

# Differences between advanced and conventional models in bifacial yield simulations

PVPMC Workshop  
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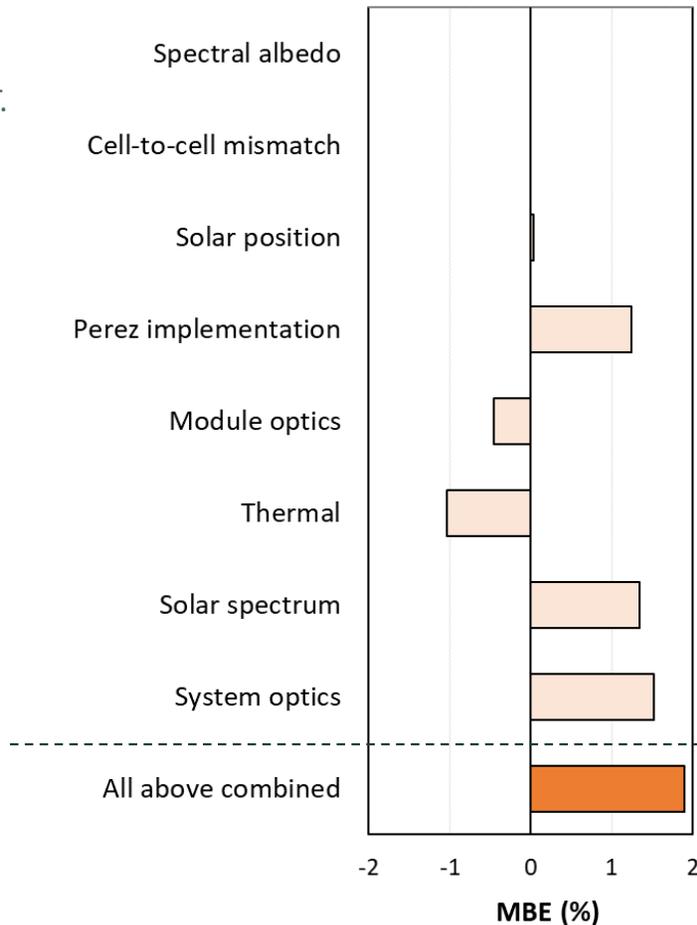
# Objective



- Quantify the difference between models for 8 physical mechanisms
  - Mostly tested with SunSolve-Yield
  - And PVSyst for its VF model
- Three system configurations
  - SATs
  - Fixed-tilt
  - Waves
- Just one location
  - Southwest Utah

# Results preview

Results for typical  
1P SAT located at  
Cove Mountain, UT.

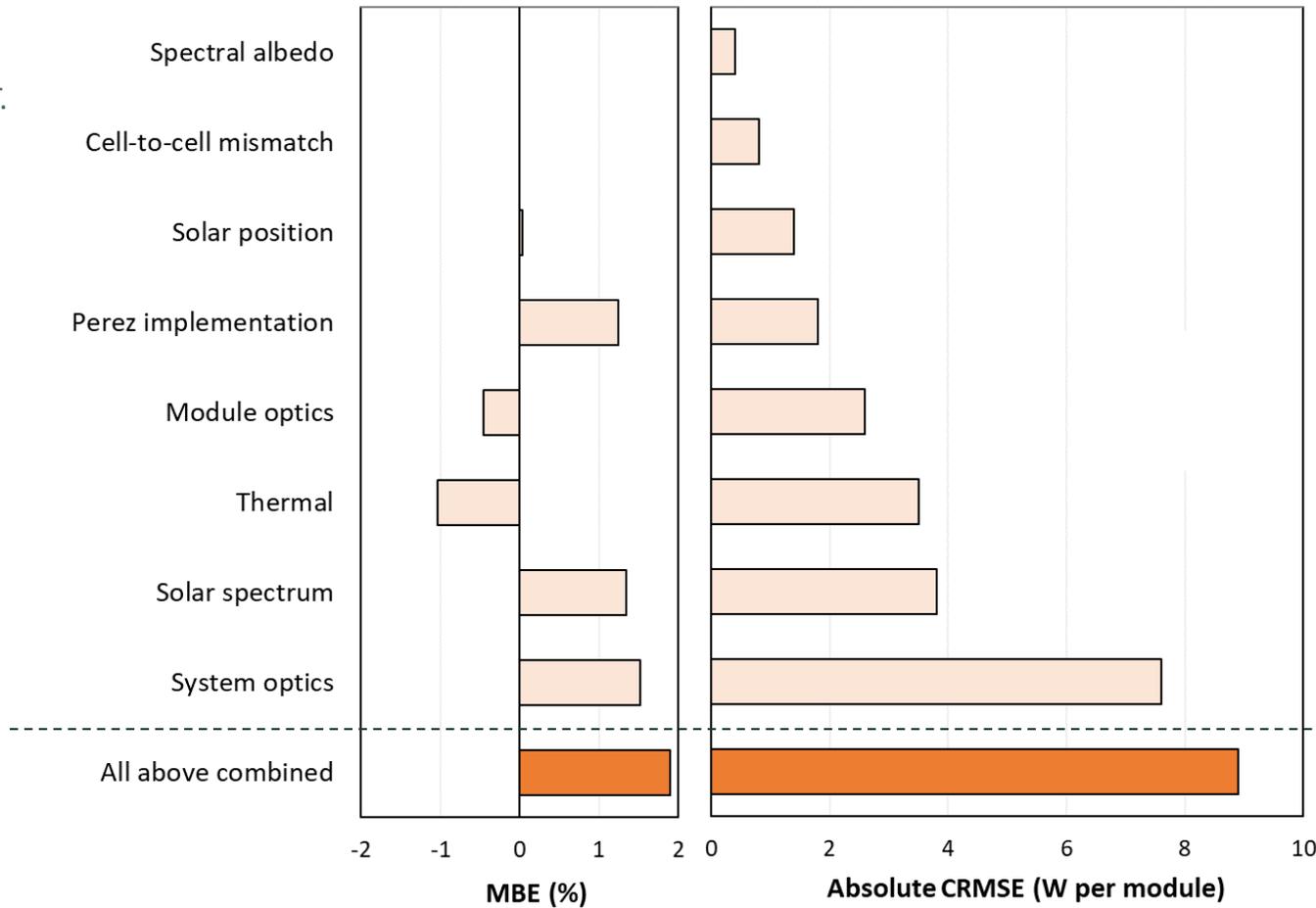


- MBE > 0: yield higher for conventional model than advanced model
- Models are convoluted
  - MBEs of individual models do not sum to MBE of all models combined.
- MBE = 0 does not imply two models are equivalent. Maybe
  - morning discrepancy compensated by noon discrepancy,
  - summer compensated by winter,
  - one poor sub-model compensated by another poor sub-model.

# Results preview



Results for typical  
1P SAT located at  
Cove Mountain, UT.



Average  $P_{mod}$

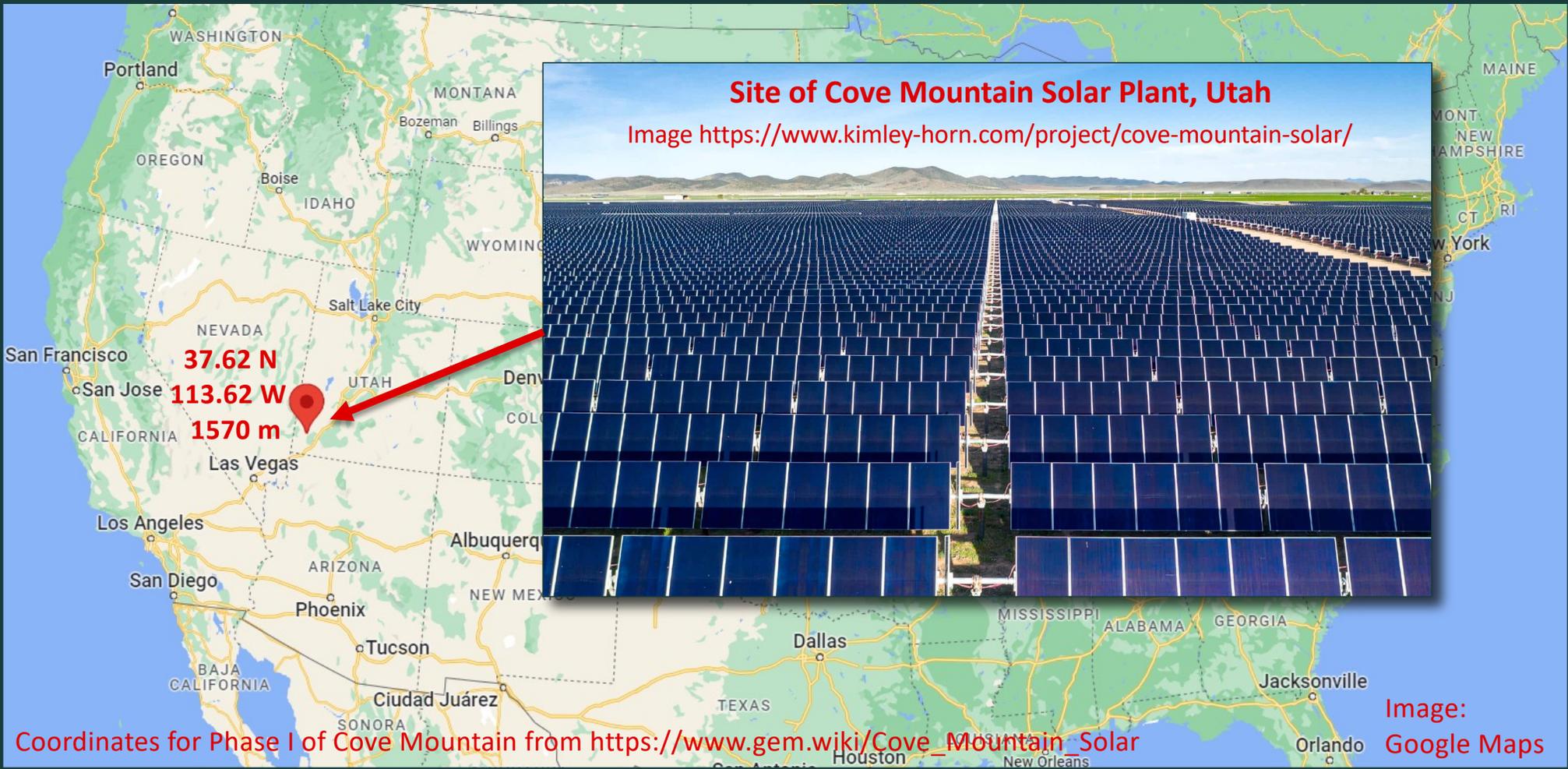
315 W

## Three early comments

- This is not an investigation into the accuracy of the models.
- Results specific to chosen examples.
  - Model comparisons will differ for other location, weather, system configurations.
  - Consider these results as a general guide, with more emphasis on CRMSE than MBE.
- By themselves, these results don't promote any model over another.  
The value of a model depends on many things:
  - Accuracy, precision, uncertainty
  - Ease of implementation & determining inputs
  - Acceptance by industry
  - Modelling objective: e.g., annual yield, morning power, structural shading, etc.

# Simulation details

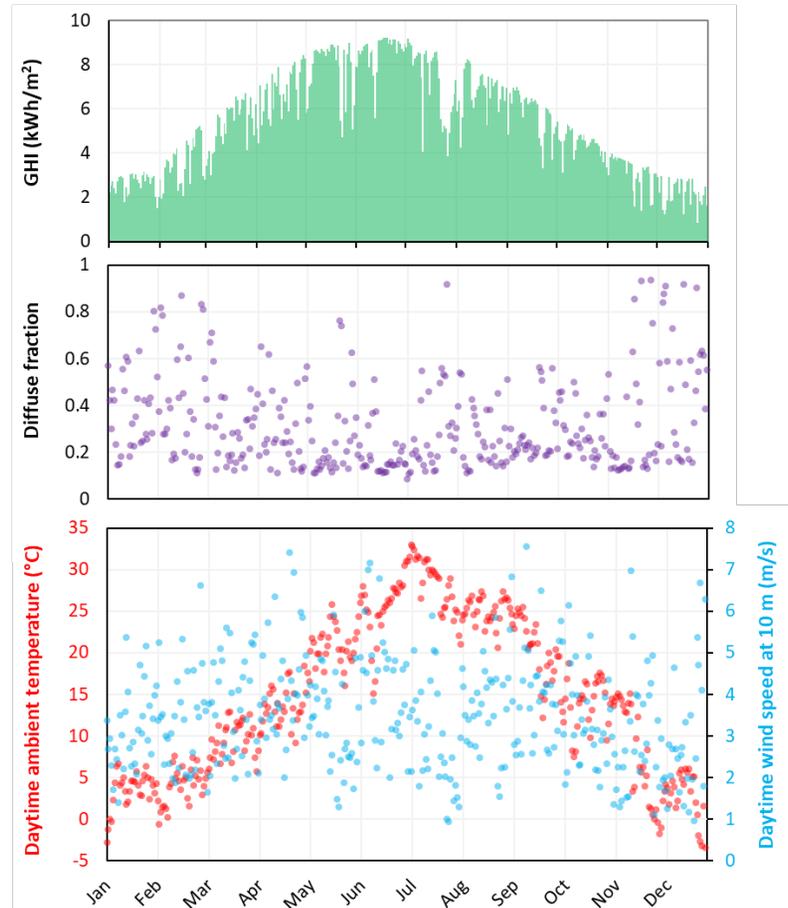
# Simulation details — site location



# Simulation details — weather



- Good solar resource
- Low cloud
- Cold winter, warm summer
- Mostly light winds



$$I = 1.96 \text{ MWh/m}^2$$

$$f_D = 26.5\%$$

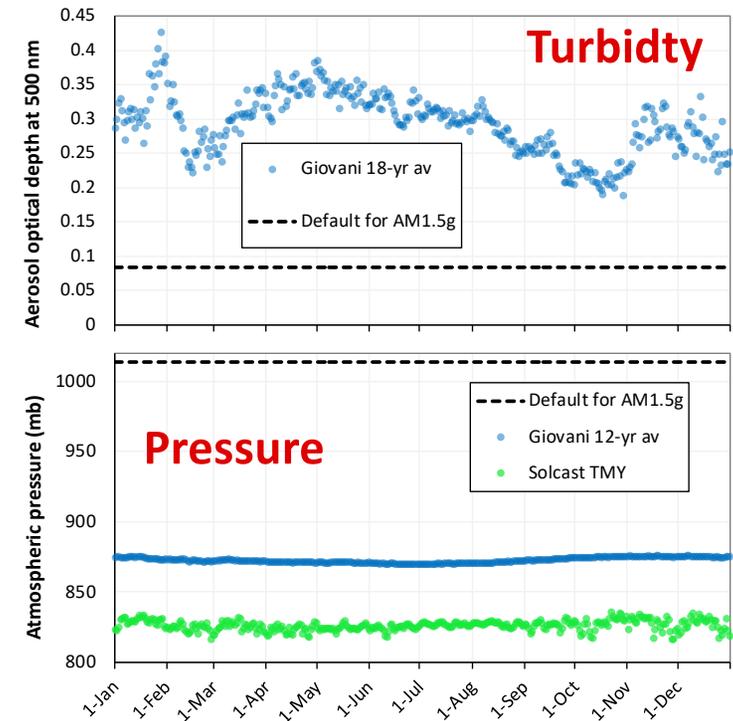
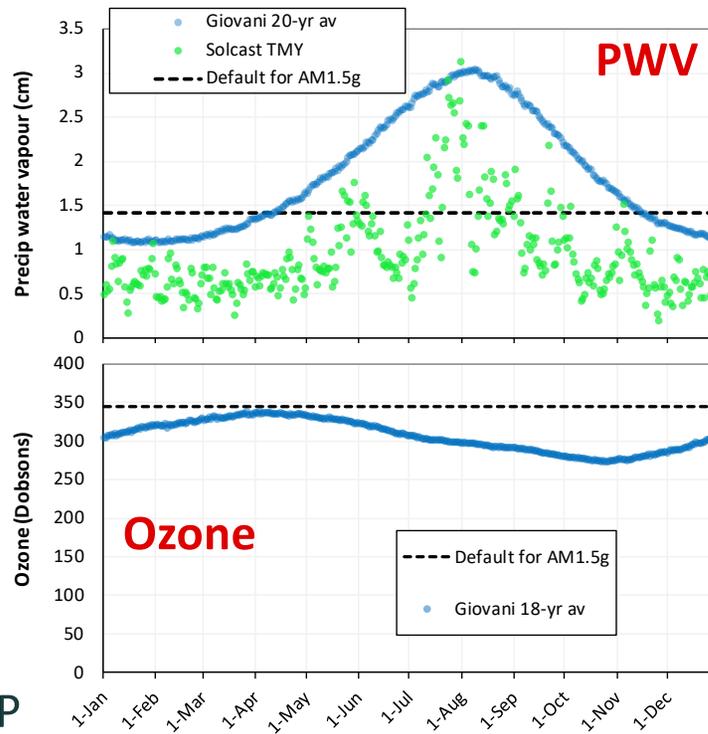
$$T_{av} = 14.7 \text{ }^\circ\text{C}$$

$$w_{av} = 3.5 \text{ m/s}$$

# Simulation details — atmosphere

- Relatively dry
- Dusty
- Moderate ozone
- Low pressure due to altitude (1570 m)

- We use
  - Solcast for PWV & P
  - Giovanni for O<sub>3</sub> and turbidity

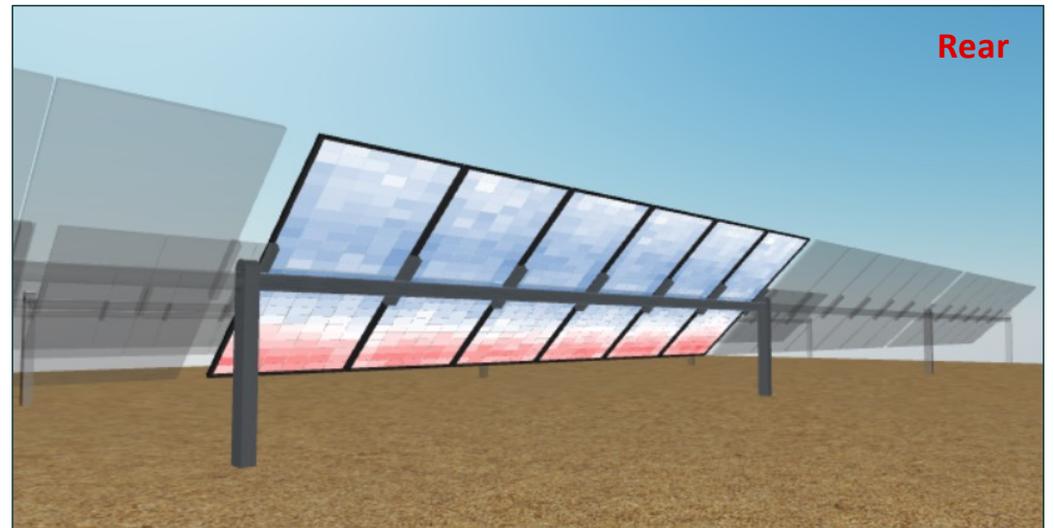
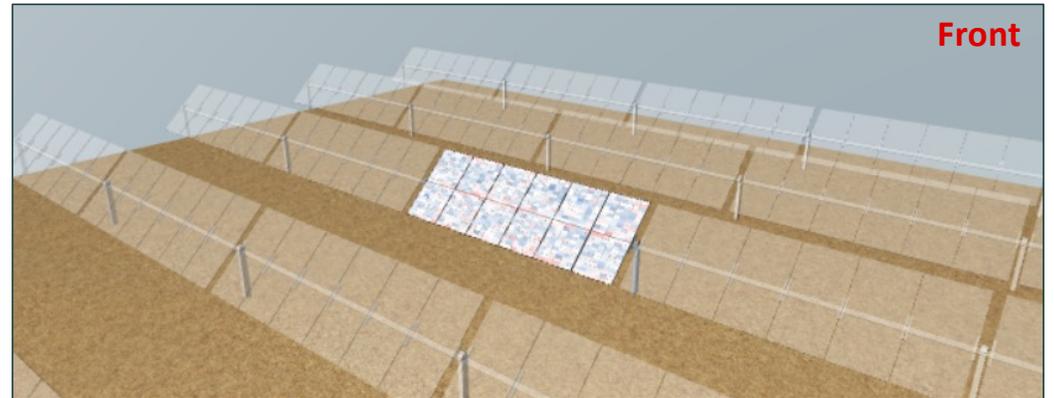


Blue data is long-term daily average from NASA's satellites and analysis of 1° bounding box. <https://giovanni.gsfc.nasa.gov/giovanni>.

