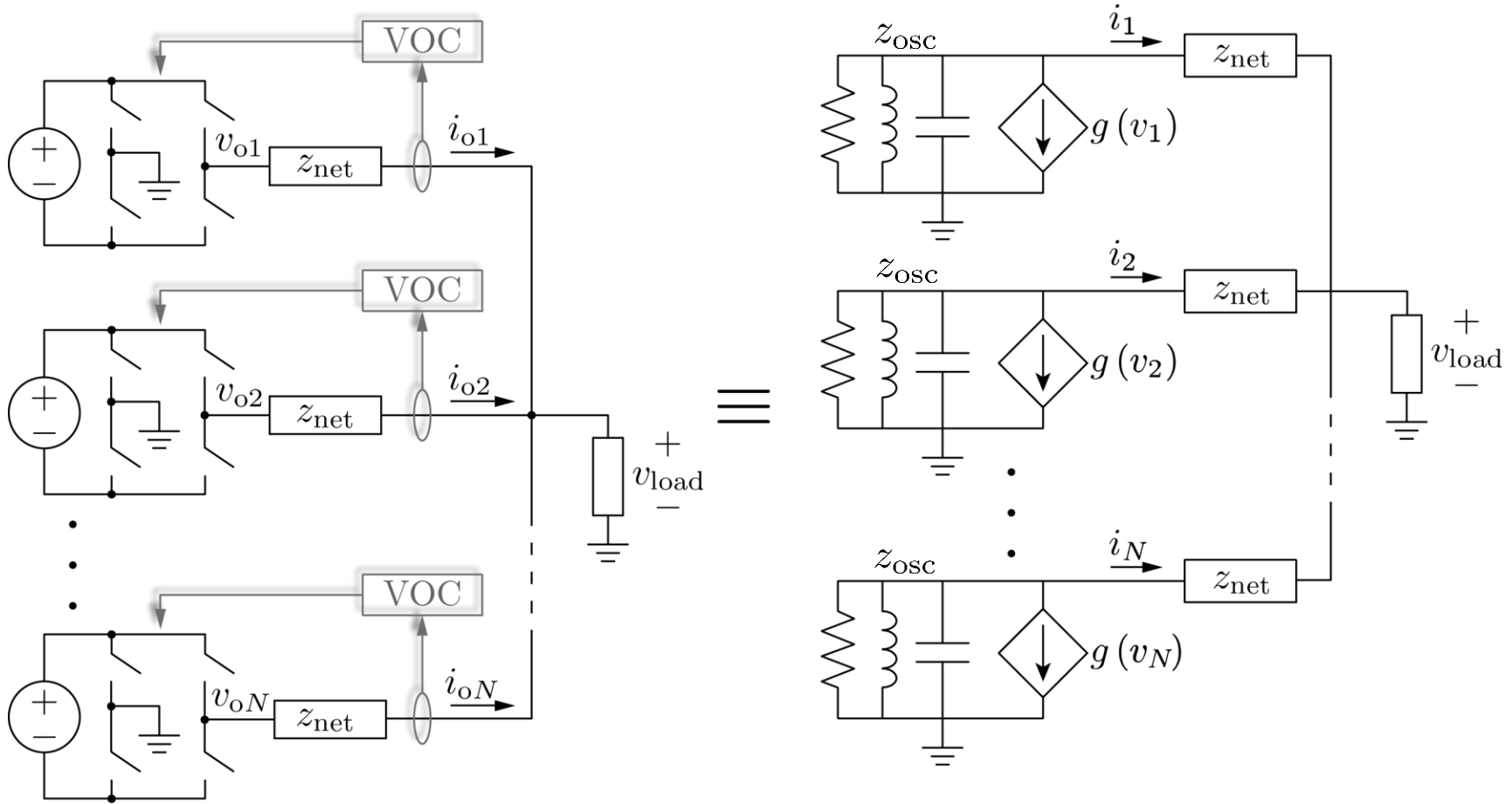


Condition for global asymptotic synchronization

$$\sup_{\omega \in \mathbb{R}} \left\| \frac{z_{\text{net}}(j\omega) z_{\text{osc}}(j\omega)}{z_{\text{net}}(j\omega) + z_{\text{osc}}(j\omega)} \right\|_2 \sigma < 1$$



System-level Behavior



- Modular
 - Robust
 - Resilient
- Condition for global asymptotic synchronization
- $$\sup_{\omega \in \mathbb{R}} \left\| \frac{z_{net}(j\omega) z_{osc}(j\omega)}{z_{net}(j\omega) + z_{osc}(j\omega)} \right\|_2 \sigma < 1$$

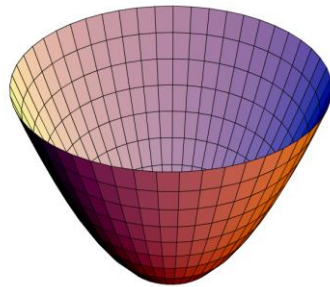
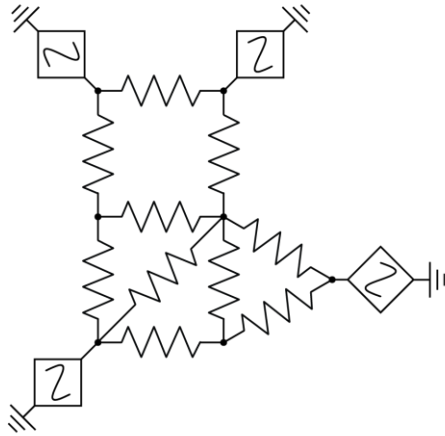


