

Getting more useful information from modelling of iv curves and matrix measurements

Steve Ransome (SRCL, UK)

independent PV consultant

www.steveransome.com

[mailto: steve@steveransome.com](mailto:steve@steveransome.com)

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Salt Lake City, USA..

Existing modelling methods give reasonable energy yield estimates, but there are simple analysis methods that can be done to

- differentiate PV technologies (from r_{series} , r_{shunt} etc.)
- partition PR losses into separate causes (e.g. v_{oc} , r_{sc})
- find what may be limiting performance (e.g. r_{oc} is high)
- calculate degradation rates for each loss factor under different weather conditions (e.g. r_{sc} fall causes higher degradation at low G)
- be able to suggest optimization targets (e.g. reduce r_{series})

This talk suggests some improvements to modelling methods, normalizing of measurements, loss and graphical analysis

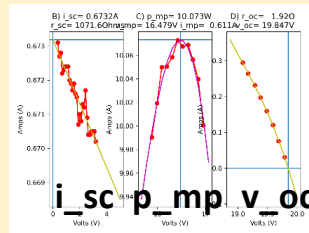
Outdoor data used for this study

<https://www.nrel.gov/docs/fy14osti/61610.pdf>

- ✓ 11 modules of different technologies (CdTe, CIGS, aSi, 3JaSi, mcSi, scSi, HIT ...)
- ✓ Measured 3 sites FL, CO, OR for >1year
- ✓ ~180 IV points for curves each 5-15 mins
- ✓ Pyranometers for G_POA, DHI, GHI, BNI
- ✓ Soiling, precipitation, RH (ignored here)
- ✓ Fits to i_{sc} , i_{mp} , v_{mp} , v_{oc} were given

However

- ✗ No windspeed
- ✗ No spectrum
- ✗ No r_{sc} or r_{oc} fits but calculated here →



User's Manual for Data for Validating Models for PV Module Performance

W. Marion, A. Anderberg, C. Deline, S. Glick, M. Muller, G. Perrin, J. Rodriguez, S. Rummel, K. Terwilliger, and T.J. Silverman