Green data is daily average of Solcast, recently acquired by DNV. <https://solcast.com/>

## Simulation details — SAT

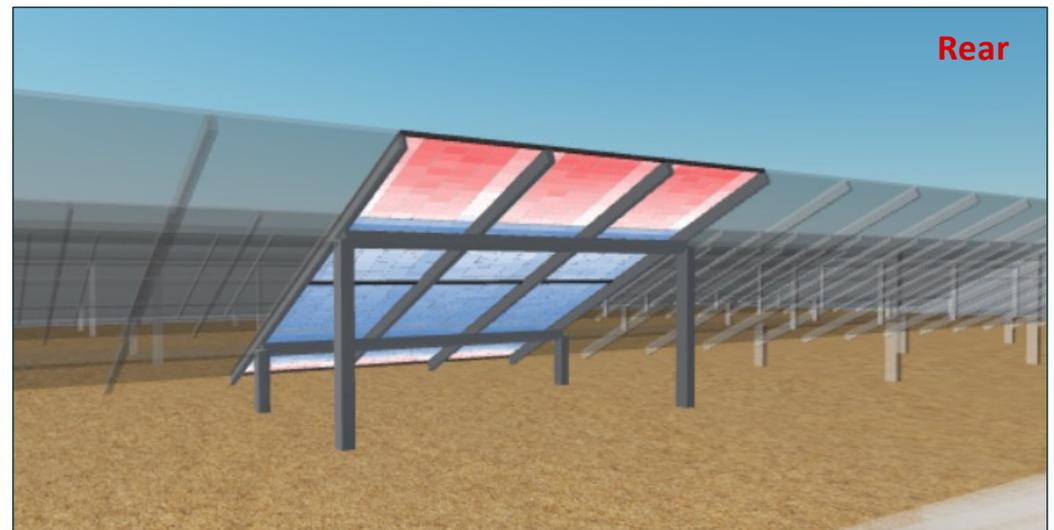
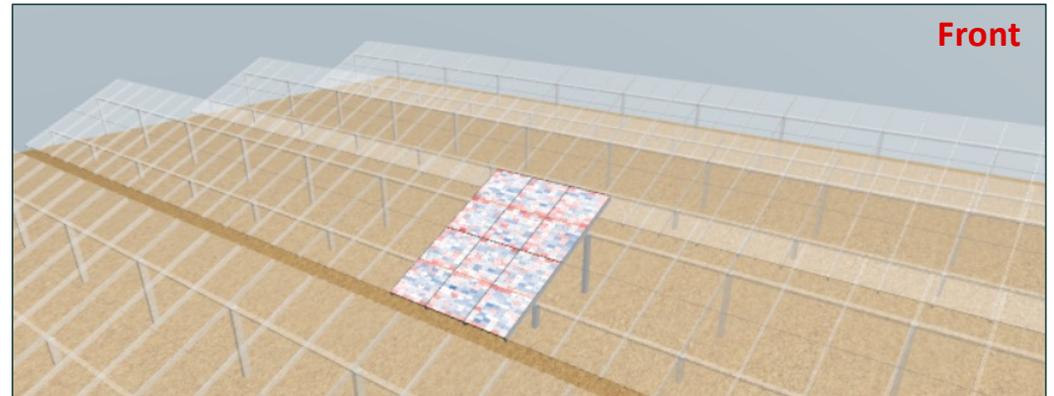
- 1P (one in portrait)
- Six modules per bay
- Posts between bays
- Circular torque tube
- Small clamps (rails)
- Max tilt  $\pm 55^\circ$ , backtracking
  
- Example results of ray tracing for 9 am, 10-May, light cloud.



## Simulation details — fixed-tilt



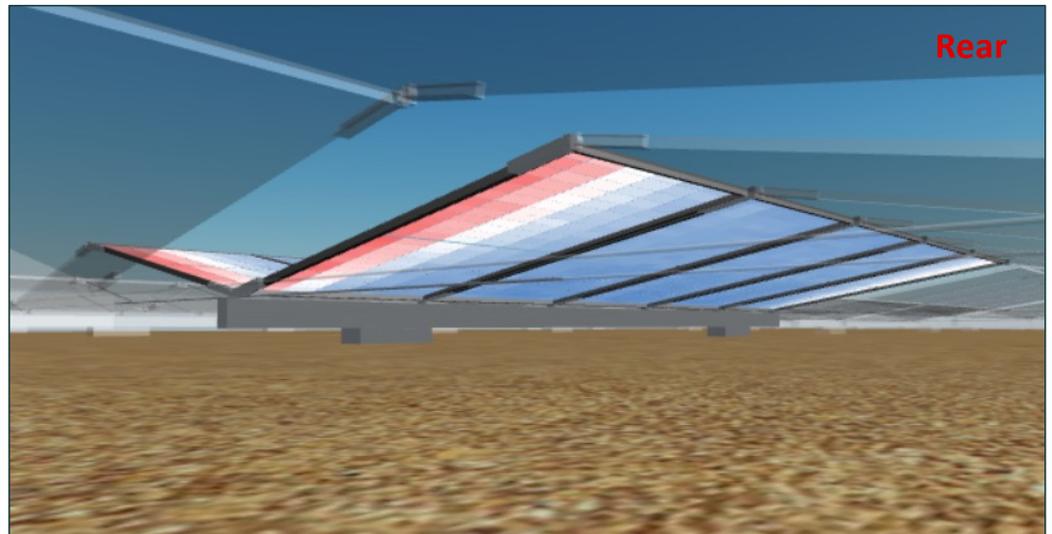
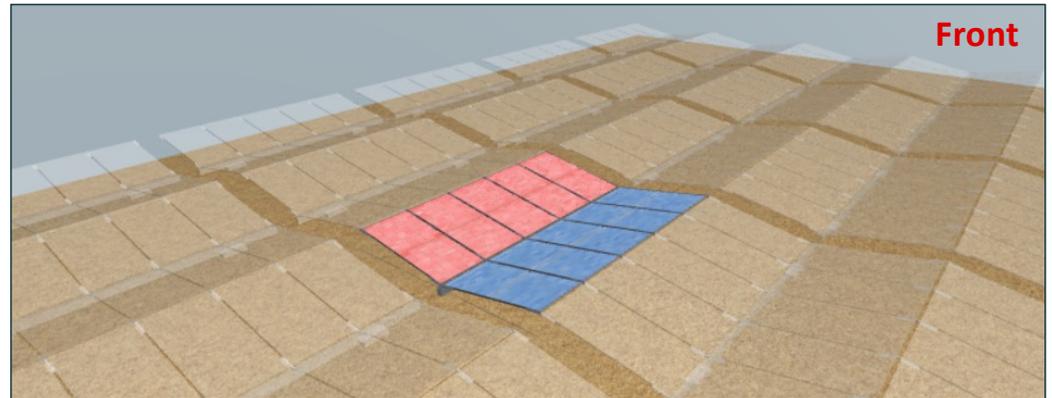
- 2P (two in portrait).
- Six modules per bay
- Posts between bays
- Rafters
- Purlins
- Tilt 25°
  
- Example results of ray tracing for 10 am, 10-May, light cloud.



## Simulation details — waves



- 1P (one in portrait).
- Ten modules per wave.
- Concrete slabs below modules.
- Rafters
- Purlins
- Tilt 10°.
  
- Example results of ray tracing for 9 am, 10-May, light cloud



# Simulation details — module



**P<sub>MP</sub>** 550 W  
**Bifi** 70%

**V<sub>OC</sub>** 49.80 V  
**I<sub>SC</sub>** 13.99 A

**V<sub>MP</sub>** 41.95 V  
**I<sub>MP</sub>** 13.12 A

**FF:** 0.790  
**Eff:** 21.31%



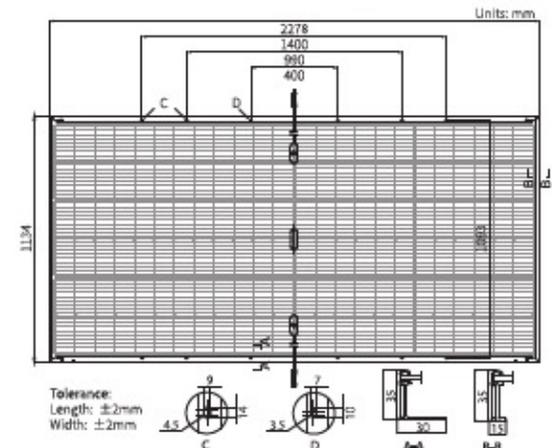
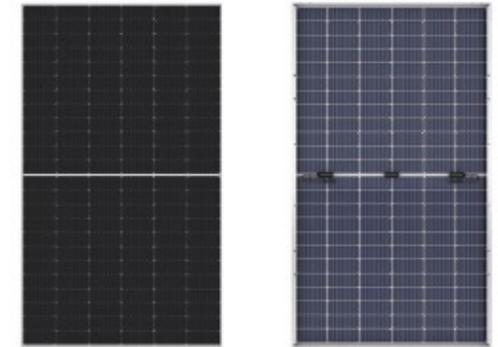
## LONGI LR5-72HBD 550M 144 half-cut cells

### Temperature Ratings (STC)

Temperature Coefficient of I <sub>sc</sub>	+0.050%/°C
Temperature Coefficient of Voc	-0.265%/°C
Temperature Coefficient of P <sub>max</sub>	-0.340%/°C

### Mechanical Parameters

Cell Orientation	144 (6×24)
Junction Box	IP68, three diodes
Output Cable	4mm <sup>2</sup> , +400, -200mm/±1400mm length can be customized
Glass	Dual glass, 2.0+2.0mm heat strengthened glass
Frame	Anodized aluminum alloy frame
Weight	32.6kg
Dimension	2278×1134×35mm
Packaging	31pcs per pallet / 155pcs per 20' GP / 620pcs per 40' HC



## Simulation details — general



- Infinitely large system — no edge effects from system perimeter.
- DC module output — average of all modules in a bay.
- 1 hourly time steps.

# Models examined

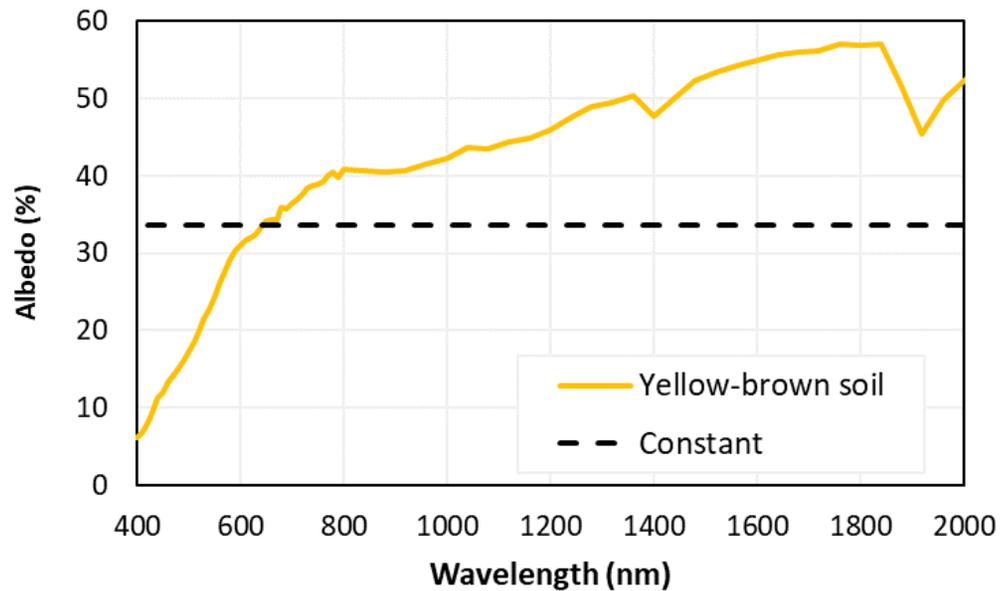
# 1. Spectral albedo

## Conventional

- Constant
- 33.7%

## Advanced

- Wavelength-dependent
- Yellow-brown soil (NASA)



## 2. Electrical mismatch

### Conventional

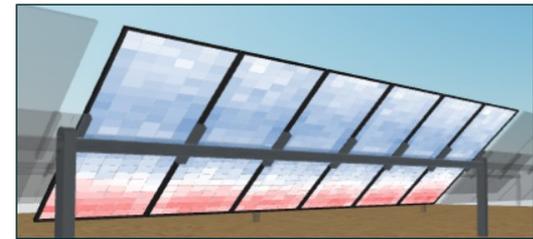
- Constant
  - Here, we use the annual weighted average mismatch loss  $f_M$  as determined by SunSolve (front & rear combined)

	$f_M$
SAT	0.5%
Fixed	0.5%
Waves	0.7%

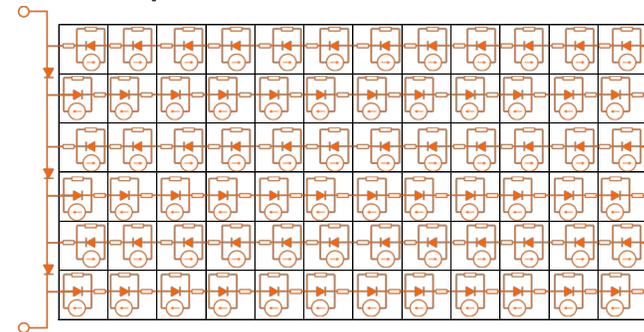
Fixed  $f_M$  omits row-to-row shading of direct light since that is accounted for in PVSystem.

### Advanced

- Calculated at all time steps
  1. Solve  $J_L$  in each cell



2. Solve equivalent-circuit of module



## 3. Solar position



### Conventional

- PVSyst [1]
  - Simple equations.
  - Omits refraction.

### Advanced

- Reda–Andreas 2004 [2]
  - Masses of tables and equations.
  - Accounts for refraction.
  - Zenith and azimuth to within  $\pm 0.0003^\circ$  between 2000 BCE and 6000 CE.

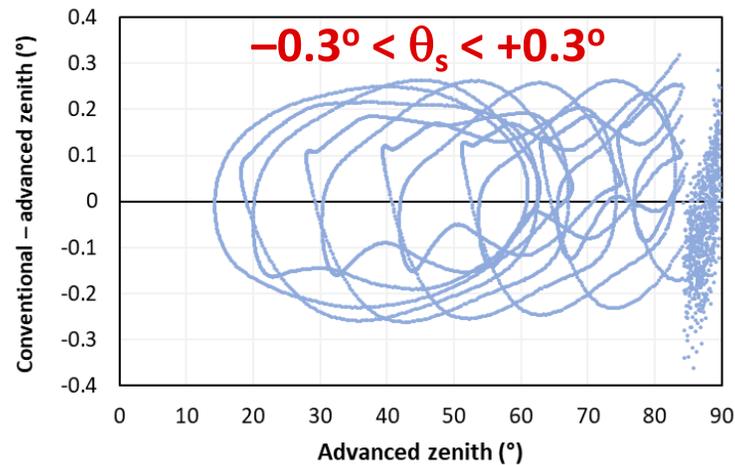
[1] [https://www.pvsyst.com/help/solar\\_geometry.htm](https://www.pvsyst.com/help/solar_geometry.htm)

[2] Reda and Andreas, "Solar position algorithm for solar radiation applications," *Solar Energy* **76** (5), 577–589, 2004.

### 3. Solar position

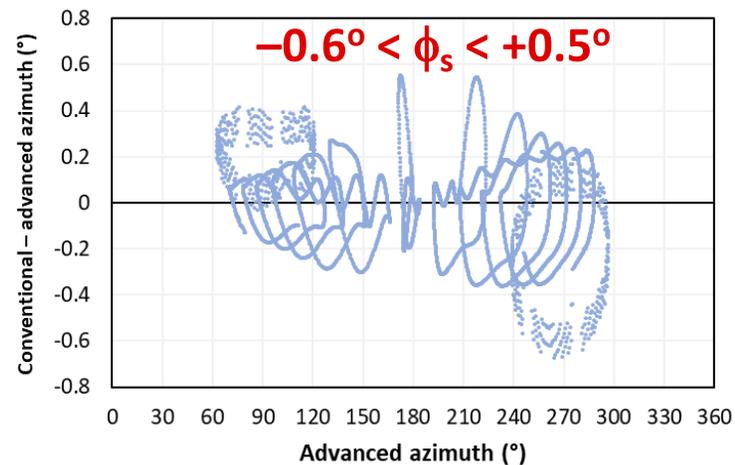
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## 4. Diffuse sky distribution



### Conventional

- PVSyst Perez (1990) [7]

### Alternative implementation

- PVL Perez (1990)

NB: Change in yield when using Hay–Davies [8] rather than Perez in our example:

	<b>Conventional (PVSyst)</b>	<b>Alternative (SunSolve-Yield)</b>
SAT	-1.35%	+0.15%
Fixed	-1.50%	+0.17%
Waves	-0.65%	+0.80%

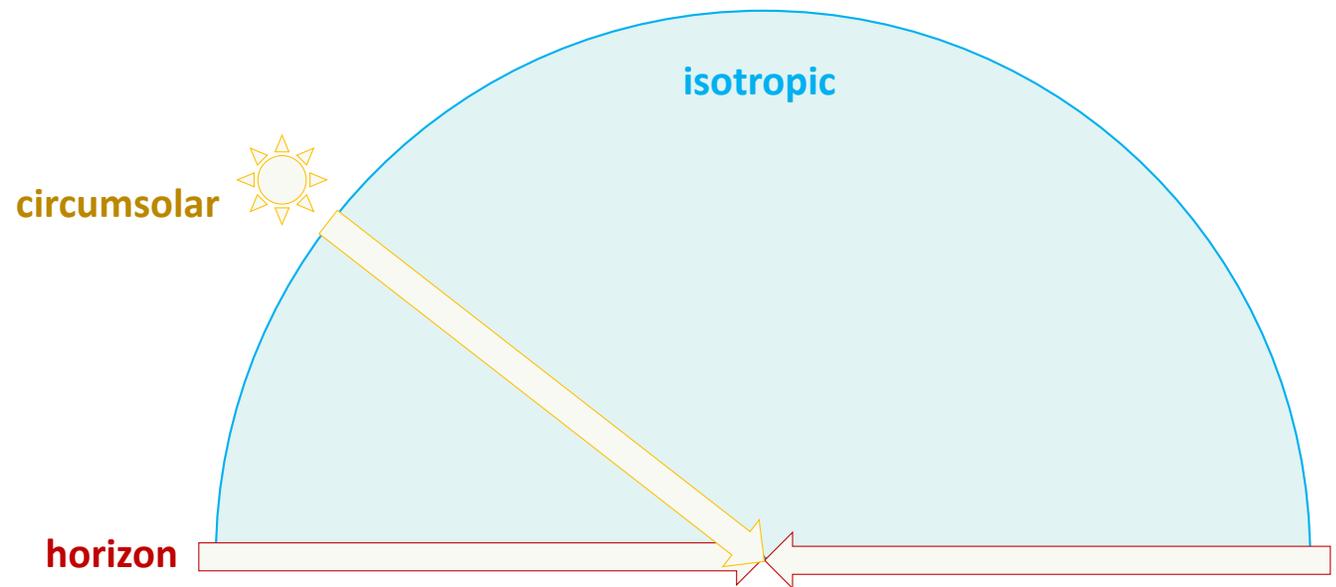
[7] Perez et al., “Modeling daylight availability and irradiance components from direct and global irradiance,” *Solar energy* 44 (5), 271-289, 1990.