Proof Sketch

$$\begin{aligned}\tilde{\gamma}(\mathcal{F}(Z_{\text{osc}}(s), Y(s))) &= \tilde{\gamma}(\mathcal{F}(\zeta(s)I, \beta(s)\Gamma)) \\ &= \|\mathcal{F}(\zeta(s)I, \beta(s)\Gamma)\|_{\infty} \\ &= \sup_{\omega \in \mathbb{R}} \frac{\|(I + \zeta(j\omega)\beta(j\omega)\Gamma)^{-1} \zeta(j\omega)\tilde{i}_g(j\omega)\|_2}{\|\tilde{i}_g(j\omega)\|_2} \\ &= \sup_{\omega \in \mathbb{R}} \frac{\|Q(I + \zeta(j\omega)\beta(j\omega)\Lambda)^{-1} \zeta(j\omega)Q^T\tilde{i}_g(j\omega)\|_2}{\|Q^T\tilde{i}_g(j\omega)\|_2}\end{aligned}$$



State-of-the-Art



- Existing framework: Resistive networks
- Analysis: Storage function proportional to signal differences^{[1]-[3]}
- Power systems: Energy-storage elements pervasive in network
- Consequences: Formulation of storage function is difficult

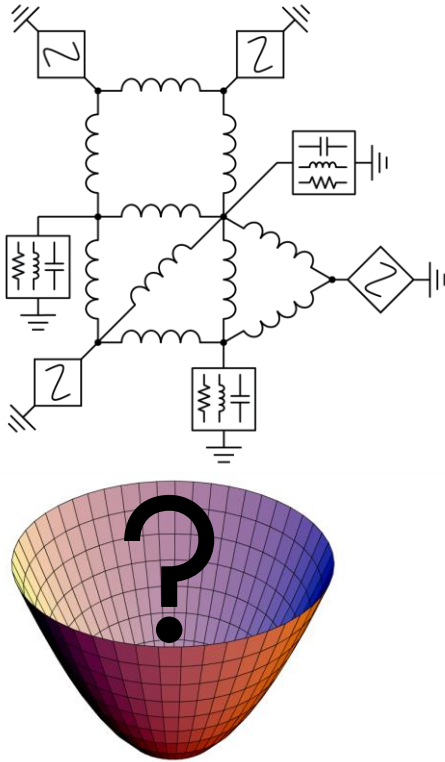
[1] M. Arcak, "Passivity as a design tool for group coordination," *IEEE Transactions on Automatic Control*, 2007.

[2] G.-B. Stan, R. Sepulchre, "Analysis of interconnected oscillators by dissipativity theory," *IEEE Transactions Automatic Control*, 2007.

[3] A. Pogromsky, H. Nijmeijer, "Cooperative oscillatory behavior of mutually coupled dynamical systems," *IEEE Transactions on Circuits and Systems*, 2001.



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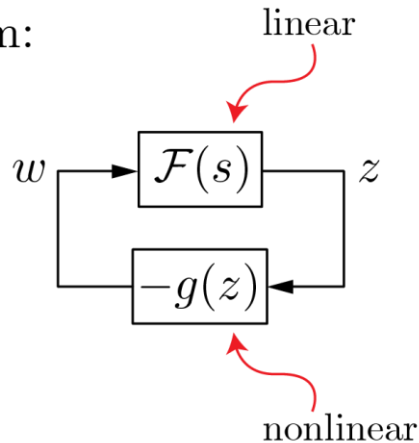
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Our Approach

original system:



- 1) Compartmentalize subsystems
- 2) Coordinate transformation
- 3) Prove stability

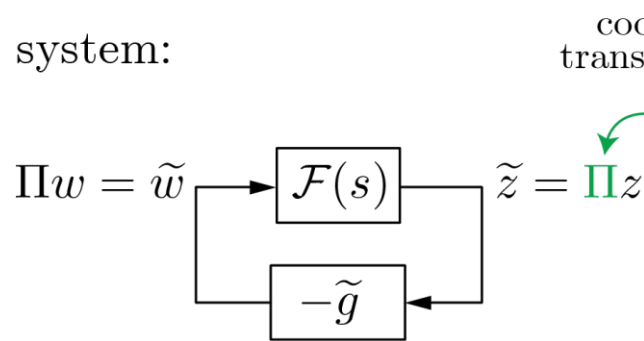
[1] S. Dhople, B. Johnson, F. Dörfler, A. Hamadeh, "Synchronization of nonlinear circuits in dynamic electrical networks with general topologies," *IEEE Transactions on Circuits and Systems*, 2014.

[2] B. Johnson, S. Dhople, A. Hamadeh, P. Krein, "Synchronization of nonlinear oscillators in an LTI electrical network," *IEEE Transactions on Circuits and Systems*, 2014.