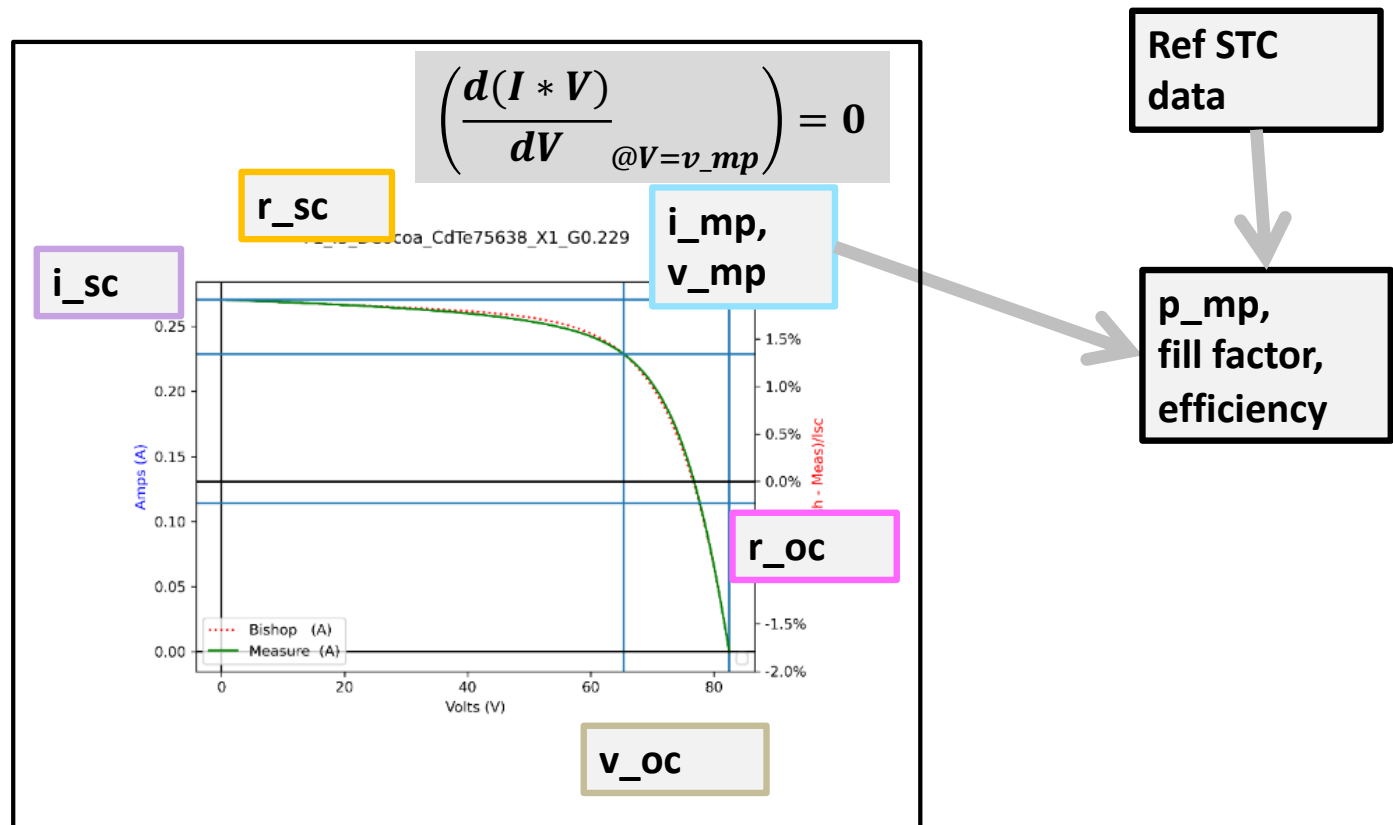
NREL is a national laboratory of the U.S. Department of Energy Office of Energy Efficiency & Renewable Energy Operated by the Alliance for Sustainable Energy, LLC

This report is available at no cost from the National Renewable Energy Laboratory (NREL) at www.nrel.gov/publications.

Technical Report
NREL/TP-5200-61610
April 2014

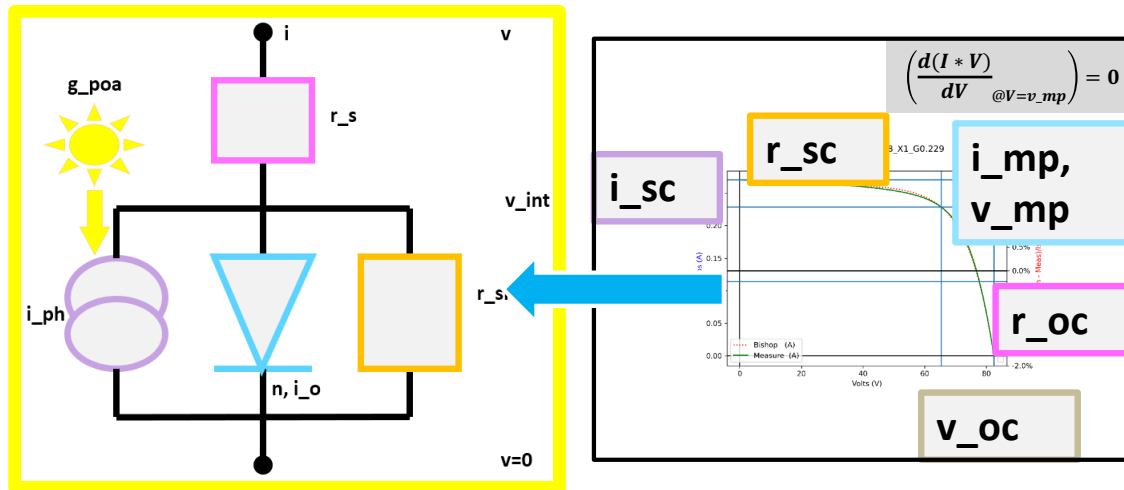
Contract No. DE-AC36-08GO28308

Typical measured NREL IV curve with some fitted parameters (A, V, Ω, W)