[8] Hay and Davies, “Calculation of solar radiation incident on an included surface,” *1st Canadian Solar Radiation Data Workshop*, Ontario, 166, 1980.

## 4. Diffuse sky distribution

Models, like simple Perez (1990), approximate the diffuse light with three sources:

- isotropic
- circumsolar
- horizon

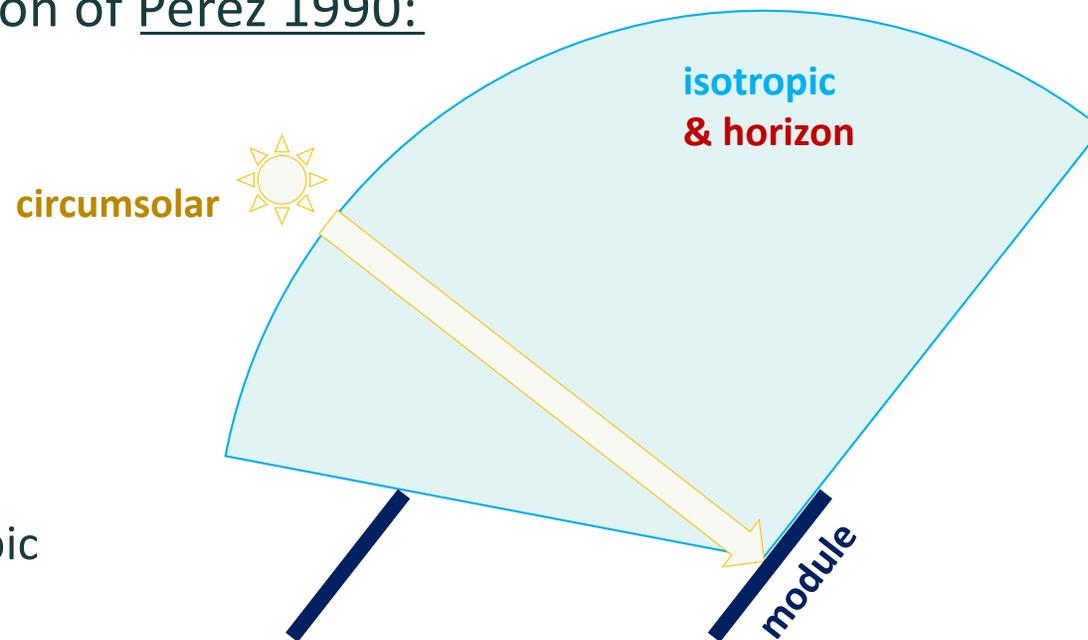


## 4. Diffuse sky distribution

- Adaption for infinite field accounts for shading from modules.

- PVSyst's implementation of Perez 1990:

- isotropic
  - partial shading
- circumsolar
  - possible shading
- horizon
  - same shading as isotropic

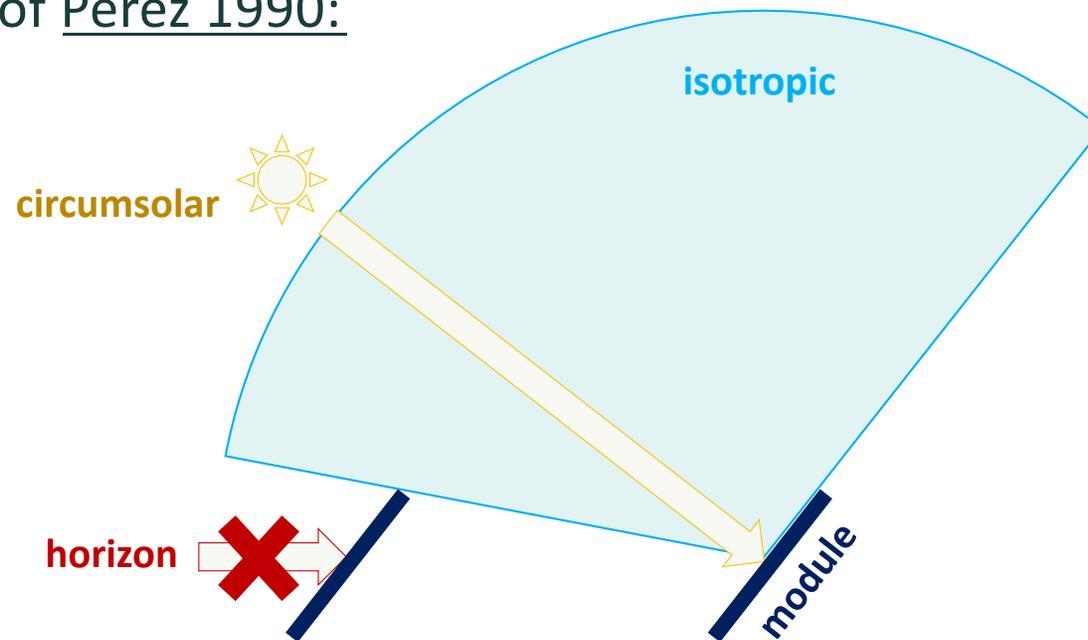


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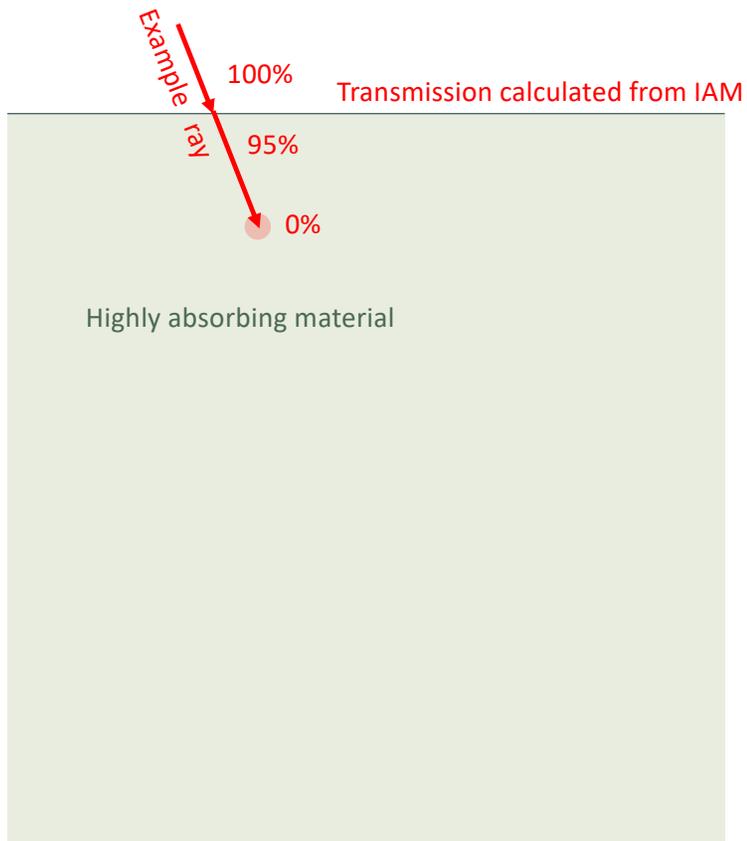
- PVL's implementation of Perez 1990:

- isotropic
  - partial shading
- circumsolar
  - possible shading
- horizon
  - completely shaded

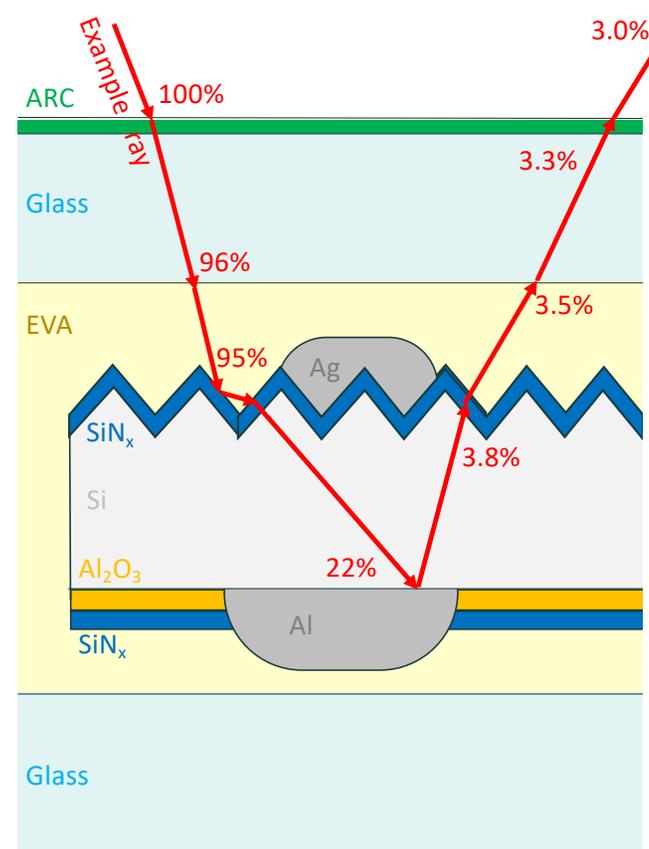


# 5. Module optics

## Conventional



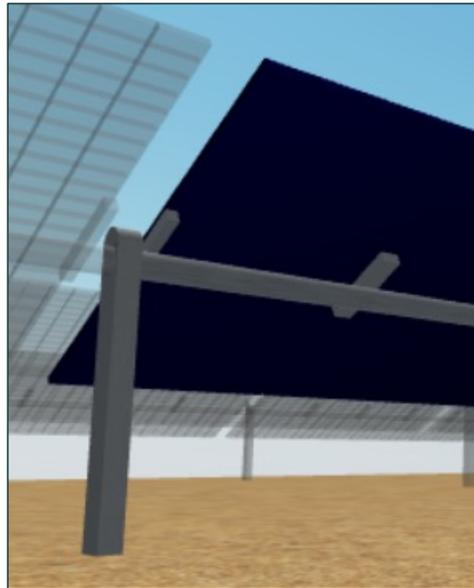
## Advanced



## 5. Module optics

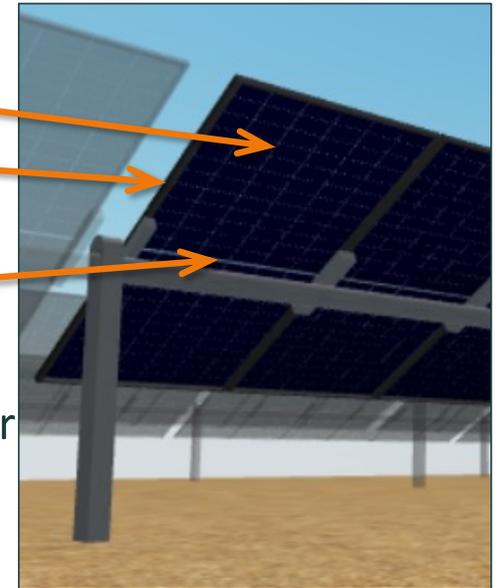
### Conventional

- ‘Simple’ (like PV Syst, SAM, etc.)
  - No reflection
  - IAM from look-up table
  - $\lambda$ -independent
  - No cell spacing
  - No frames
  - Spatially uniform
  
- $J_L$  responds linearly to absorption



### Advanced

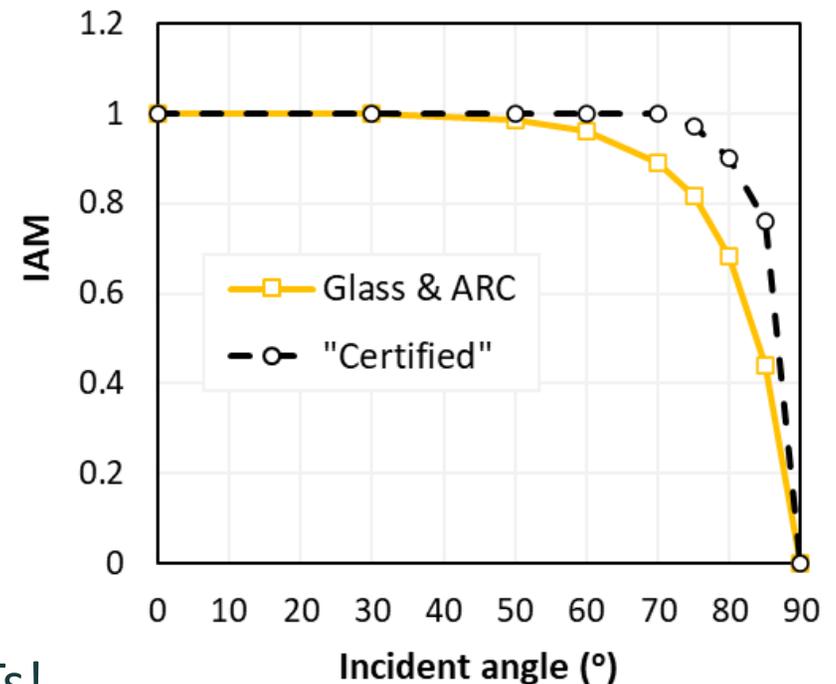
- Ray tracing into the module
  - Reflection
  - Calcs with Fresnel & thin-film optics
  - $\lambda$ -dependent
  - Cell layout
  - Frames
  - Fingers, ribbons, backsheet, pyramids, etc.
  
- $J_L$  responds linearly to absorption



## 5. Module optics

### Conventional – IAM

- PAN files sometimes contain an unrealistic IAM.
- Sometimes it's even “certified”.
- PVSyst allows a calculated IAM instead of PAN IAM
- For conventional, we use calculated IAM, “Fresnel, AR coating”
- “Certified” gives 1.45% more yield for SATs!

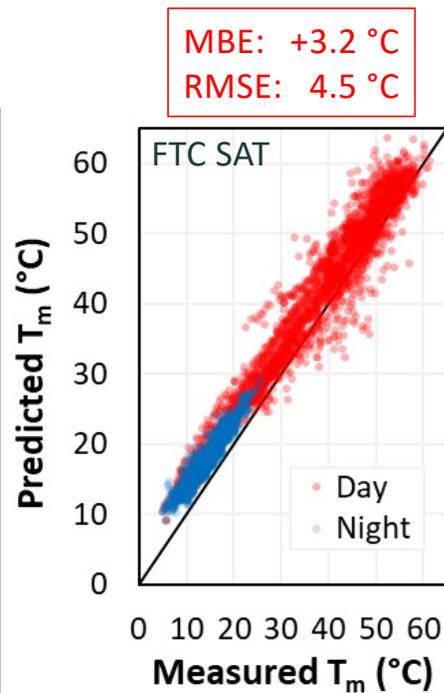


## 6. Thermal model

### Conventional

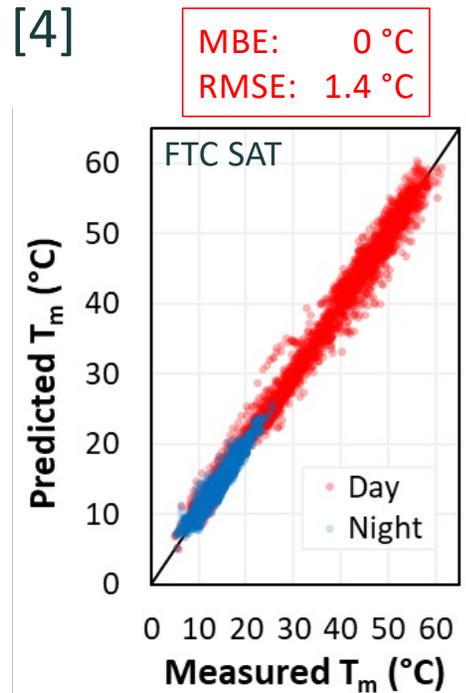
- Faiman [3]

	$U_c$	$U_v$
SAT	25	1.2
Fixed	25	1.2
Waves	27	0



### Advanced

- PVL (PVSC 2022) [4] distinguishes
  - Radiative losses
  - Transient effects
  - Tilt dependence
- Inputs fit to experiment



[3] D. Faiman, "Assessing the outdoor operating temperature of photovoltaic modules," *Progress in Photovoltaics*, 16 (4), 307-315, 2008.

[4] K.R. McIntosh *et al.*, "The influence of wind and module tilt on the operating temperature of single-axis trackers," *49th IEEE PVSC*, 1033-1036, 2022.

## 7. Solar spectra

### Conventional

- AM1.5g

### Advanced

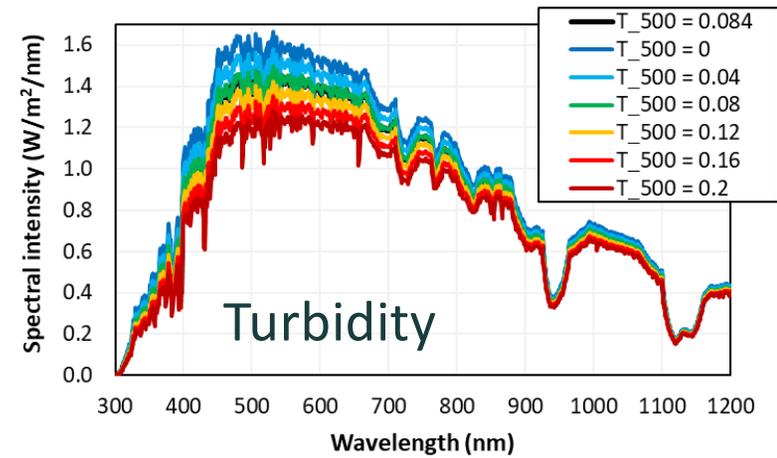
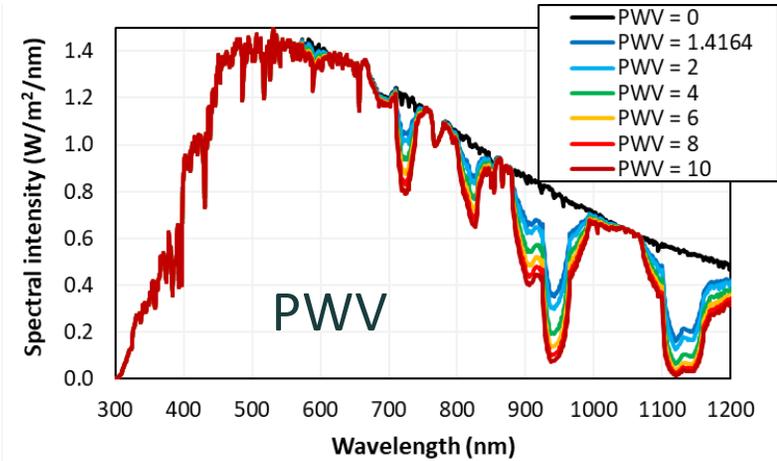
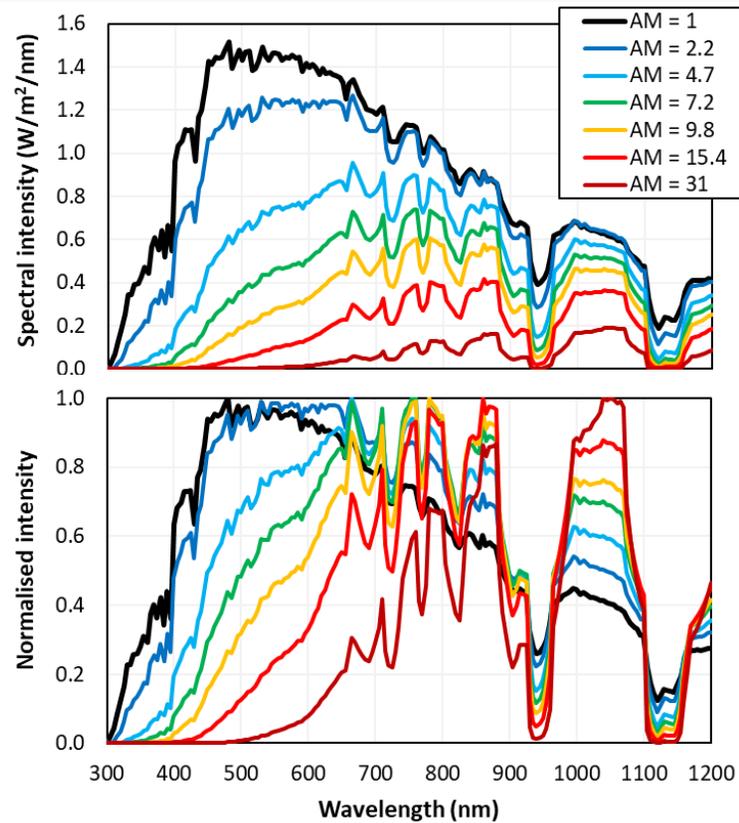
- Calculated at all time steps
  - SPECTRL2 for clear skies [5]
  - Ernst modification for cloudy skies [6]
- Affected by
  - Air mass (i.e., solar location)
  - Precipitable water vapour
  - Turbidity
  - Ozone
  - Air pressure
  - Far-field albedo

[5] Bird and Riordon, "Simple solar spectral model for direct and diffuse irradiance..." *Journal of Climate and Applied Metrology*, **25**, 87–97, 1986.