Our Approach

differential system:



coordinate
transformation

- 1) Compartmentalize subsystems
- 2) Coordinate transformation
- 3) Prove stability

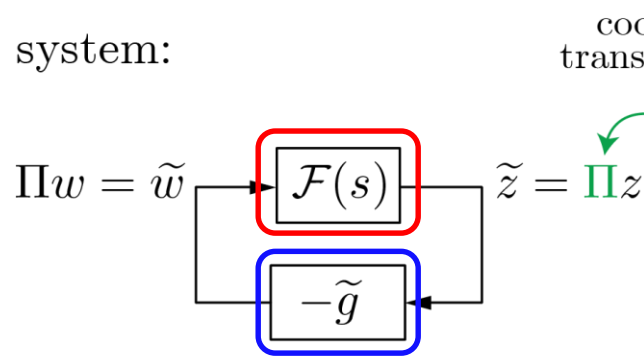
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Our Approach

differential system:



- 1) Compartmentalize subsystems
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$$\sup_{\omega \in \mathbb{R}} \left\| \frac{z_{\text{net}}(j\omega) z_{\text{osc}}(j\omega)}{z_{\text{net}}(j\omega) + z_{\text{osc}}(j\omega)} \right\|_2 \sigma < 1$$

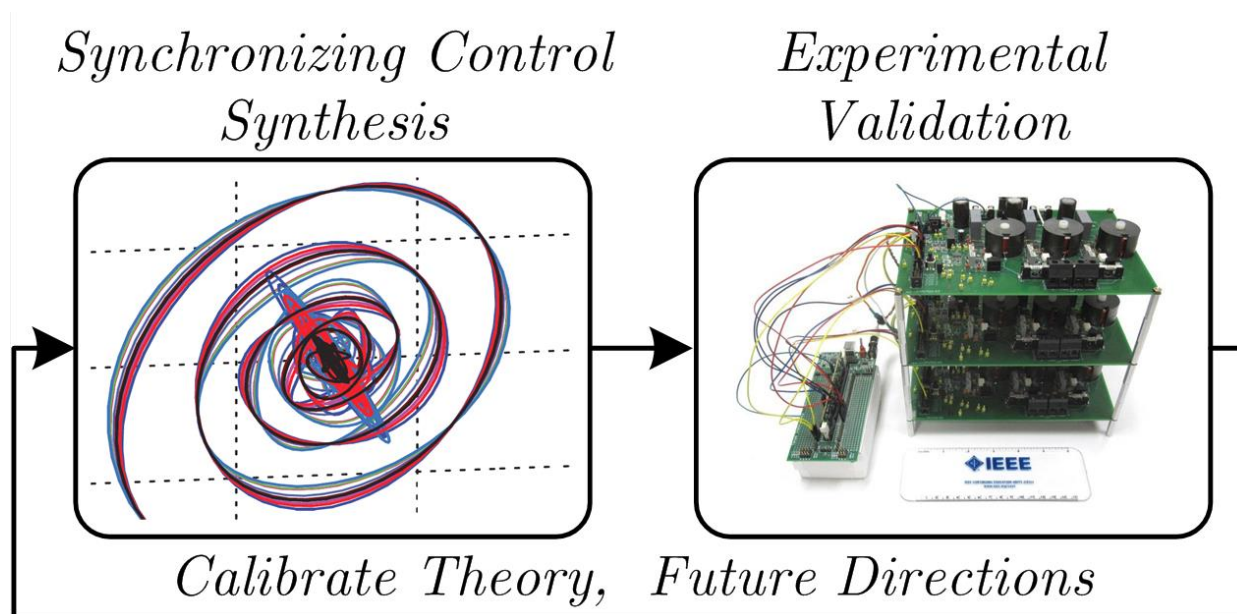
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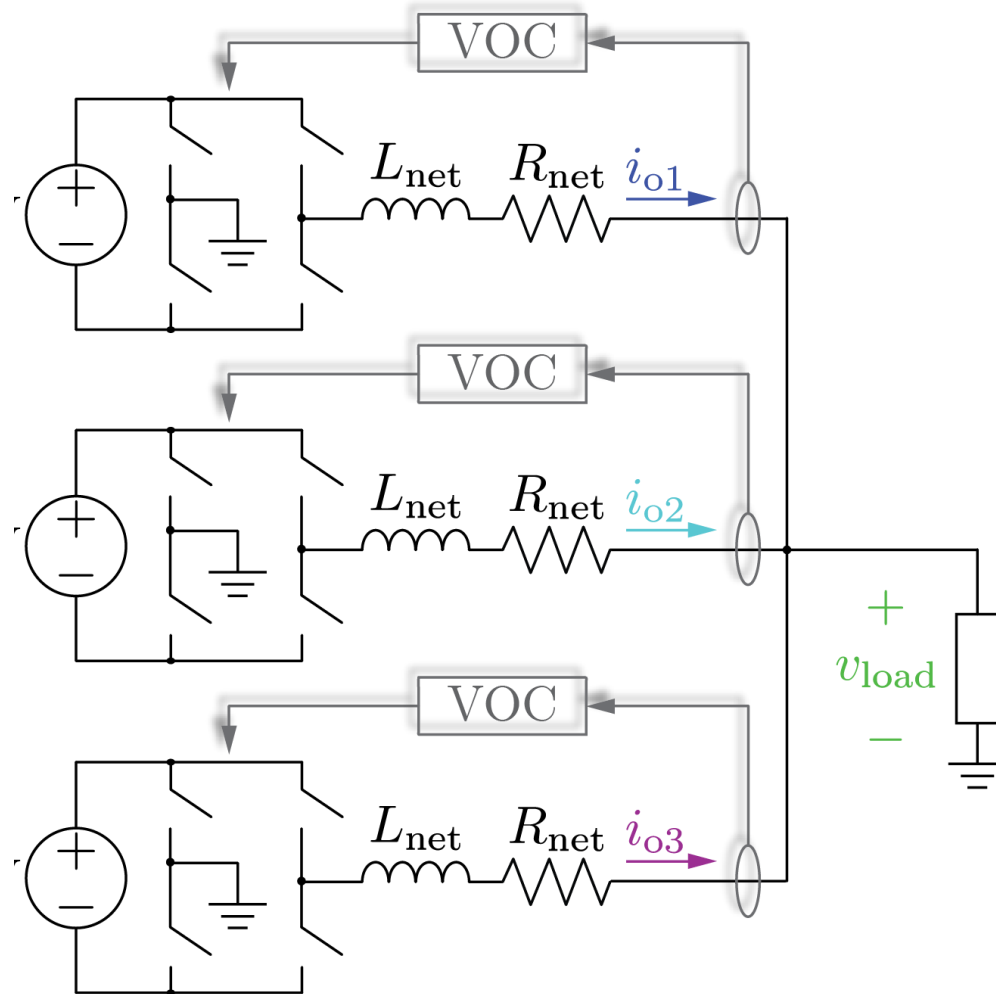
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Research Philosophy