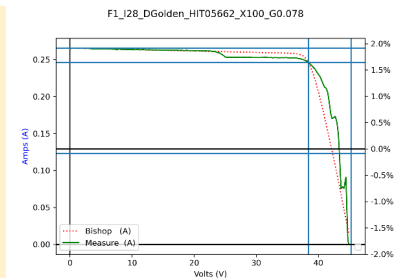
IV curve → 1-diode model fit with 5 components

color shows which component 'dominates' each fit parameter



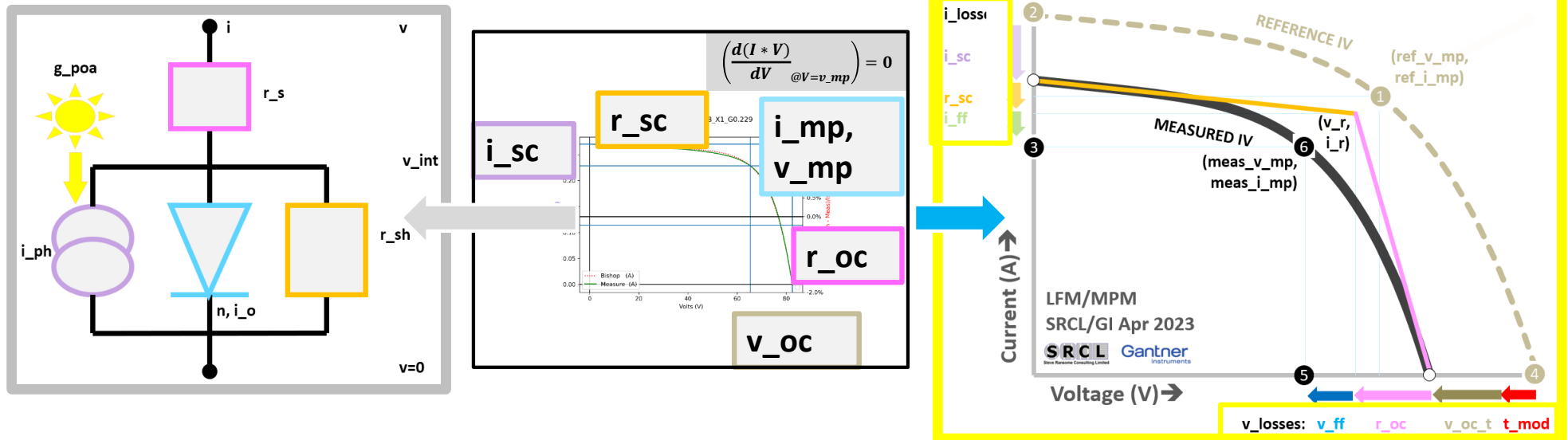
1-diode best fits to IV curves are limited by

- Point distribution : e.g. “poor r_{sh} fit if few near i_{sc} ”
- Differing fit algorithms, non-unique best fits
- “imperfections” mismatch, rollover, variable cloud during scan
- Note : 5 variables are insufficient to fit all IV curves perfectly



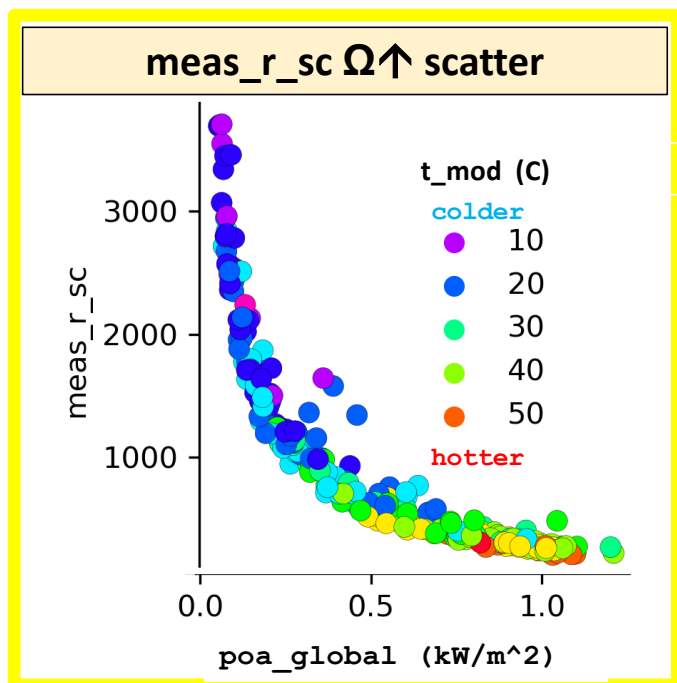
IV Curve → MLFM* fit with 6 normalised electrical and 1 temperature correction