[6] M. Ernst, et al. "SUNCALCULATOR: A program to calculate the angular and spectral..." *Solar Energy Materials and Solar Cells*, **157** 913–922, 2016.

# 7. Solar spectra

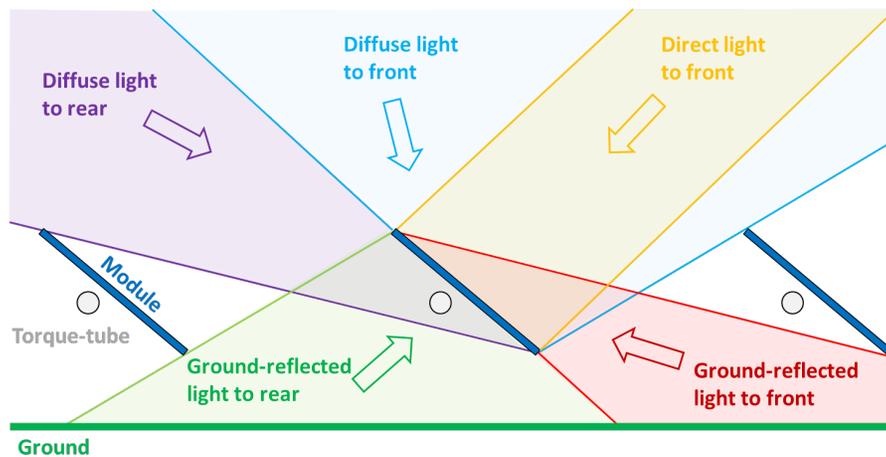
## Air mass



## 8. System optics

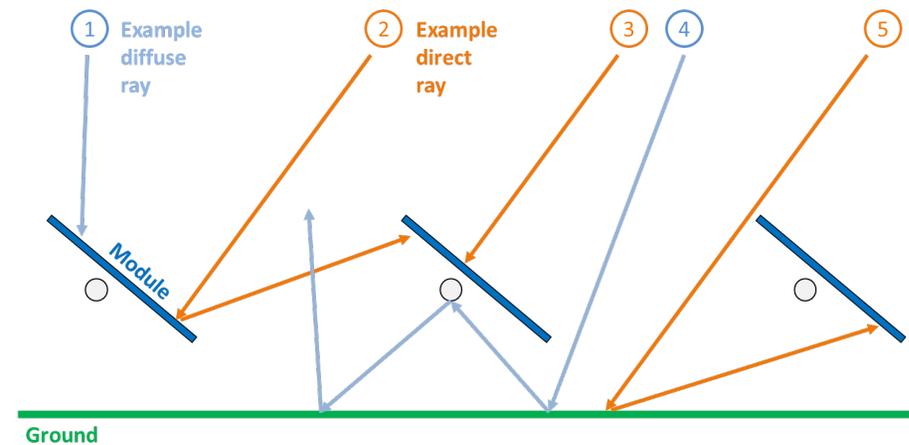
### Conventional

- View-factors & bifacial loss factors
  - Structural shading,  $f_s$
  - Transmission,  $f_T$



### Advanced

- Ray tracing



## 8. System optics

### Conventional

- View-factors & bifacial loss factors
  - Structural shading,  $f_s$
  - Transmission,  $f_T$

### Advanced

- Ray tracing

	$f_s$	$f_T$
SAT	9.7%	6.7%
Fixed	19.3%	0.0%
Waves	--	--

## 8. System optics

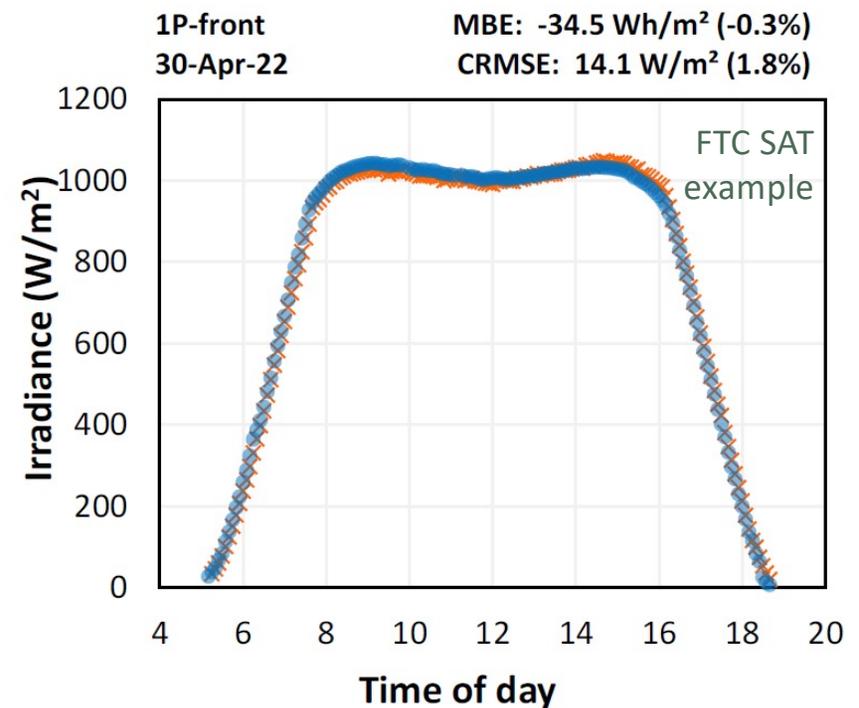
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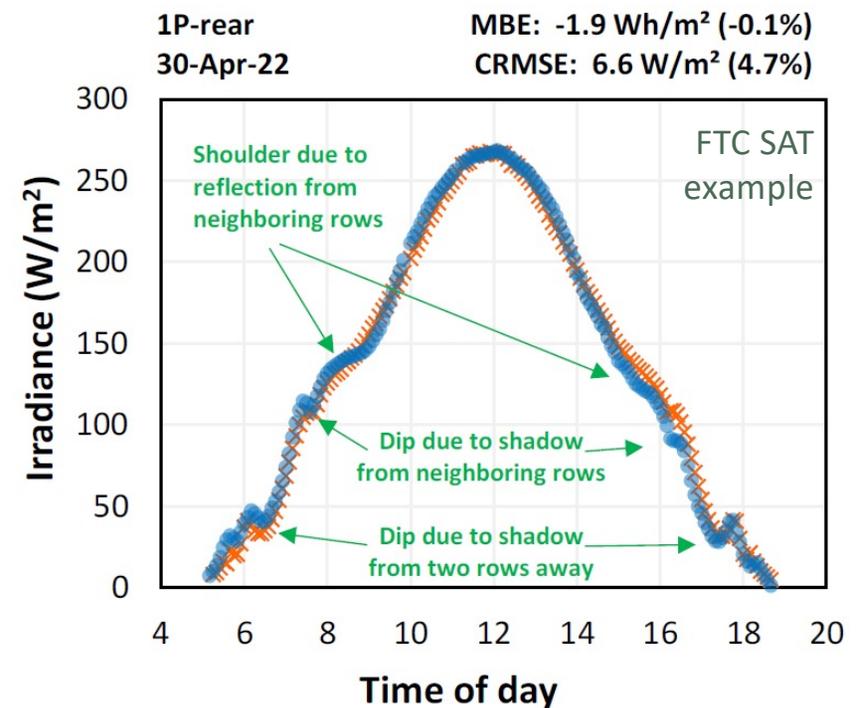
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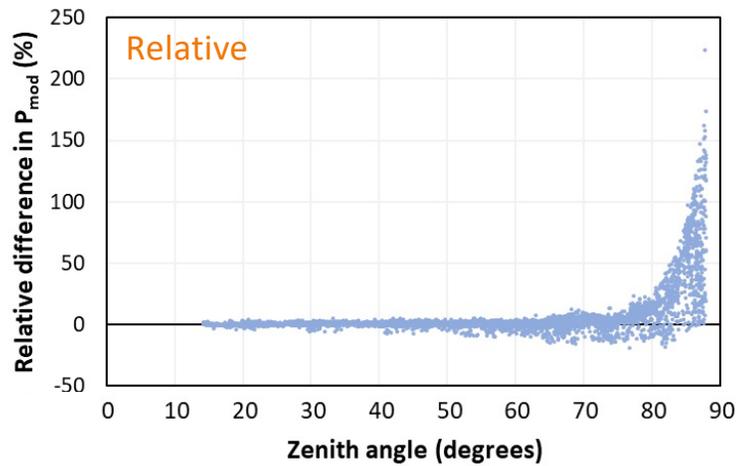
### Advanced

- Ray tracing



## **Detailed results for SATs**

# All mechanisms combined: conventional vs advanced



For 1P SAT at Cove Mt, Utah

MBE: +1.90%

CRMSE: 8.9 W

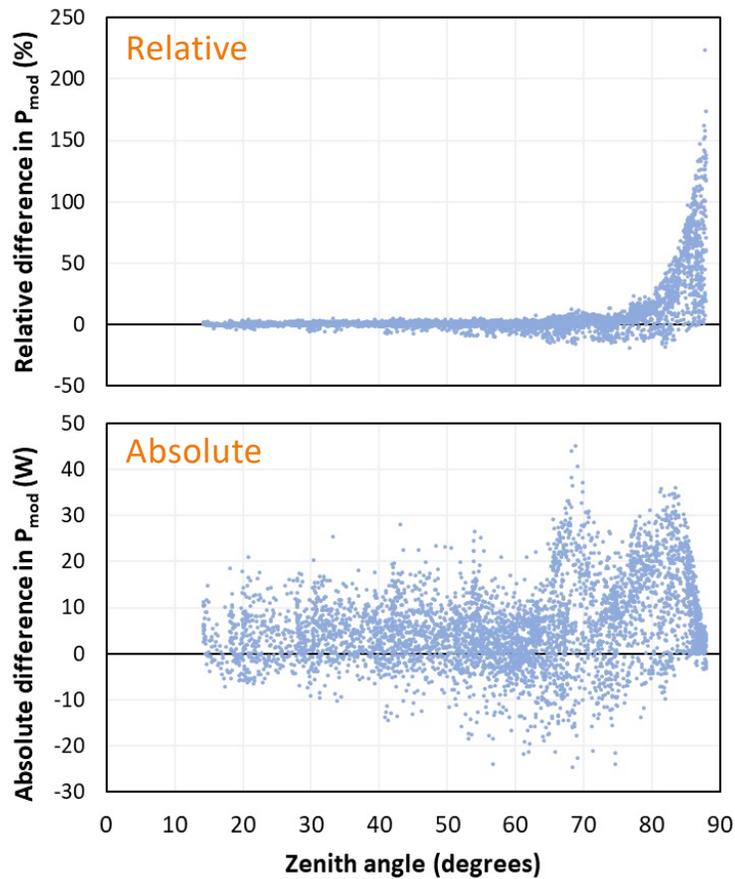
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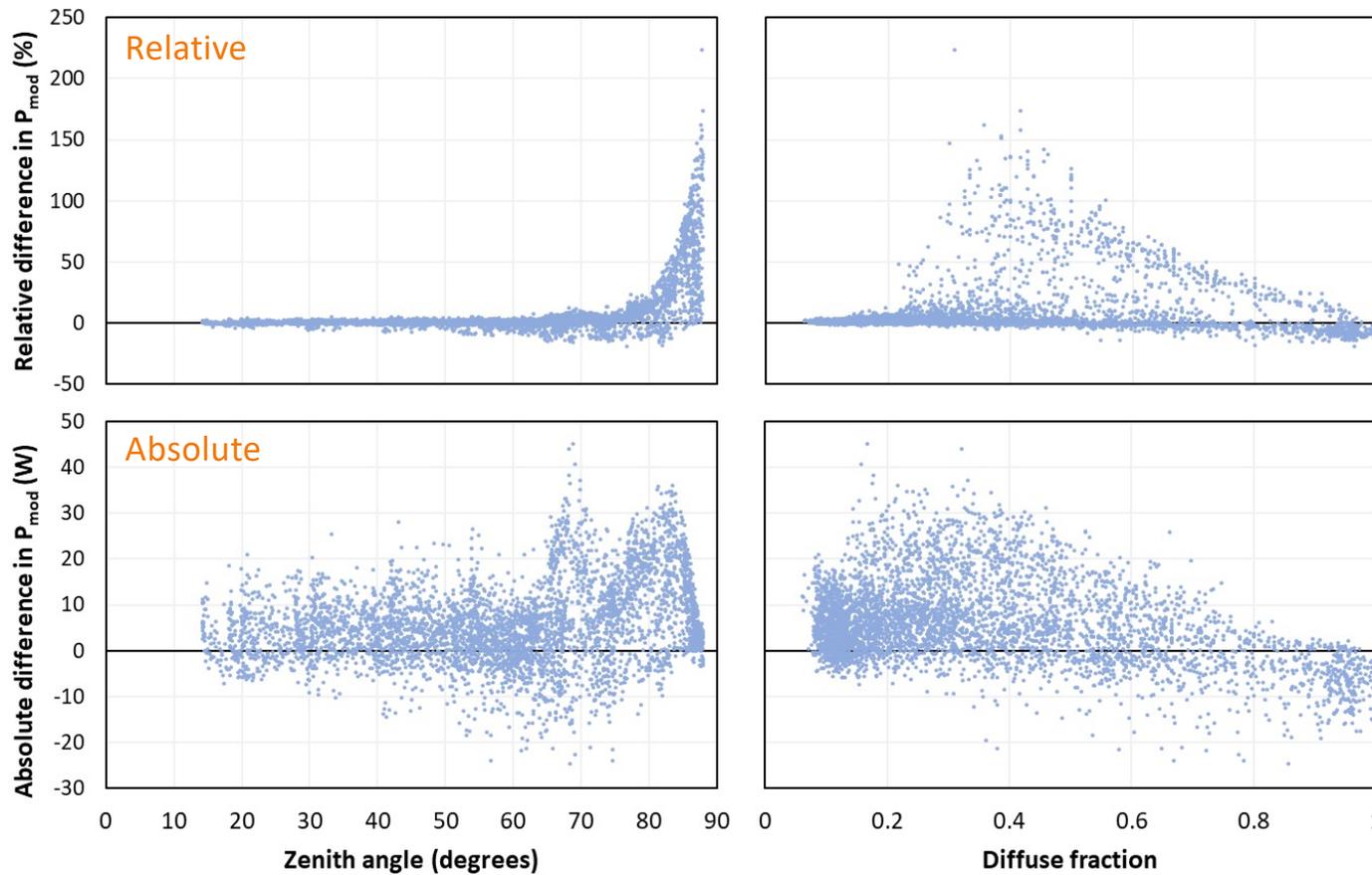
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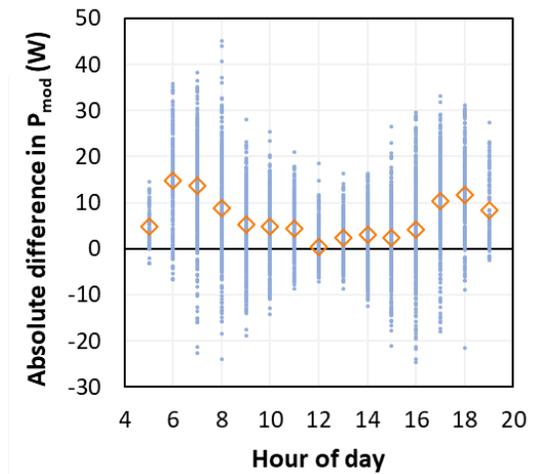
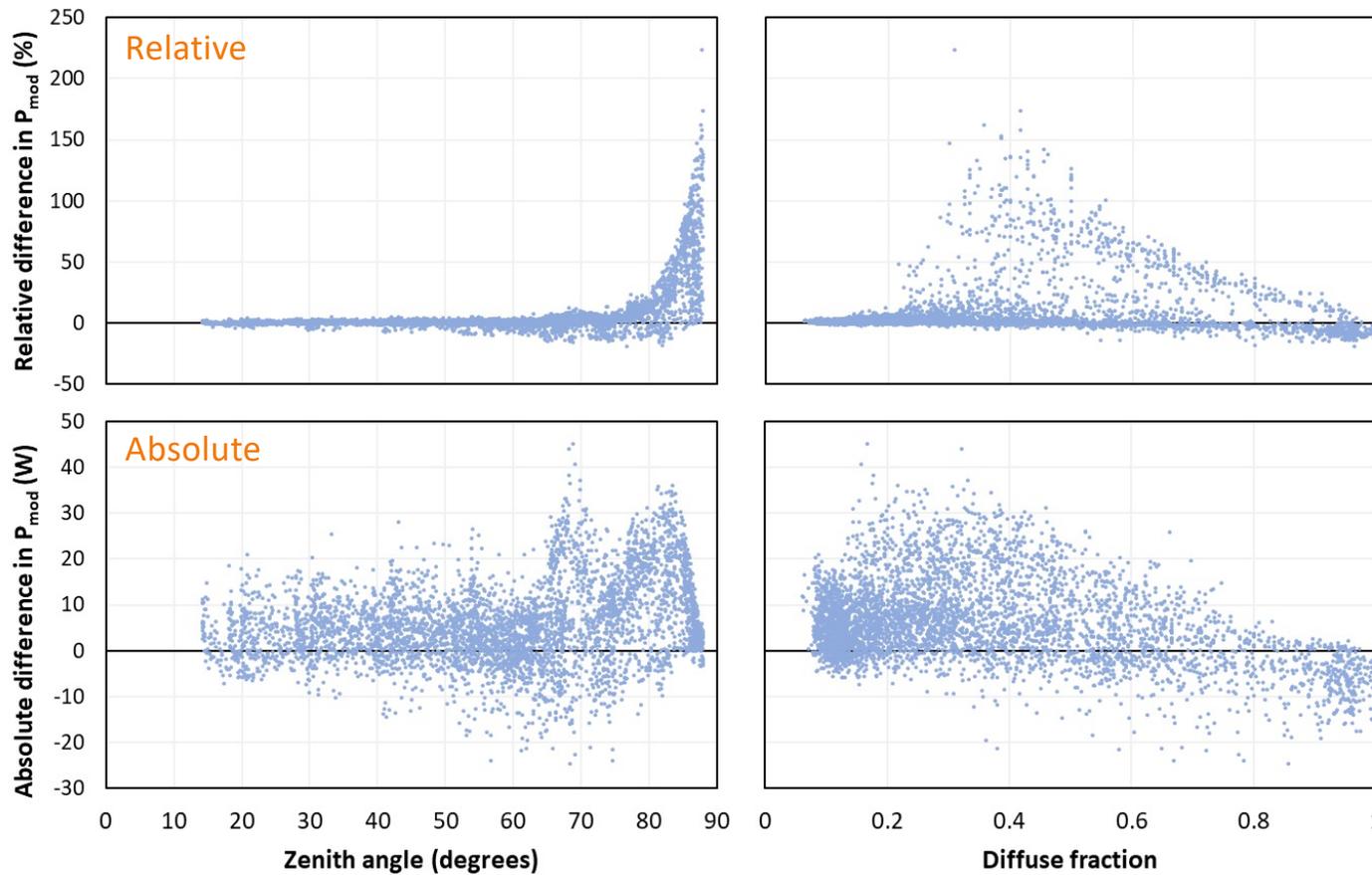
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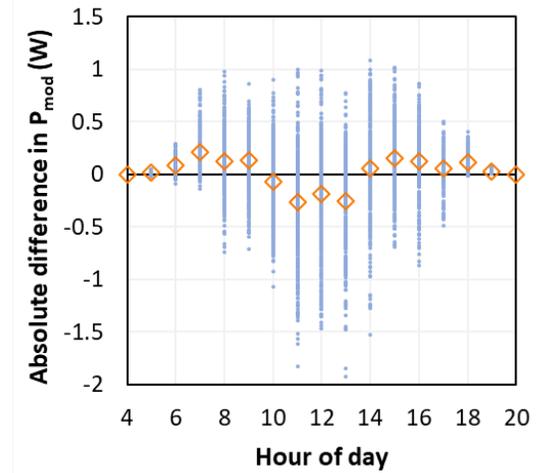
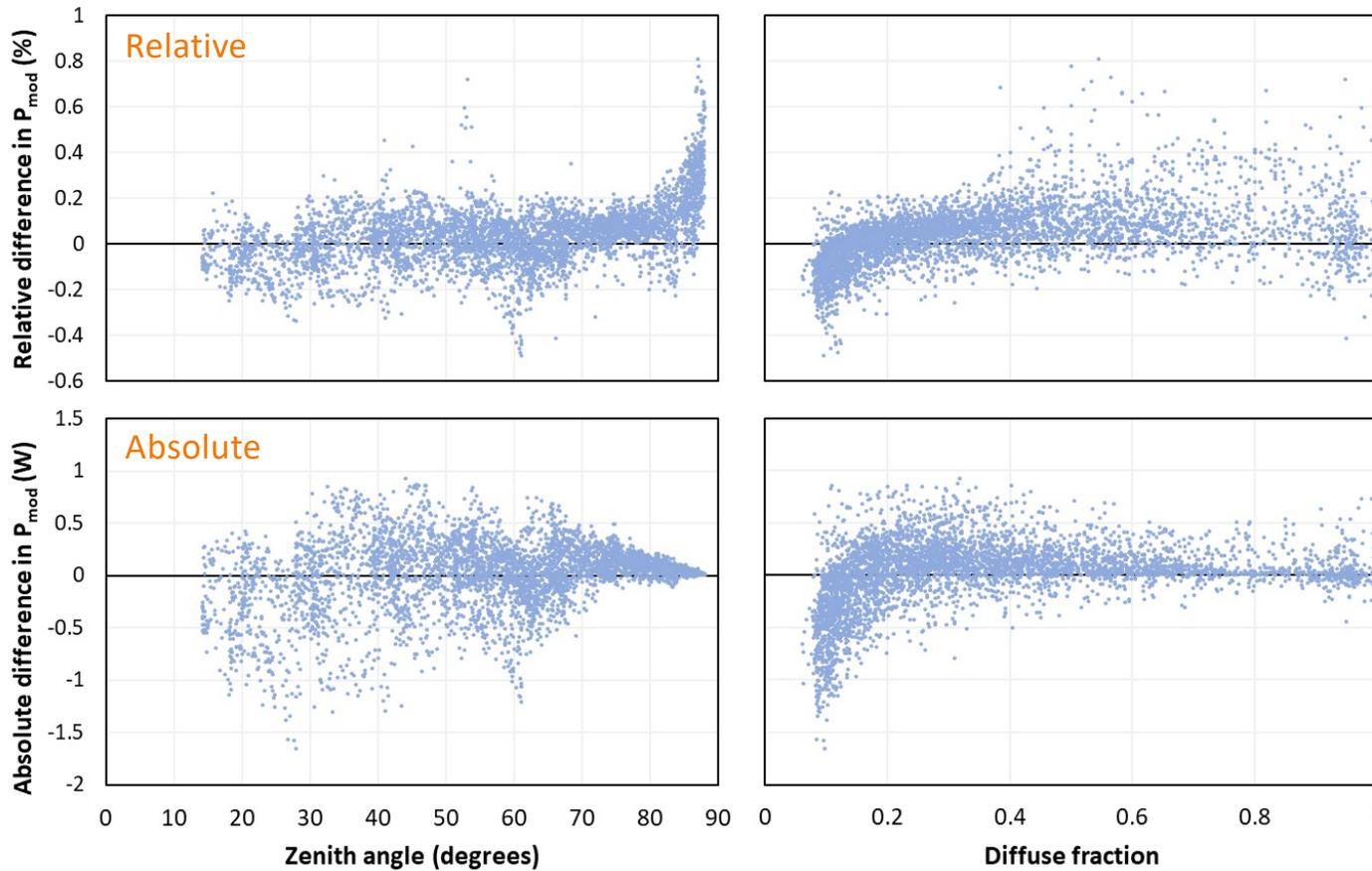
# 1. Albedo: 33.7% vs yellow-brown soil