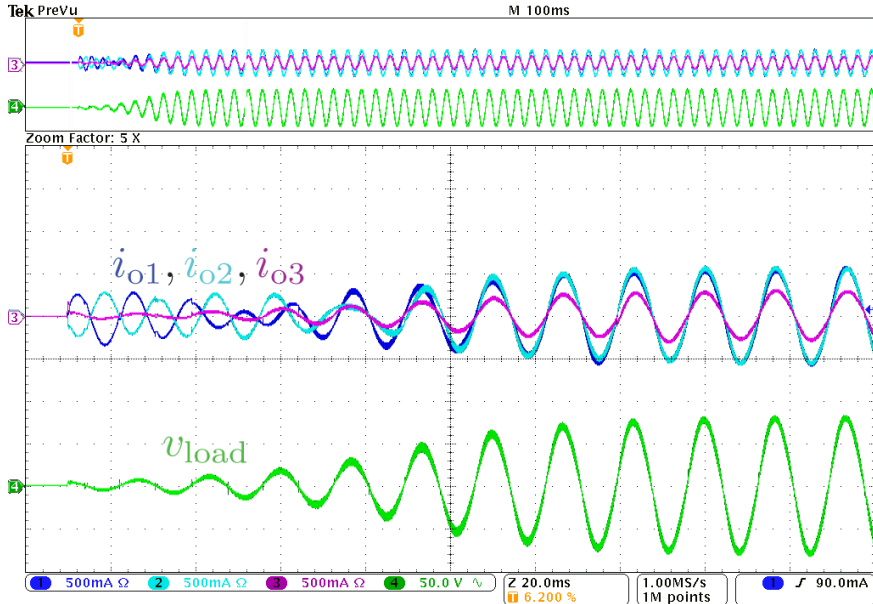
Experimental Setup



[1] B. Johnson, S. Dhople, A. Hamadeh, and P. Krein, "Synchronization of parallel single-phase inverters with virtual oscillator control," *IEEE Transactions on Power Electronics*, 2014.

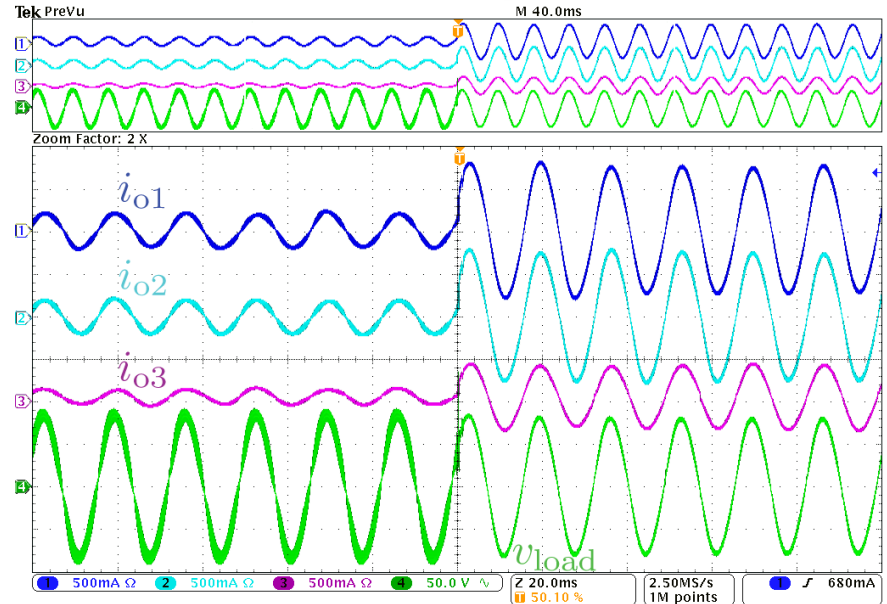


Resistive Load (Sharing)