* mechanistic loss factors model



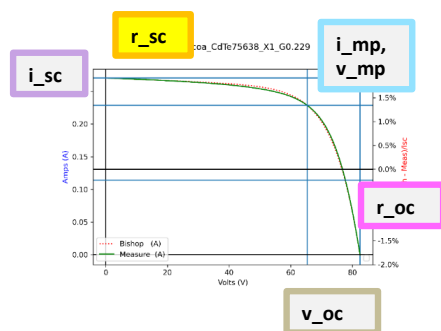
- 6+1 normalised losses from IV curve shape
- Characterise loss parameters vs. G, T and time

Analysis of $r_{sc}(G, T)$



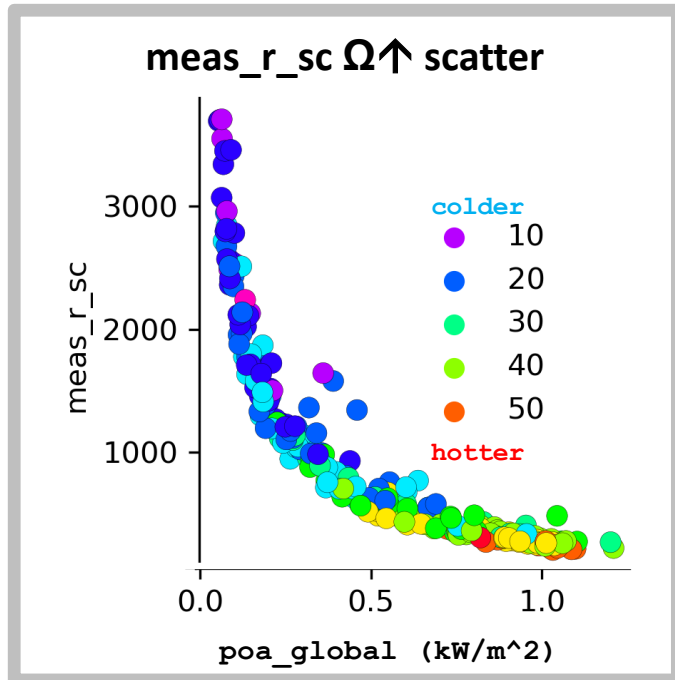
r_{sc} vs. G is curved with a small -ve T sensitivity.
Most models assume $r_{sc} = \text{constant}$ or $r_{sc} \sim 1/G$
PVSYST has exponential fit

$$r_{sc} = -1 / \left(\frac{dI}{dV} @ V=0 \right) \sim r_{shunt}$$



HIT module shown –
c-Si and thin films all have similar
shapes
(but differing values)

Analysis of $r_{sc}(G, T)$



Similar fits can be done
for any normalised
parameters

Outdoor Matrix : has
50-100 useful G,T points

IEC 61853 (indoor) has ~28
(trying to reduce to ~6
for cost savings)