For 1P SAT at Cove Mt, Utah

MBE: +0.00%

CRMSE: 0.4 W



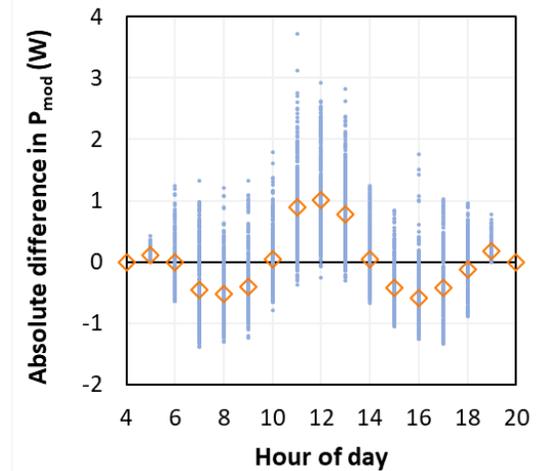
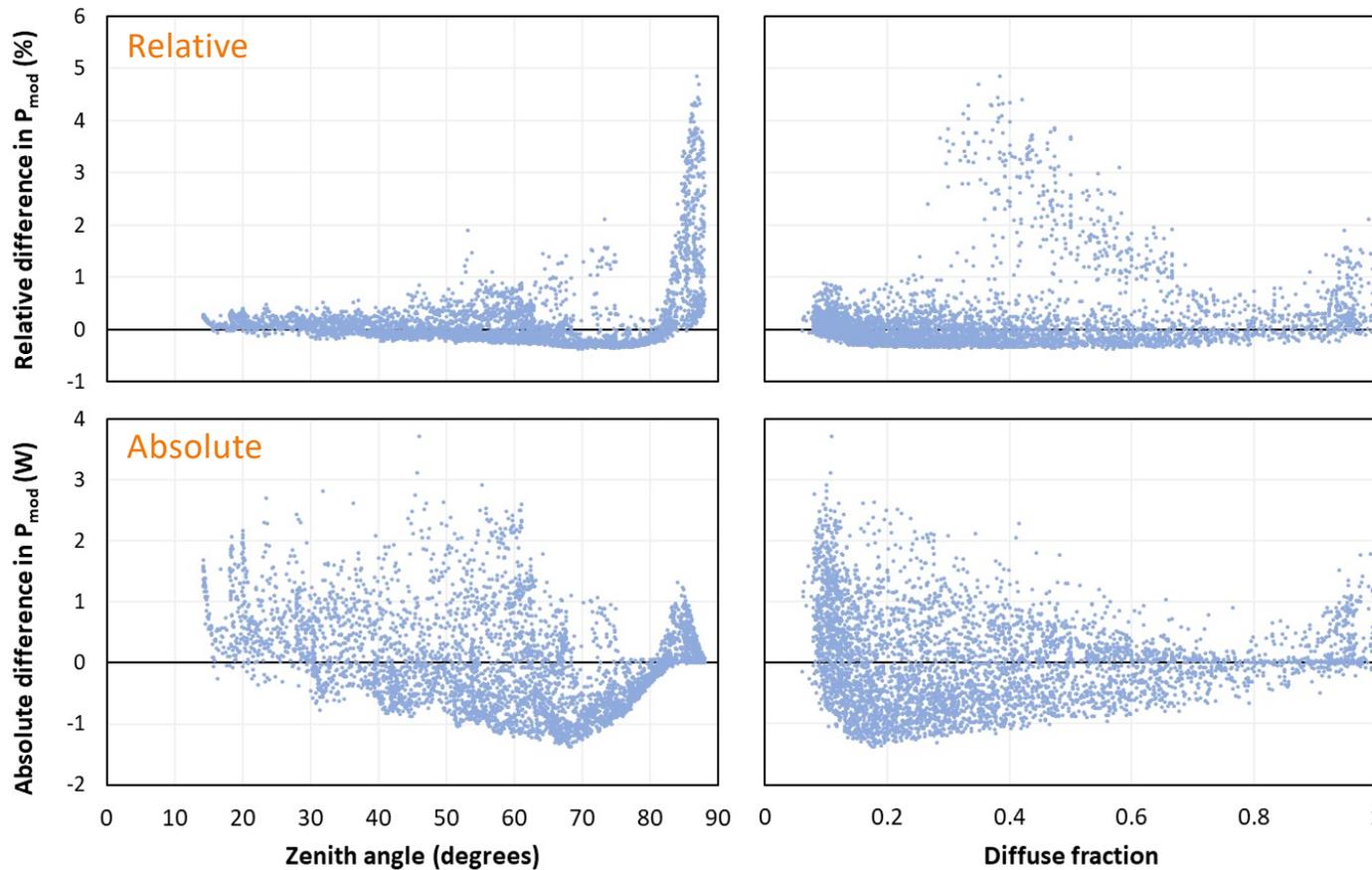
## 2. Cell-to-cell mismatch: constant vs hour-by-hour



For 1P SAT at Cove Mt, Utah

MBE: +0.00%

CRMSE: 0.8 W



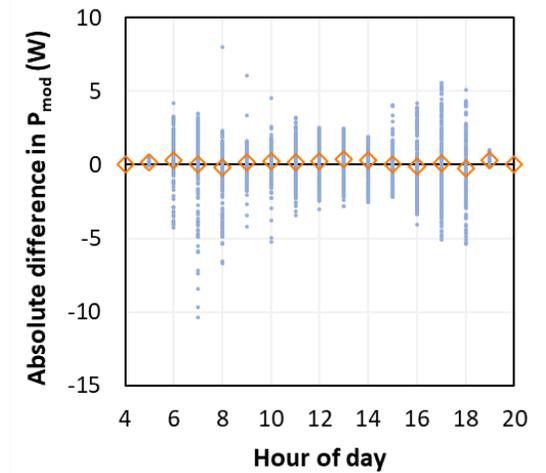
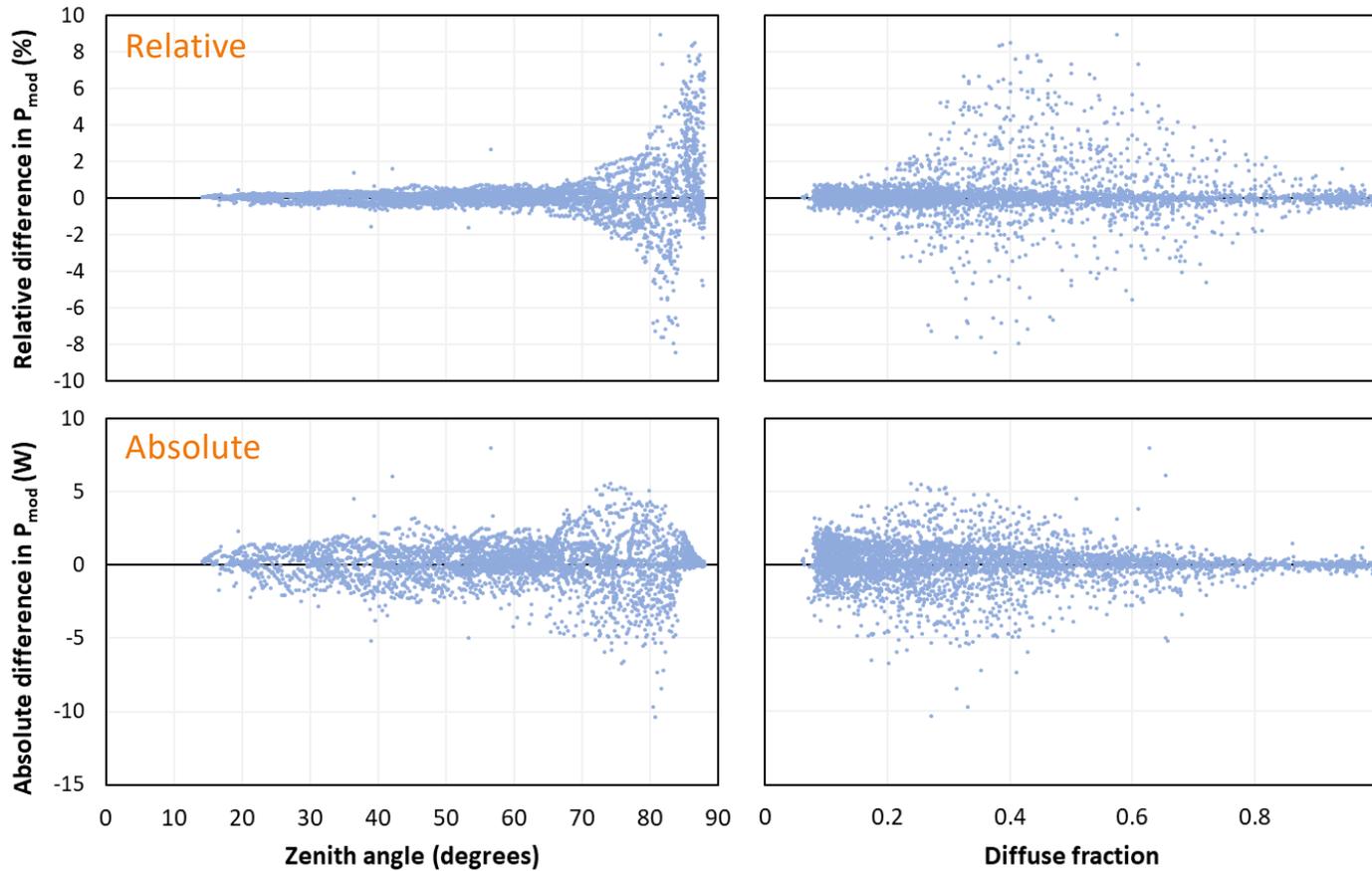
### 3. Solar position: PVSyst algo vs Reda2004