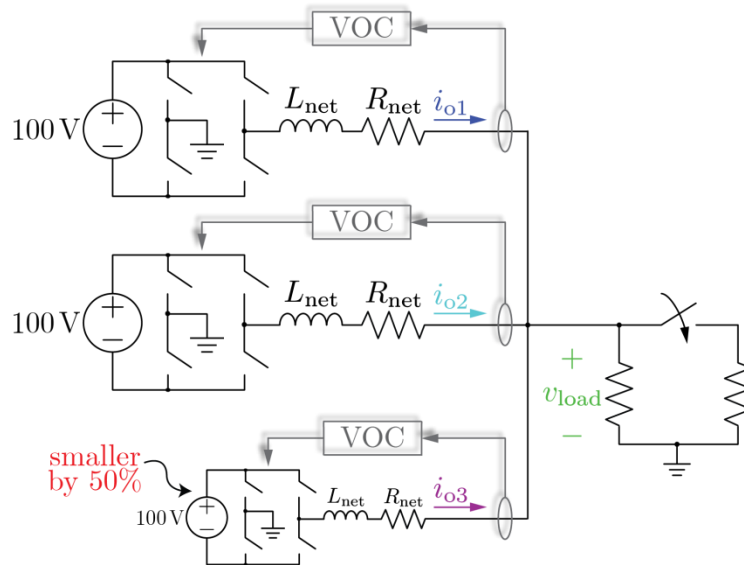
Startup

14 Dec 2012
10:15:50

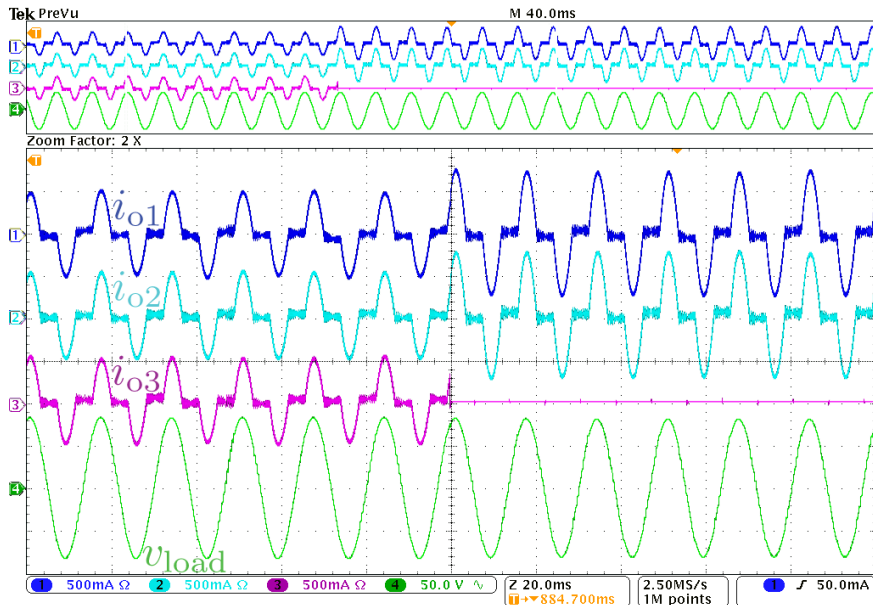


Load Step Up

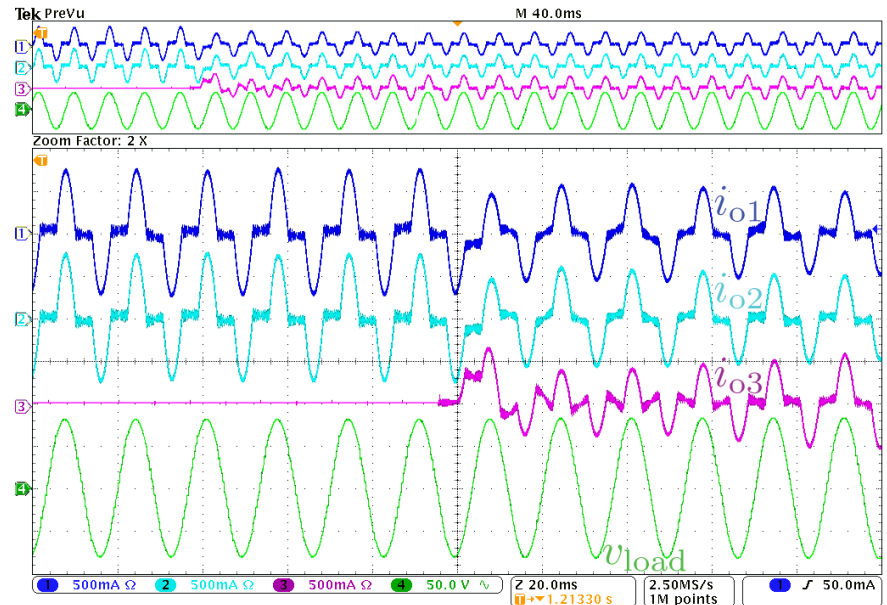
13 Dec 2012