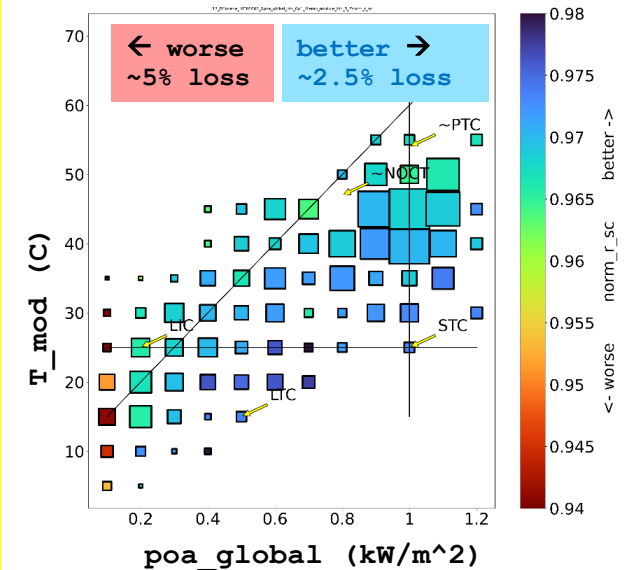
Square area proportional
to Insolation ($\text{kWh/m}^2/\text{yr}$)

**MLFM Good fit to $\text{norm_r_sc}(G, T)$
Temperature coefficient from fit as $c_{2t} \rightarrow$**

mlfm fit $\text{norm_r_sc} =$
 $= c_{1c} + c_{2t} * (T - 25) + c_{3lg} * \text{LOG}_{10}(G) + c_{4g} * G$

Improved analysis of $r_{sc}(G, T)$

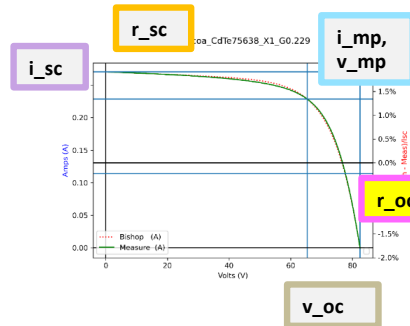
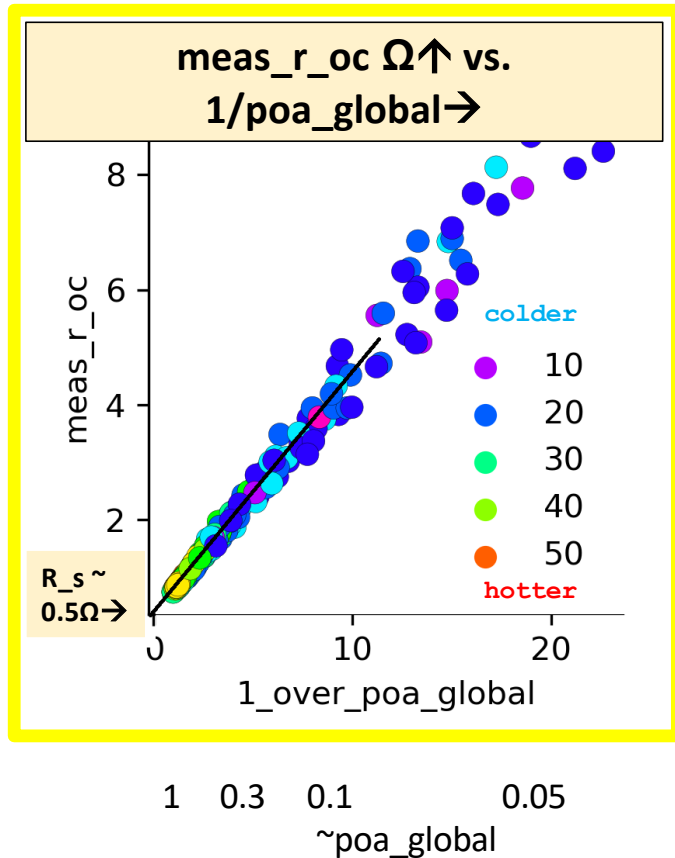
norm_r_sc (% color) matrix