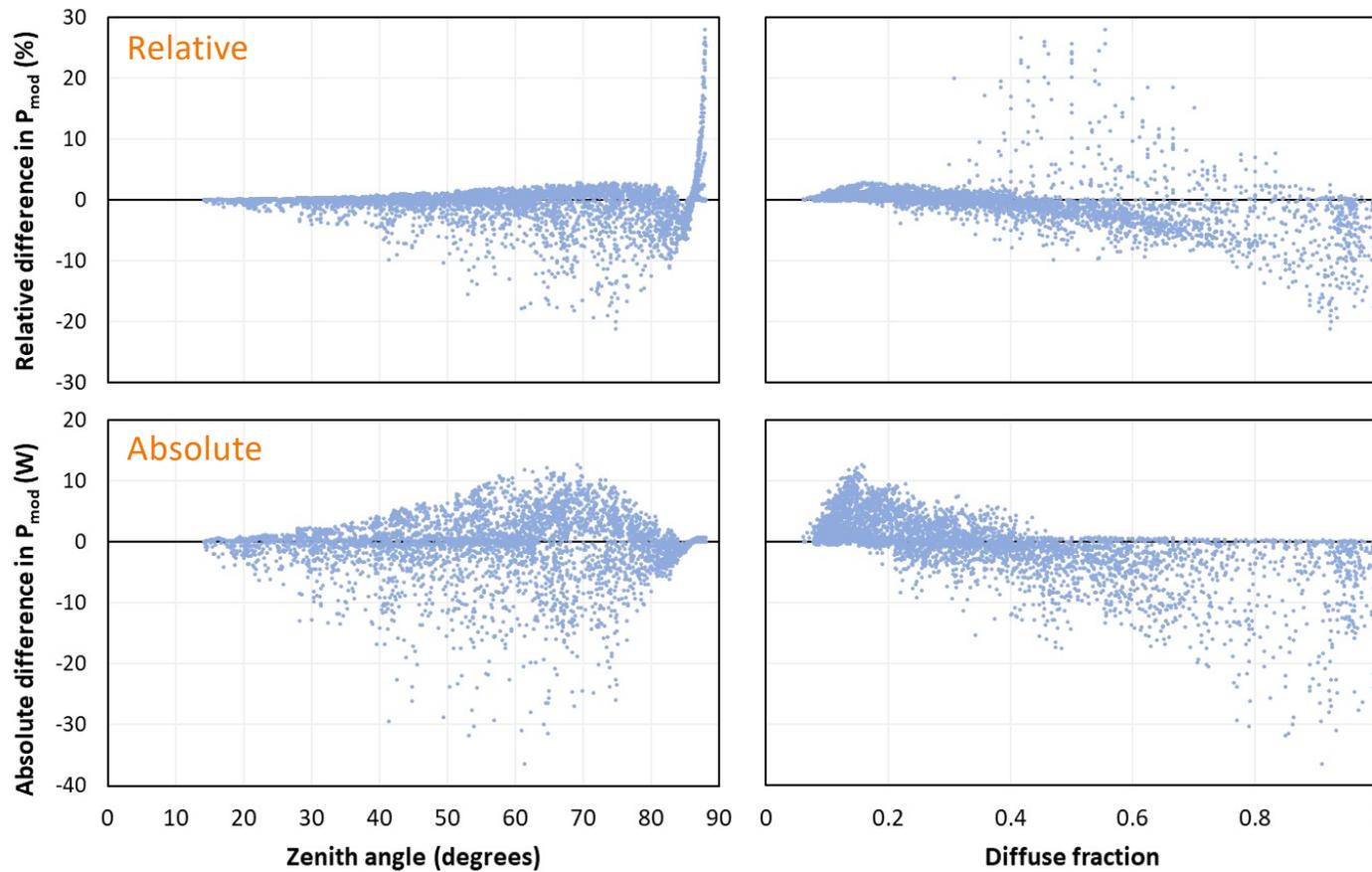
For 1P SAT at Cove Mt, Utah

MBE: +0.04%

CRMSE: 1.4 W



# 4. Sky distribution model: Hay–Davies vs Perez 1990



For 1P SAT at Cove Mt, Utah

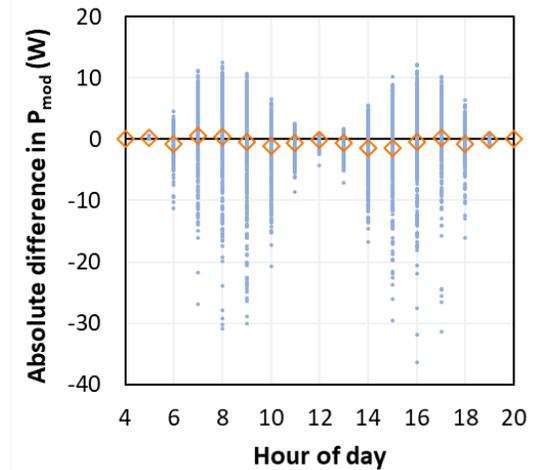
SunSolve  
PVsyst

MBE: -0.15%

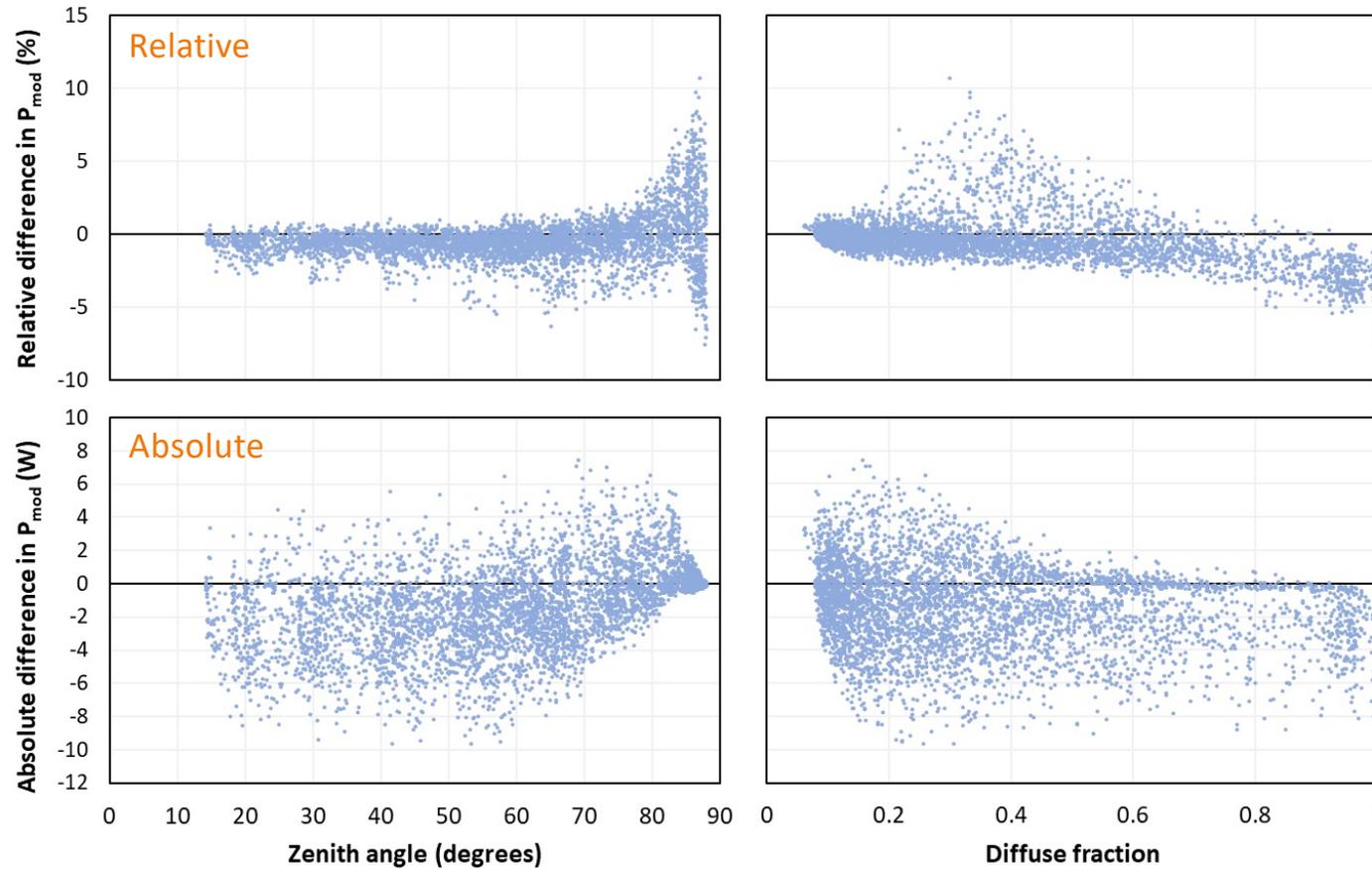
CRMSE: 5.2 W

MBE: +1.35%

CRMSE: 4.9 W



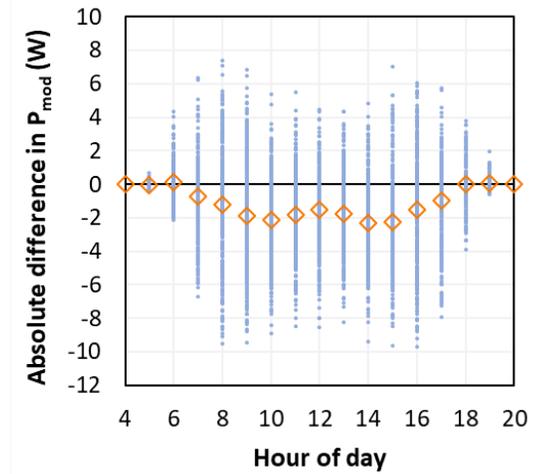
# 5. Module optics: 'simple' vs ray tracing



For 1P SAT at Cove Mt, Utah

MBE: -0.45%

CRMSE: 2.6 W



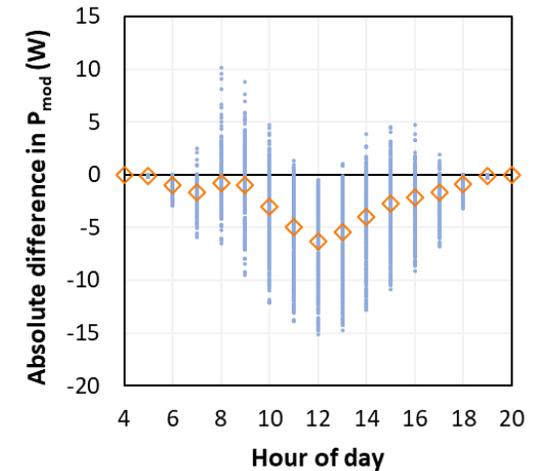
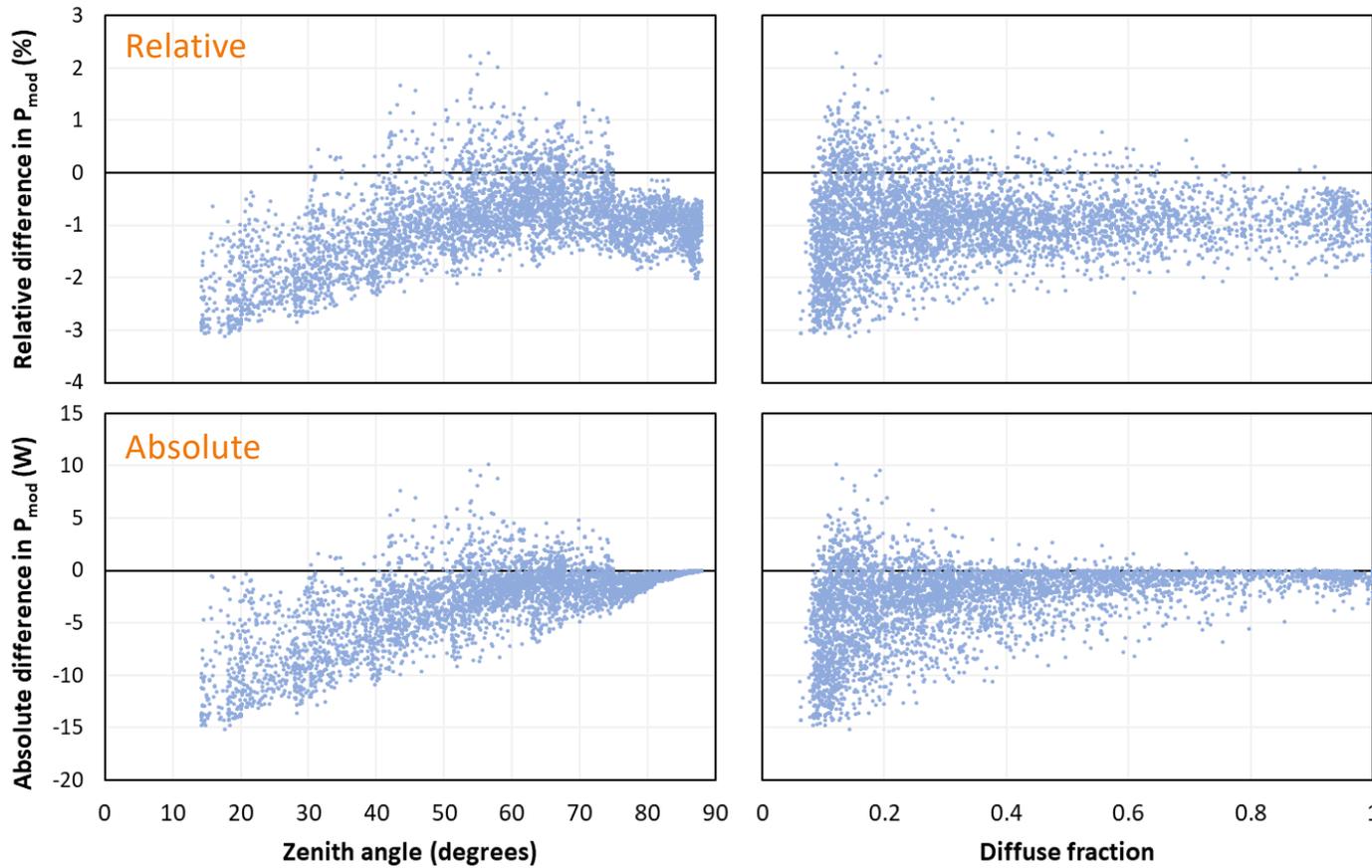
## 6. Thermal: PVL (tuned) vs Faiman (standard inputs)



For 1P SAT at Cove Mt, Utah

MBE: **-1.03%**

CRMSE: **3.5 W**



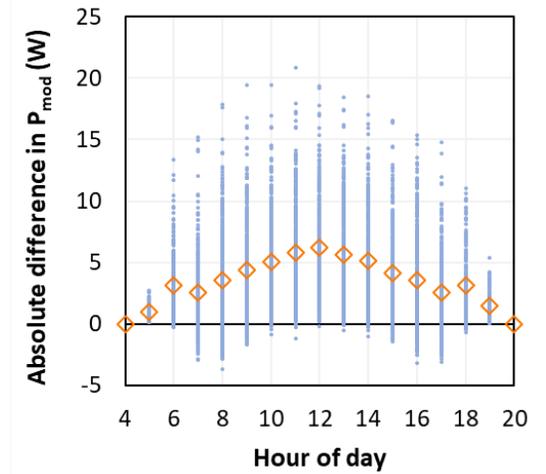
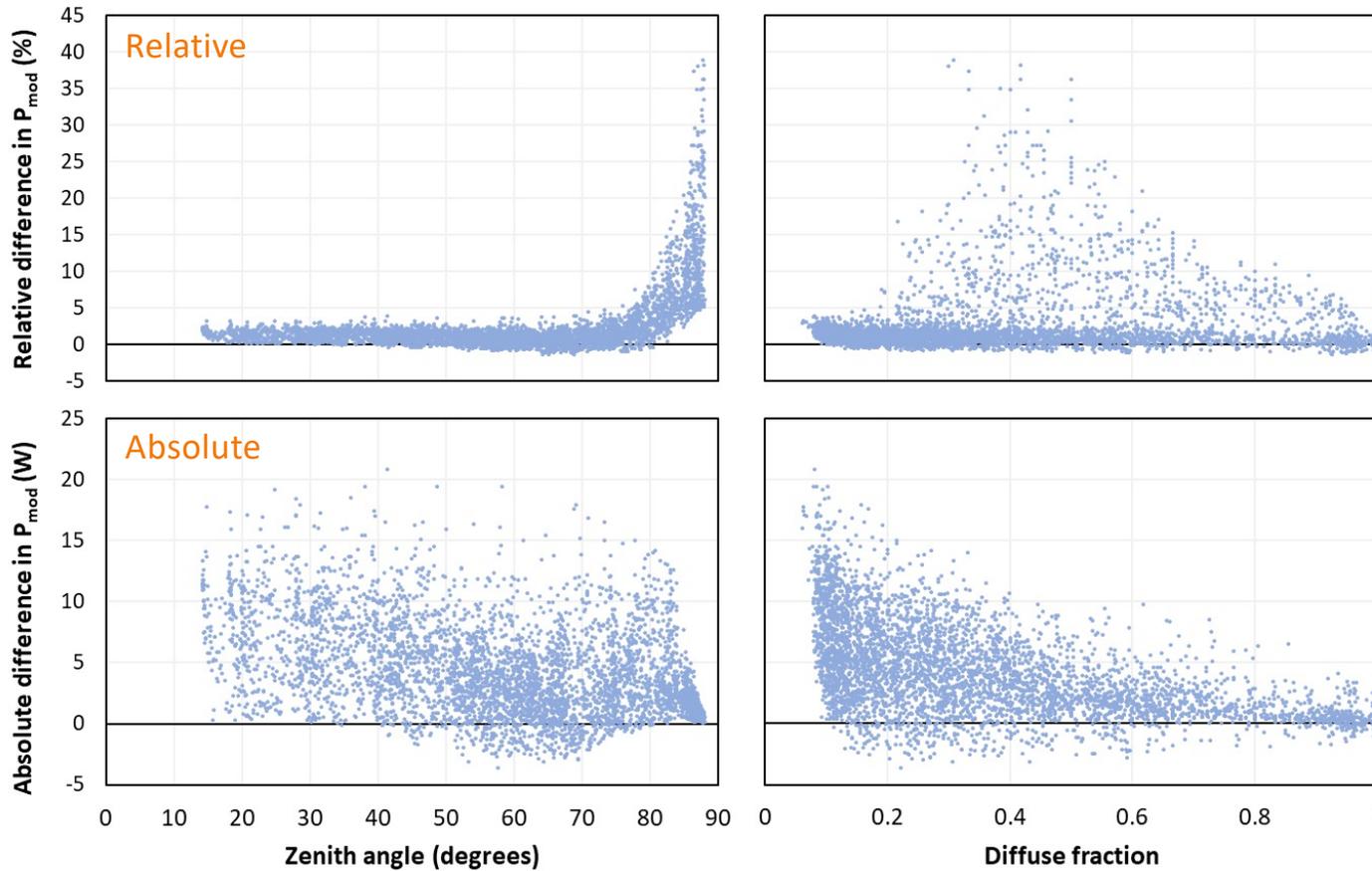
# 7. Solar spectra: AM1.5g vs SPECTRL2



For 1P SAT at Cove Mt, Utah

MBE: +1.34%

CRMSE: 3.8 W



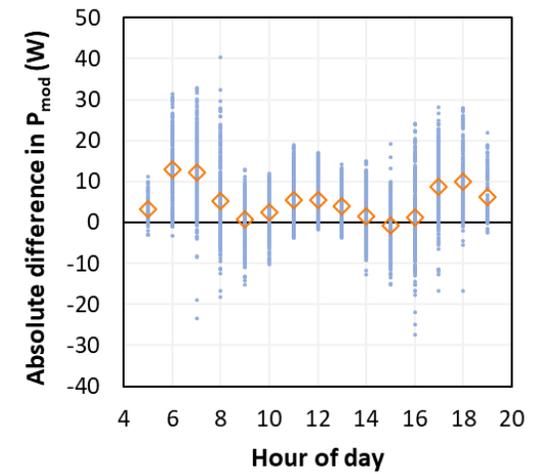
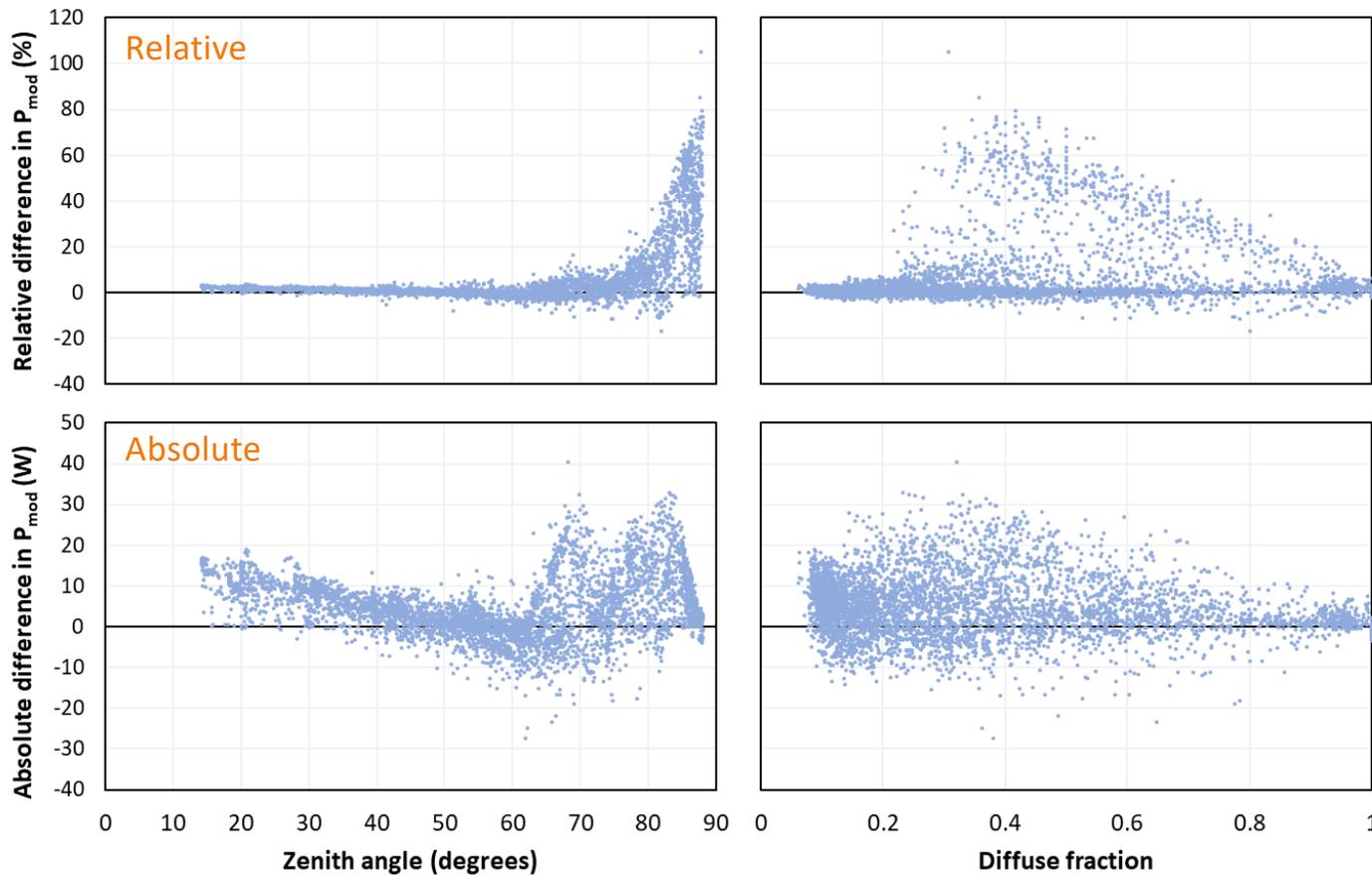
# 8. System optics: view factor vs ray tracing