10:48:17



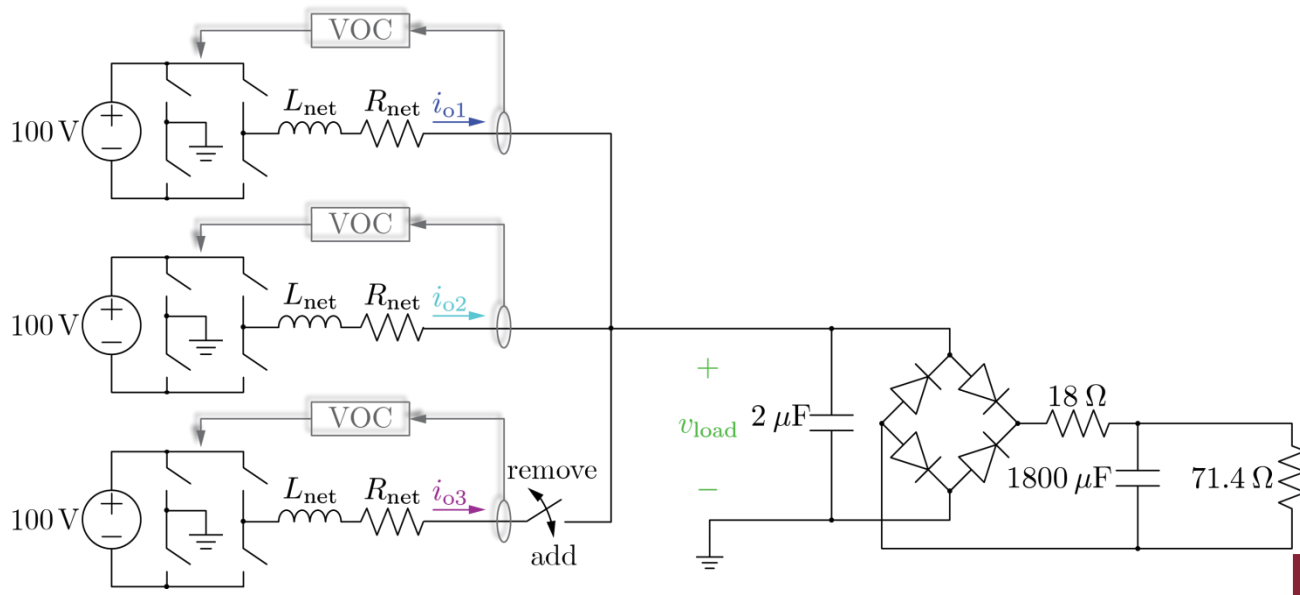
Nonlinear Load



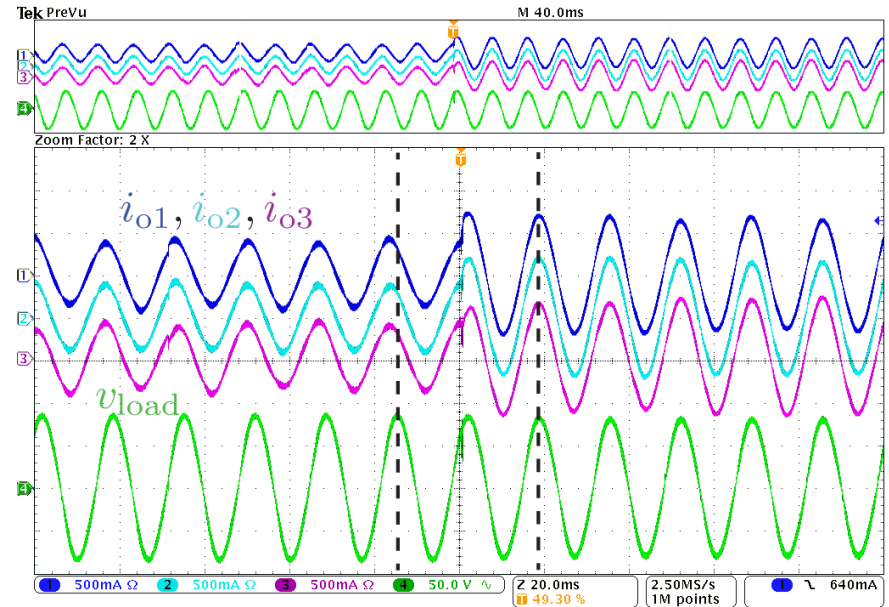
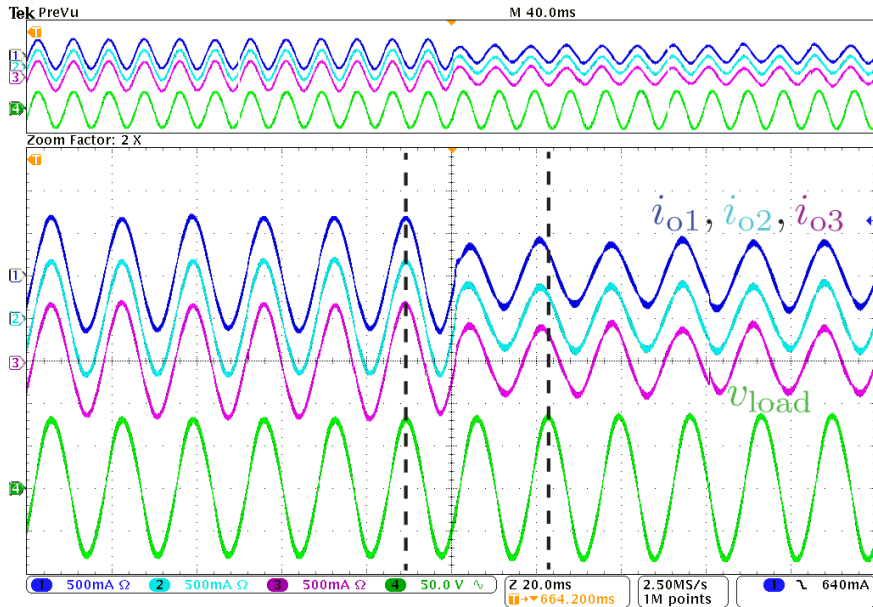
Inverter Removal