mlfm	c_1c	c_2t	c_3lg	c_4g	rmse
norm_r_sc	98.3%	-0.07%	3.0%	-0.3%	1.1%

MLfm calcs	STC	LIC	NOCT	HTC
norm_r_sc	97.4%	95.6%	96.4%	95.4%

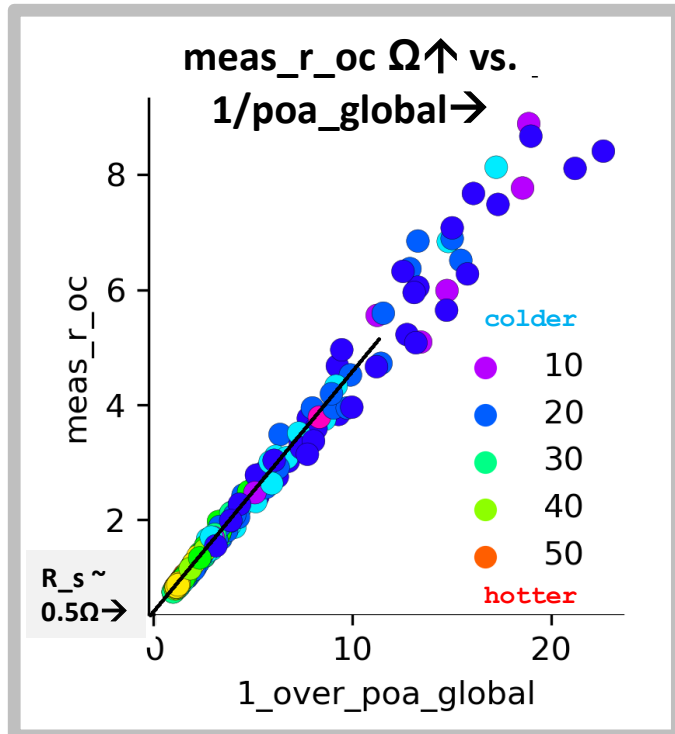
Analysis of $r_{oc}(G, T)$



$$r_{oc} = -1 / \left(\frac{dI}{dV} \bigg|_{I=0} \right) = r_s + f_n(1/G)$$

- $r_{oc} \sim \text{linear v.s } 1/G$, extrapolates to r_s at $1/G \rightarrow 0$
- Small Temp. coeff. depends on technology, usually
 - $d/dT(\text{norm}_r_{oc}) < 0$ for cSi (metal)
 - $d/dT(\text{norm}_r_{oc}) > 0$ for Thin films (TCO)
- Most models assume $r_s(G, T) = \text{constant}$

Analysis of $r_{oc}(G, T)$



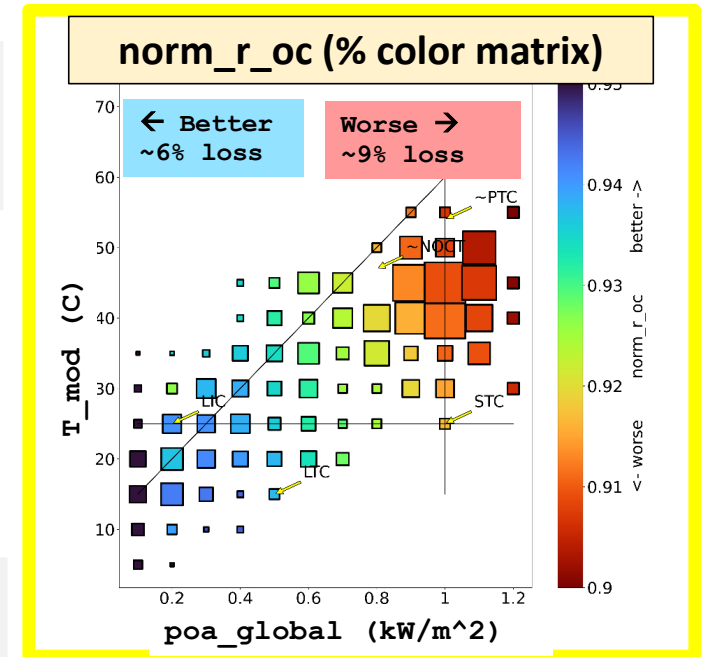
Similar fits can be done for any normalised parameters

Outdoor Matrix : has 50-100 useful G,T points

IEC 61853 (indoor) has ~28 (trying to reduce to ~6 for cost savings)