For 1P SAT at Cove Mt, Utah

MBE: +1.52%

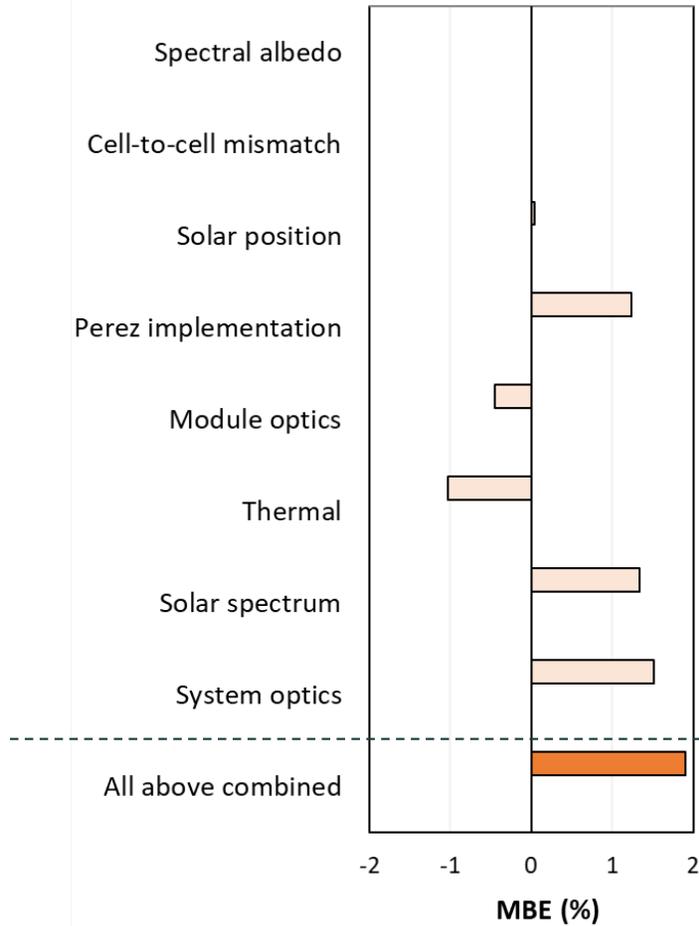
CRMSE: 7.6 W



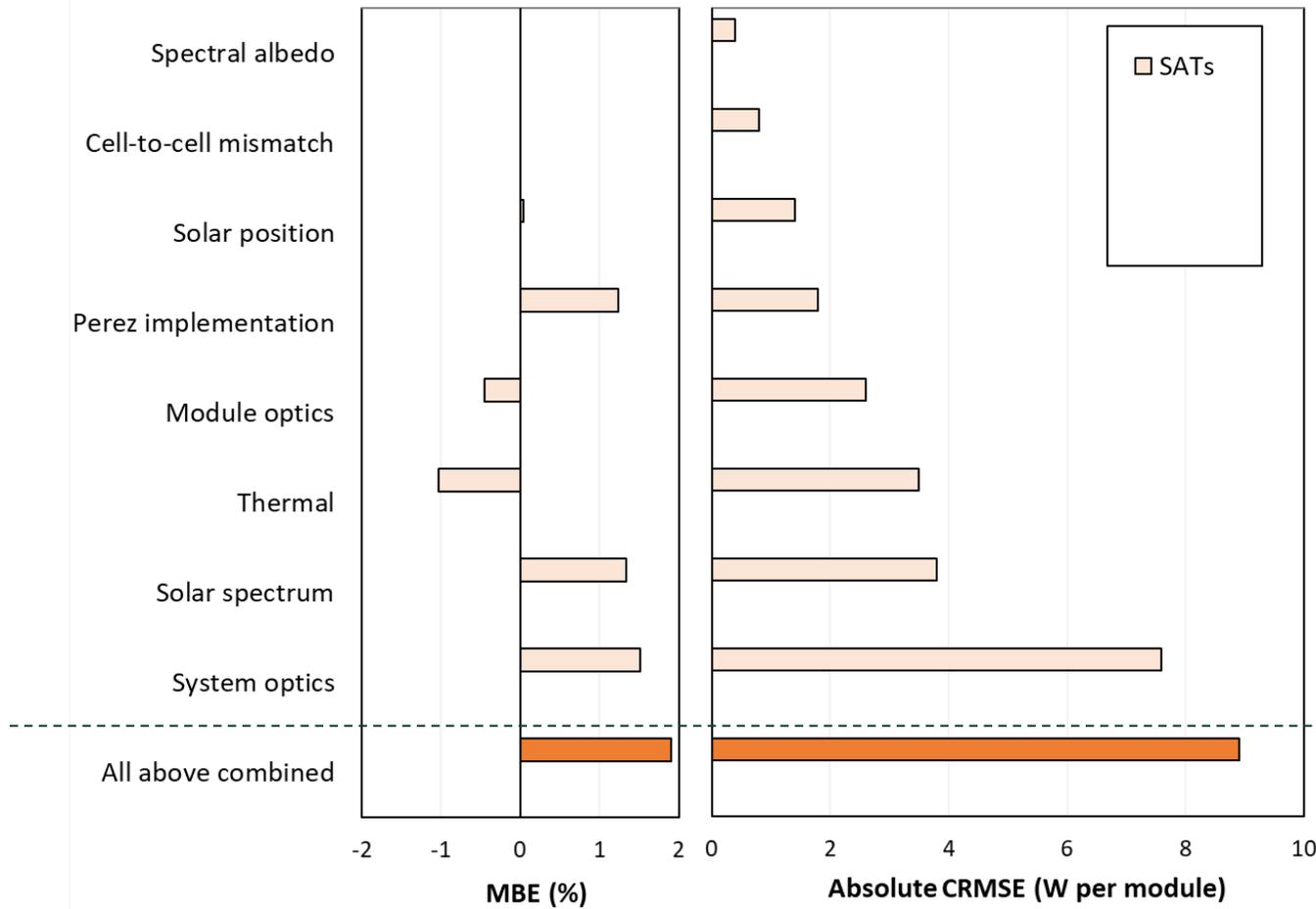
# **Results summary & conclusions**

# Results summary

Results for typical systems located at Cove Mountain, UT.



# Results summary



Results for typical systems located at Cove Mountain, UT.

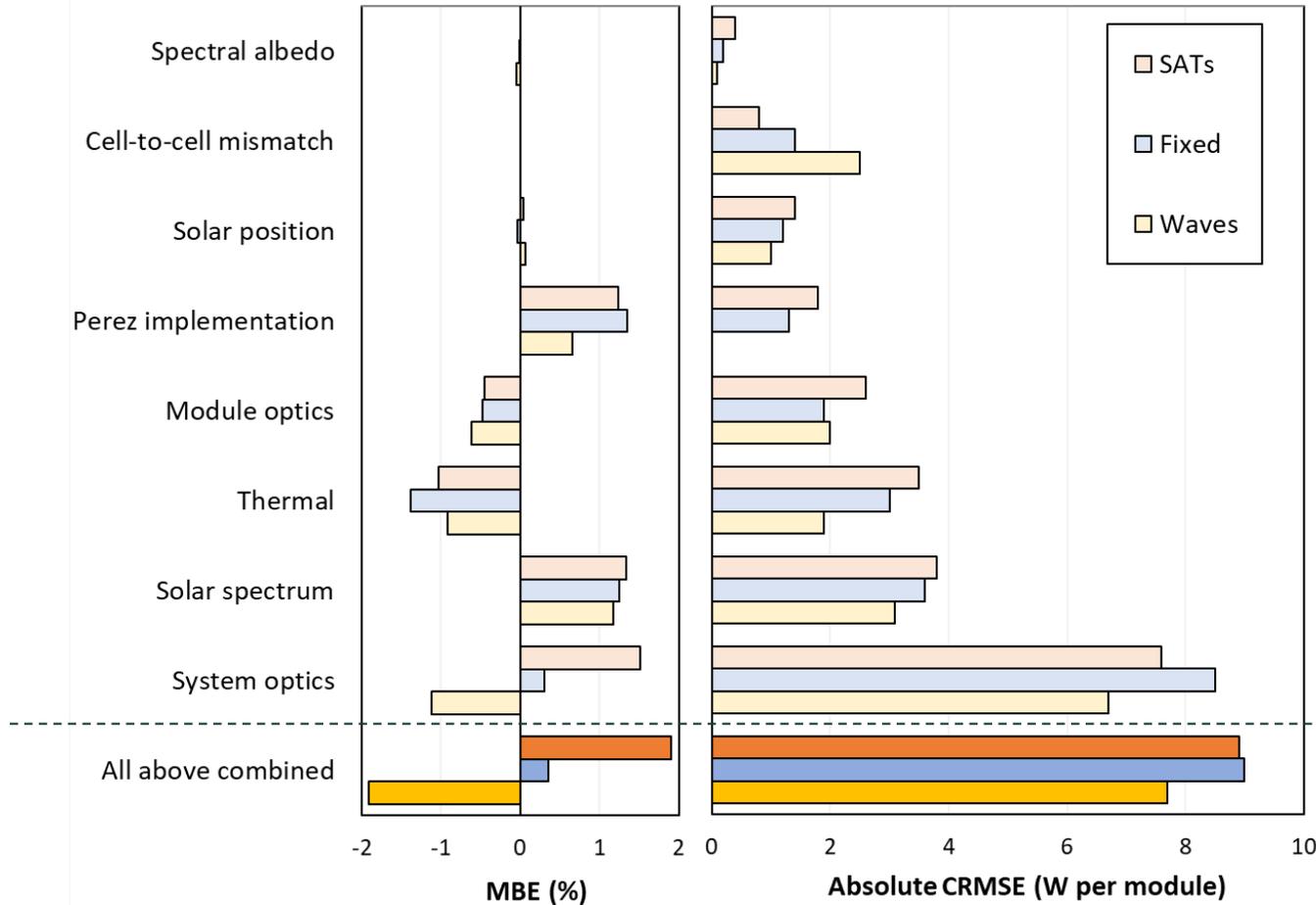
**Average  $P_{mod}$**

**SATs 315 W**

# Results summary



Results for typical systems located at Cove Mountain, UT.



## Average $P_{mod}$

**SATs 315 W**

**Fixed 254 W**

**Waves 224 W**

# Conclusions

- Simulated examples for the site of Cove Mountain plant south-west Utah.
- Largest sources of difference between conventional and advanced models:
  - System optics (VF vs RT)
  - Solar spectrum
  - Thermal
  - Module optics
  - Diffuse sky distribution
- All conventional vs all advanced

	MBE	2 × CRMSE	2 × CRMSE / P <sub>mod</sub>
SAT	+1.9%	18 W/mod	5.7%
Fixed	+0.4%	18 W/mod	7.1%
Waves	-1.9%	15 W/mod	6.9%

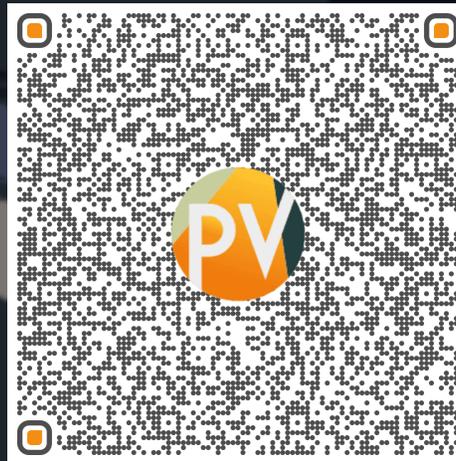
If MBE were zero (e.g., by derating module), then with 95% confidence, at any given time, the models would predict the same P<sub>mod</sub> to within

- ±15–18 W
- Equivalent to ±6–7% of the average P<sub>mod</sub>.

Thank you



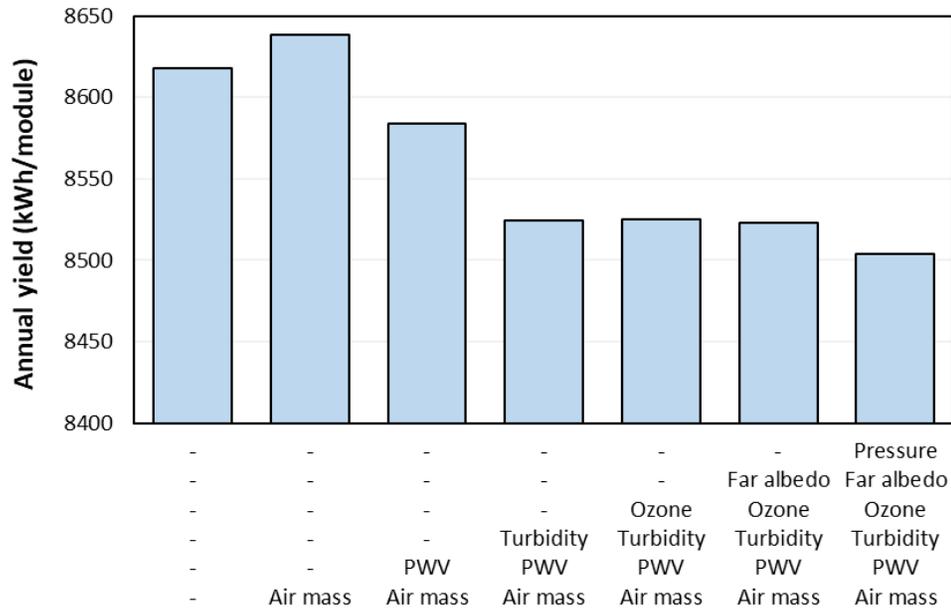
Attendees of the PVPMC workshop 2023  
are welcome to an extended free trial of  
SunSolve-Yield



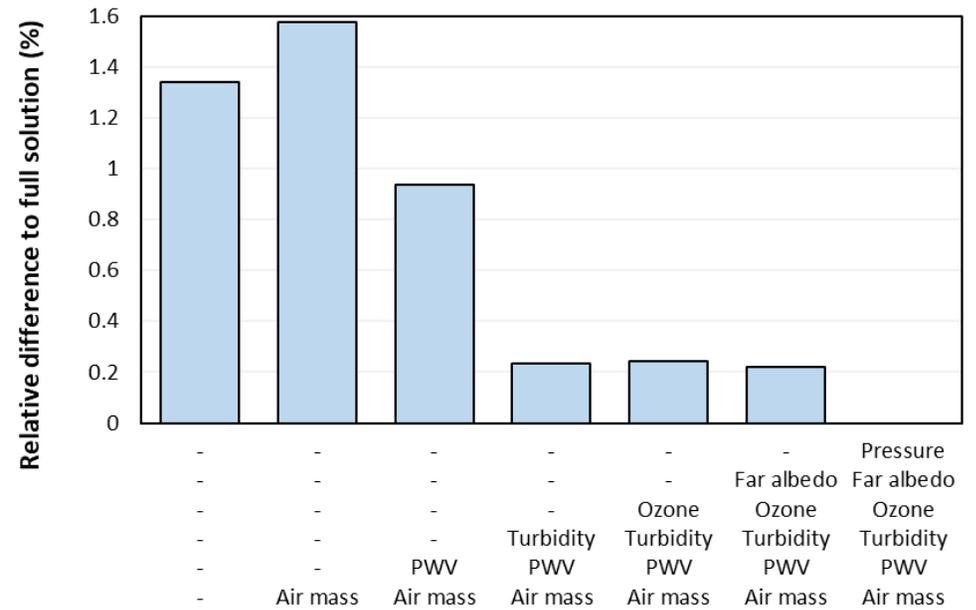
Register with this QR code during PVPMC 2023 to receive  
a free trial with twice the normal simulation allowance.

# Appendix

# Solar spectra: dependence on atmosphere (SATs)



Included in calculation of incident spectra

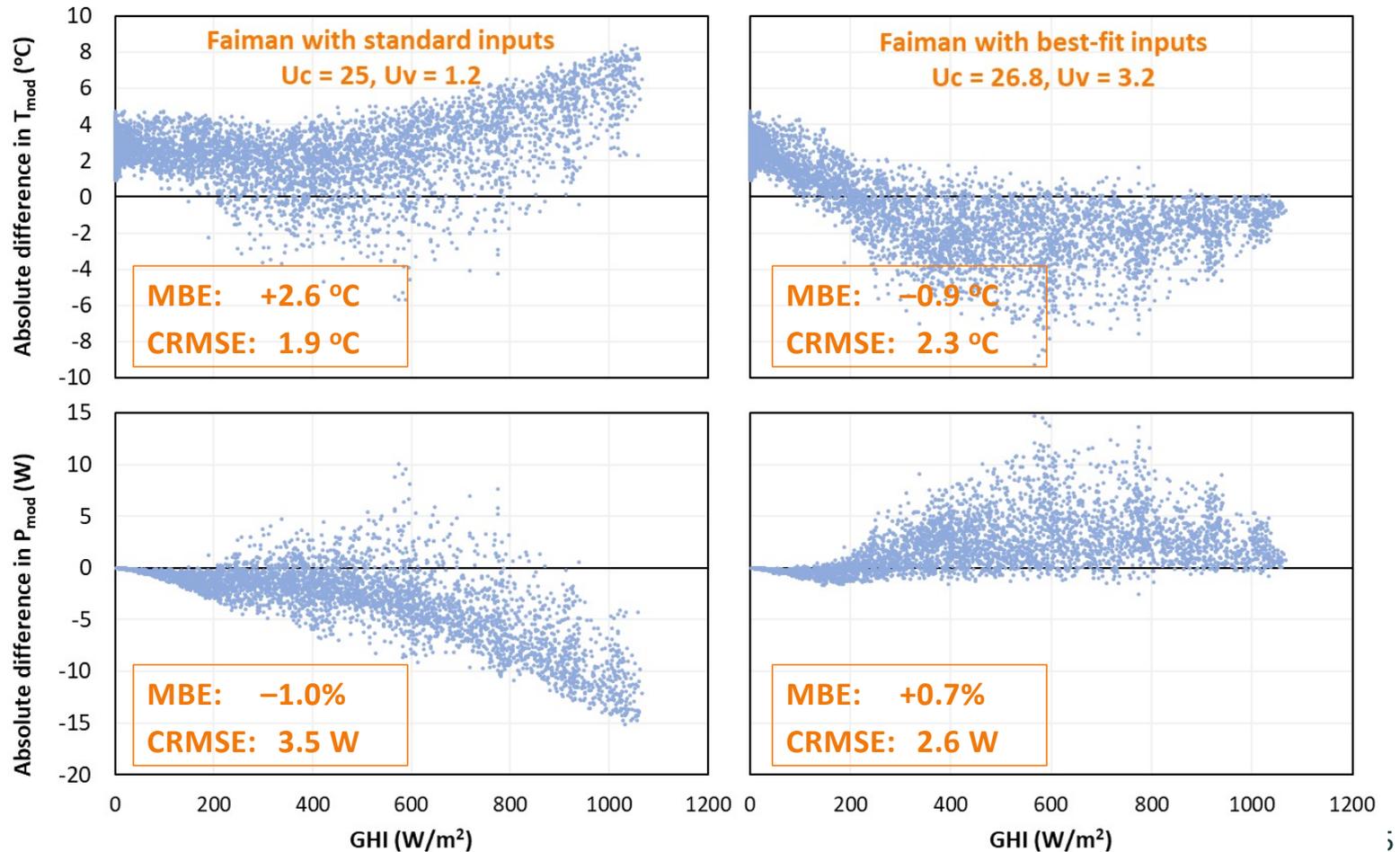


Included in calculation of incident spectra

# Thermal model: Faiman vs PVL

Absolute difference in temperature

Absolute difference in power



## A few more details



### Conventional

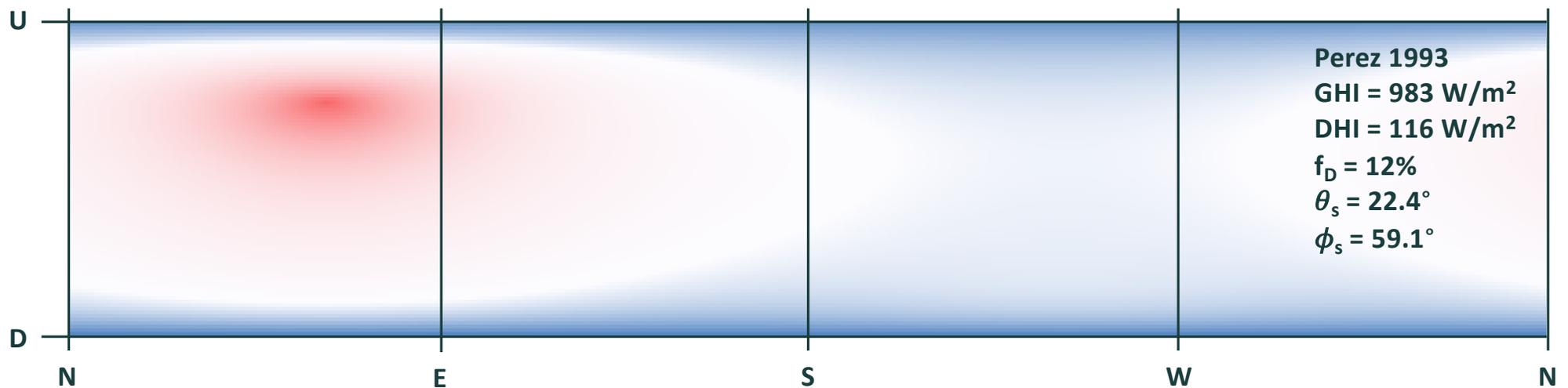
- VF:
  - Unlimited trackers, sheds or domes
  - 999 rows (max)

### Advanced

- RT:
  - 1M rays per module per condition
  - 10 min RT for full < 1 min for simple

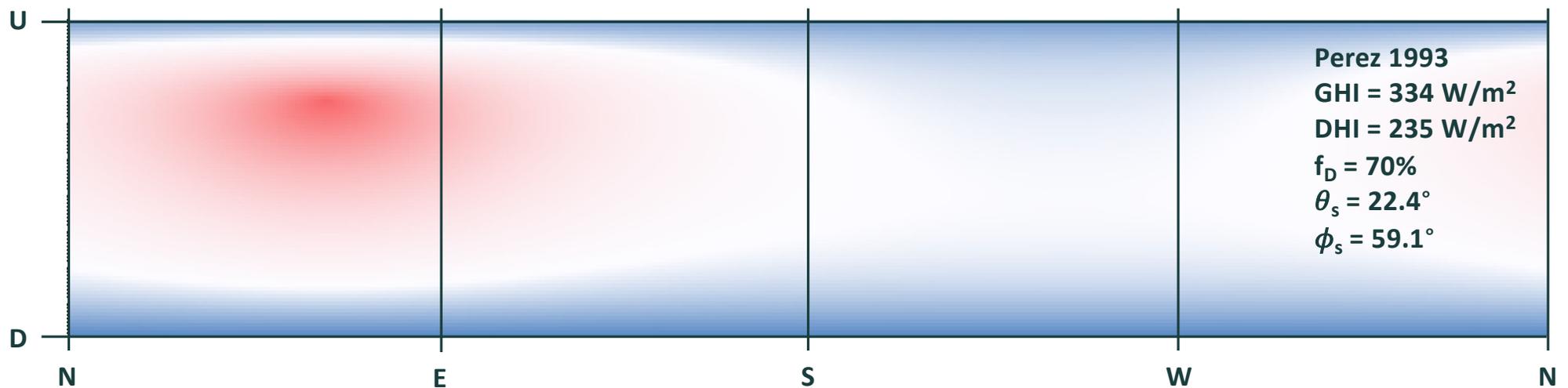
# Diffuse sky distribution

- When solved with advanced Perez model (1993).
- 12% diffuse.