Inverter Addition

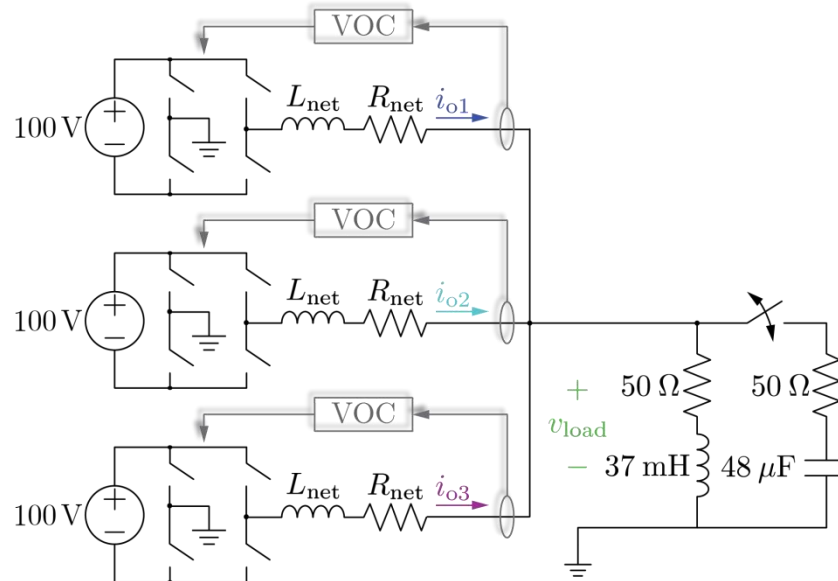


RLC Load

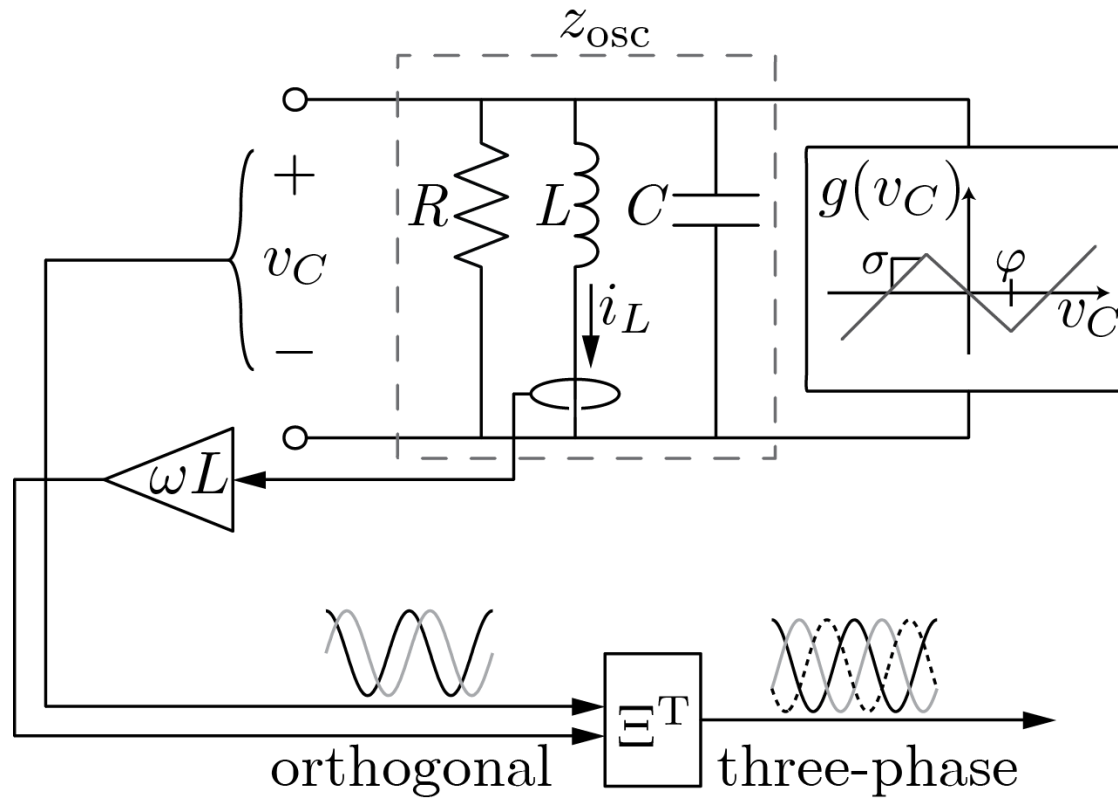


Load Step Down: $RLC \rightarrow RL$ 10 Dec 2012 16:55:43

Load Step Up: $RL \rightarrow RLC$ 10 Dec 2012 16:44:27



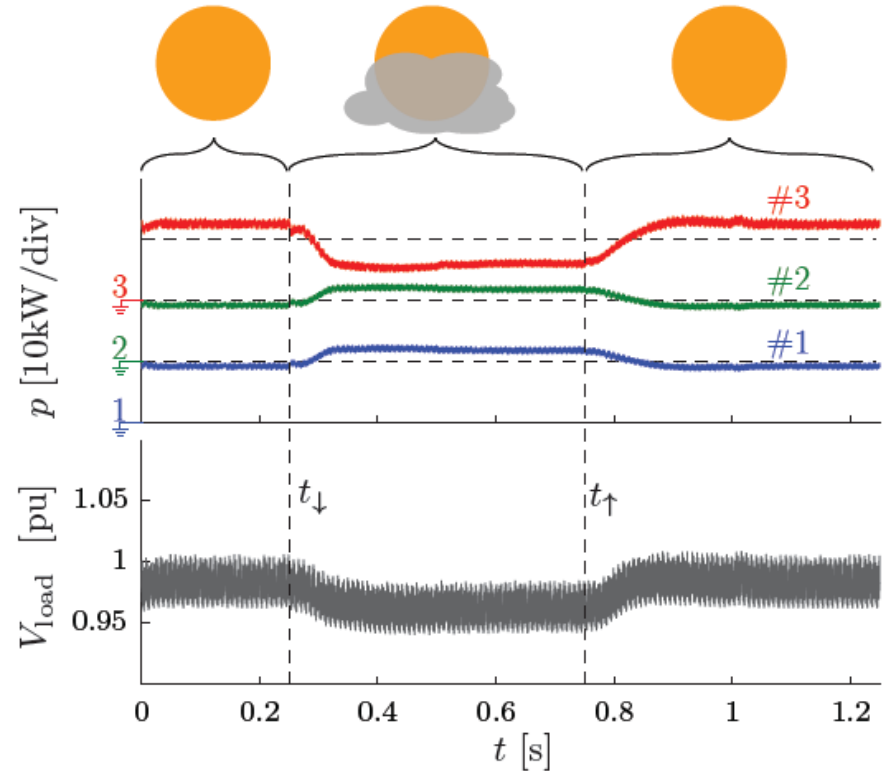
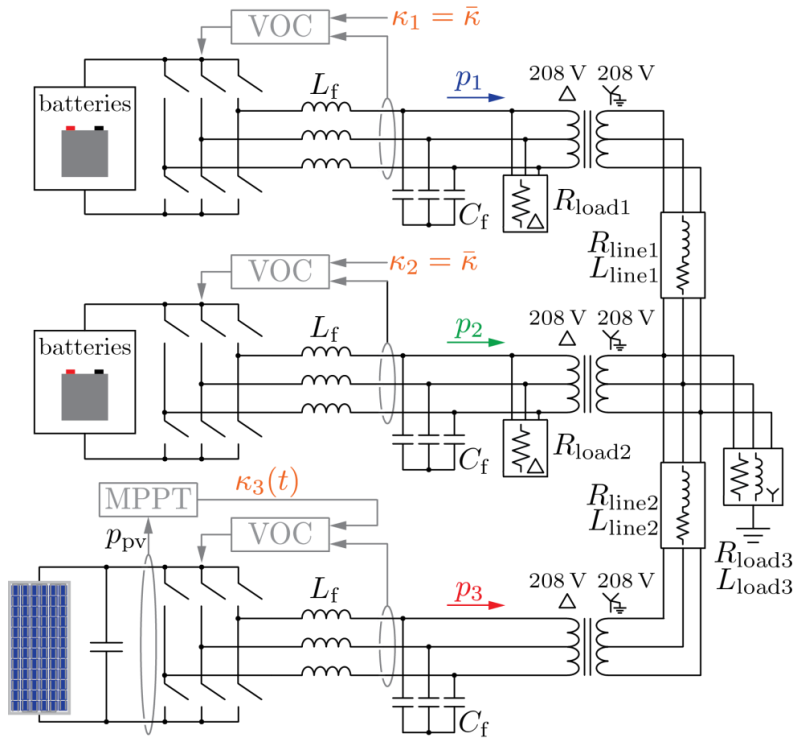
Three-phase Systems



[1] B. Johnson, S. Dhople, J. Cale, A. Hamadeh, P. Krein, "Oscillator-based control for islanded three-phase microgrids," *IEEE Journal of Photovoltaics*, 2014.



Three-phase Systems



- Three-phase systems with PV
- MPPT functionality incorporated
- Load satisfied despite variable PV generation

[1] B. Johnson, S. Dhople, J. Cale, A. Hamadeh, P. Krein, "Oscillator-based control for islanded three-phase microgrids," *IEEE Journal of Photovoltaics*, 2014.



Summary

- Time-domain control alternative to droop control
- Theoretical guarantees at inverter- and system-level
- Translational impacts: circuit theory, physics, systems biology
- Future work: interoperability, dispatchability, coordination





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