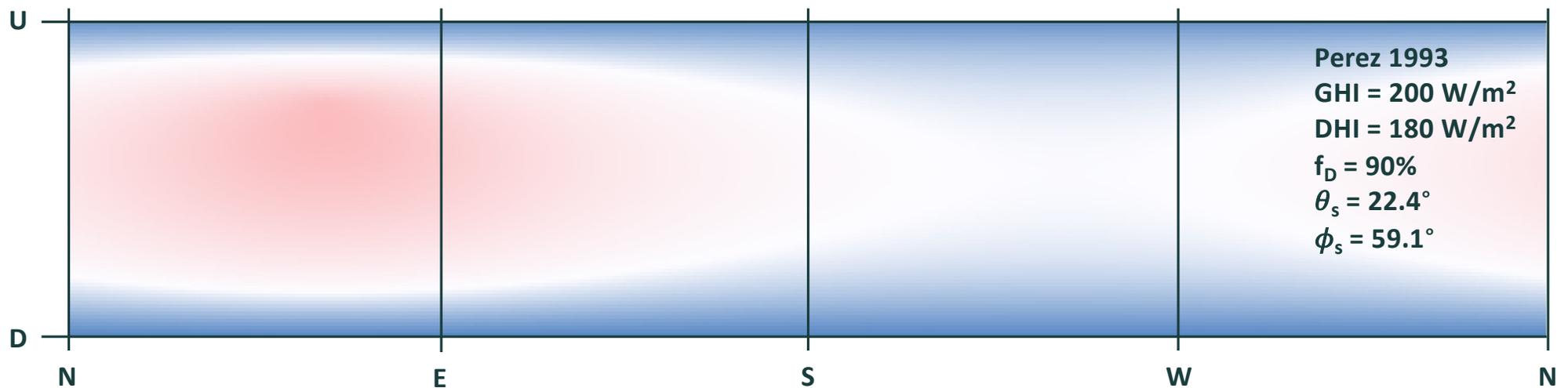
# Diffuse sky distribution

- When solved with advanced Perez model (1993).
- 70% diffuse.



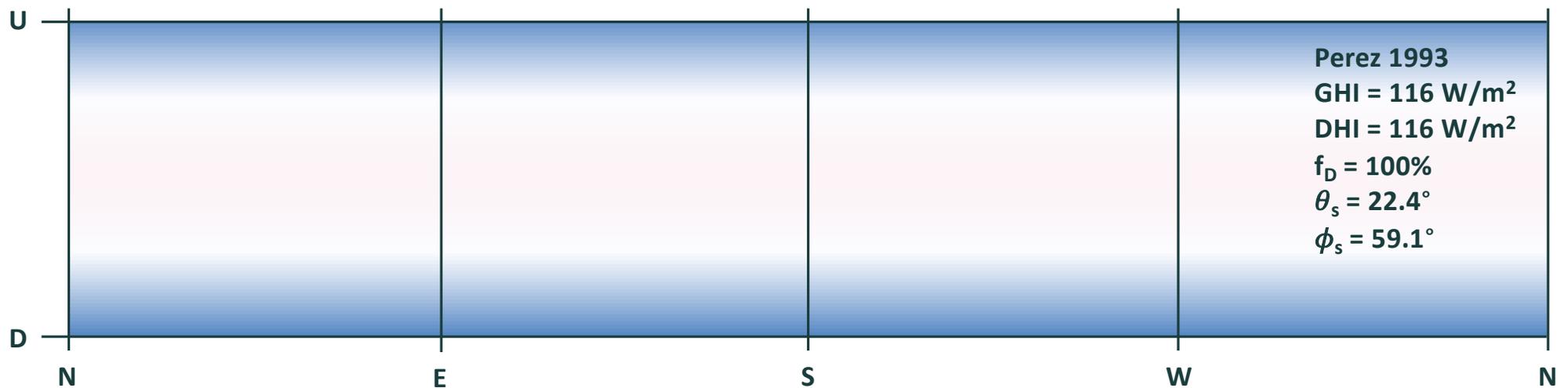
# Diffuse sky distribution

- When solved with advanced Perez model (1993).
- 90% diffuse.



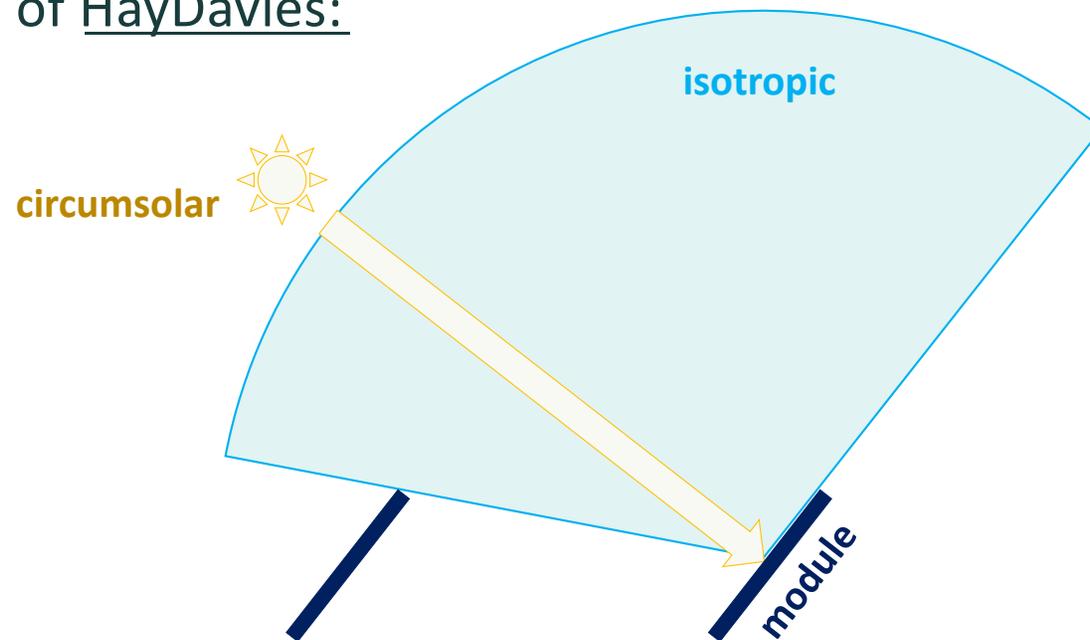
# Diffuse sky distribution

- When solved with advanced Perez model (1993).
- 100% diffuse.



# Diffuse sky distribution

- Adaption for infinite field accounts for shading from modules.
- Both implementations of HayDavies:
  - isotropic
    - partial shading
  - circumsolar
    - possible shading
  - horizon
    - none



# Results summary



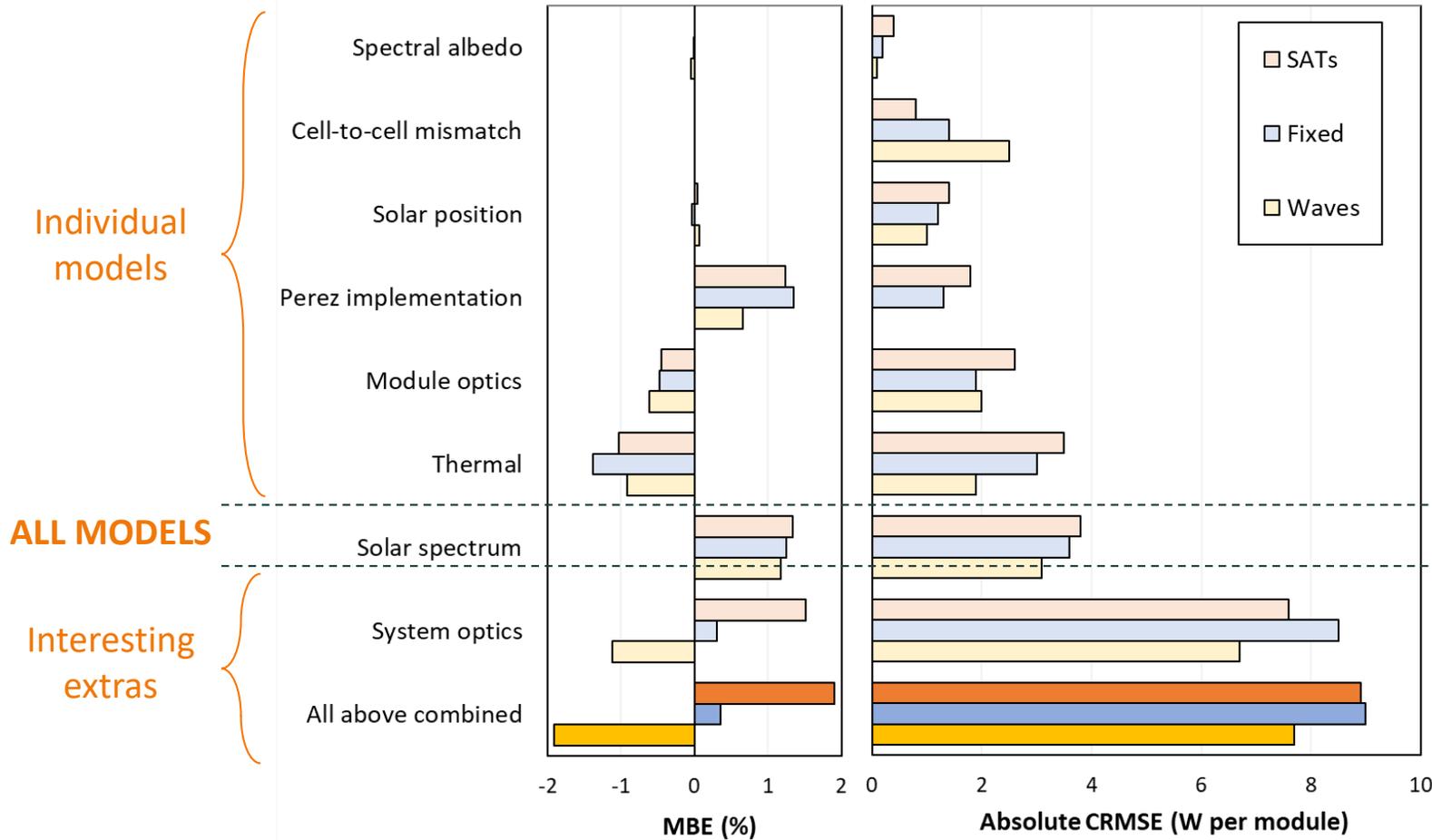
Results for typical systems located at Cove Mountain, UT.

## Average $P_{mod}$

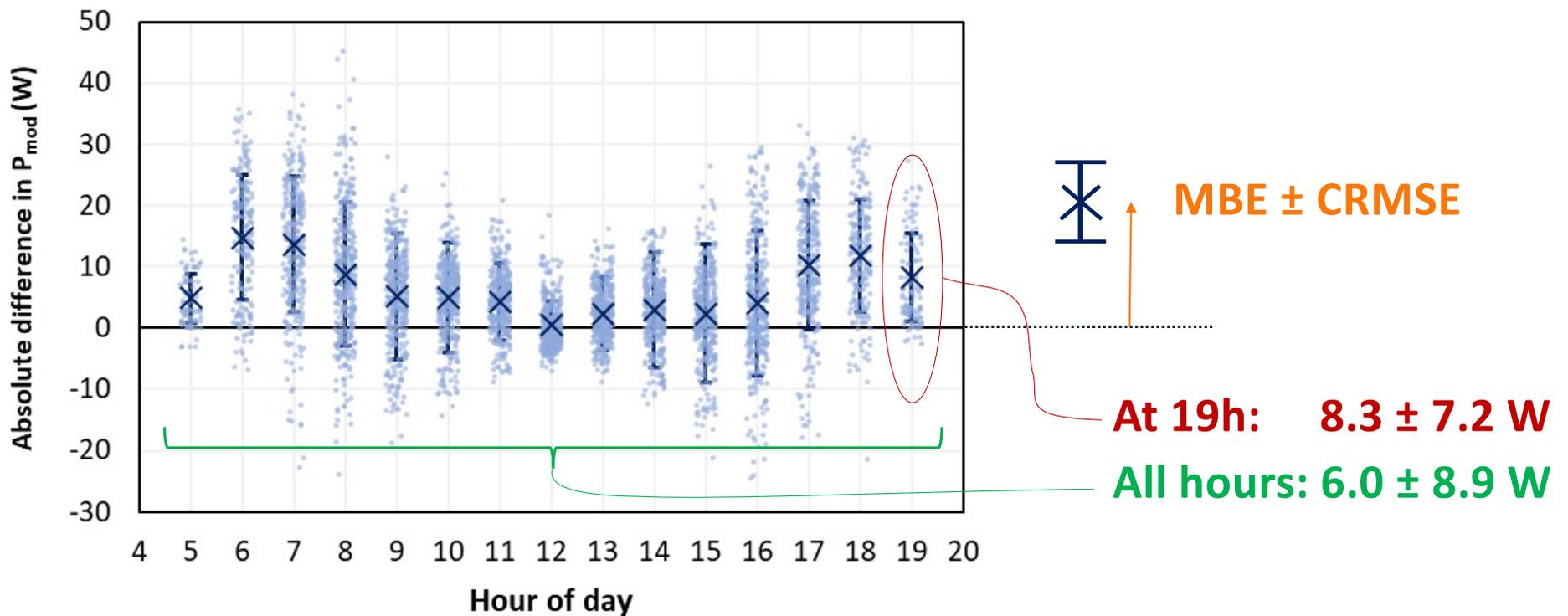
**SATs** 315 W

**Fixed** 254 W

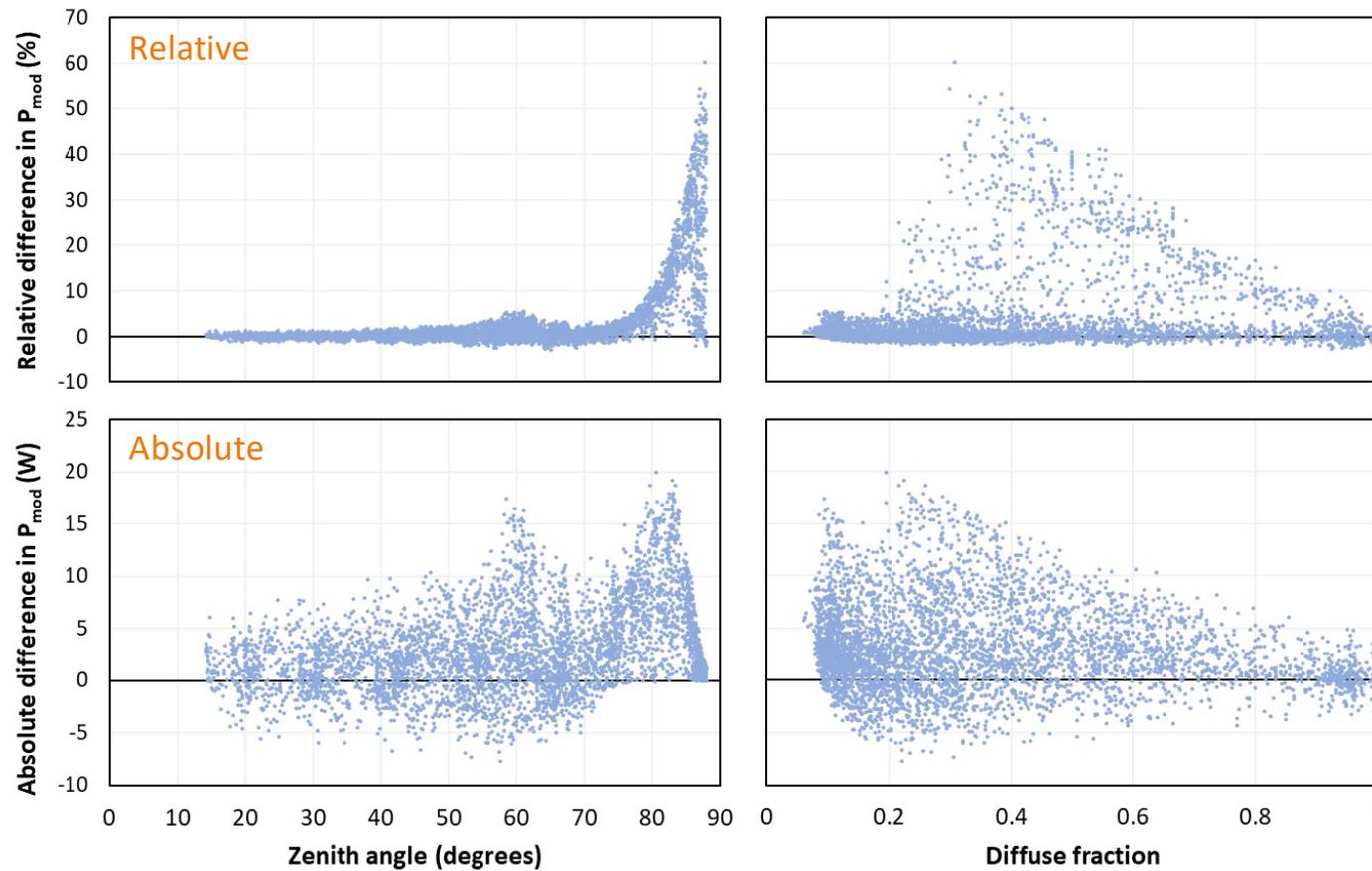
**Waves** 224 W



Difference between two models quantified with MBE & CRMSE.



# 5. Module optics: 'simple' vs ray tracing with crazy IAM



For 1P SAT at Cove Mt, Utah

MBE: +0.96%

CRMSE: 4.2 W