Square area proportional to Insolation ($\text{kWh/m}^2/\text{yr}$)

Improved analysis of $r_{oc}(G, T)$



MLFM Good fit to norm $r_{oc}(G, T)$

Temperature coefficient from fit as $c_{2t} \rightarrow$

mlfm fit norm $r_{oc} =$
 $= c_{1c} + c_{2t} * (T - 25) + c_{3lg} * \text{LOG}_{10}(G) + c_{4g} * G$

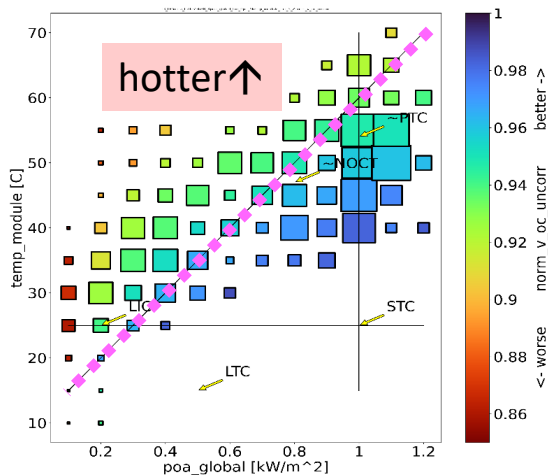
mlfm	c_1c	c_2t	c_3lg	c_4g	rmse
norm r_{oc}	97.7%	-0.04%	3.8%	-6.3%	1.5%

MLfm calcs	STC	LIC	NOCT	HTC
norm r_{oc}	91.4%	93.8%	91.5%	89.4%

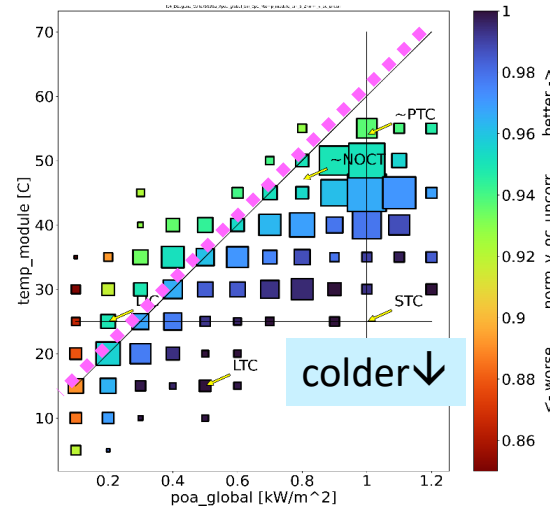
Performance at different sites or times

(CdTe, norm_v_oc = color)

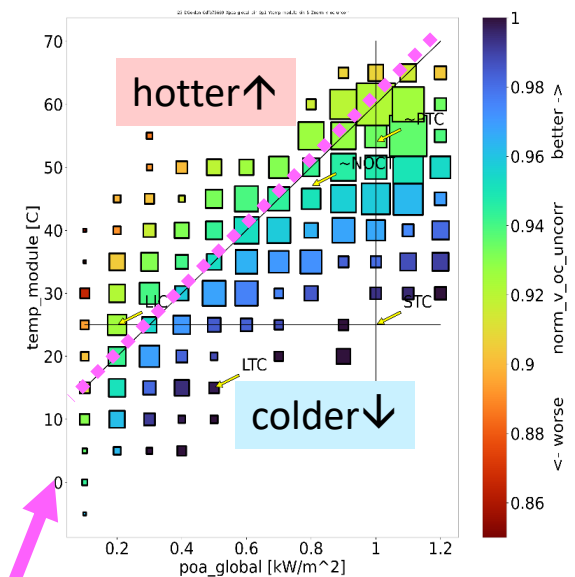
A) COCOA FLORIDA (#1)



B) EUGENE OREGON (#1)



C) GOLDEN COLORADO (#2)



(Note: differing areas of squares from climates, distributions vs. temperature and irradiance)

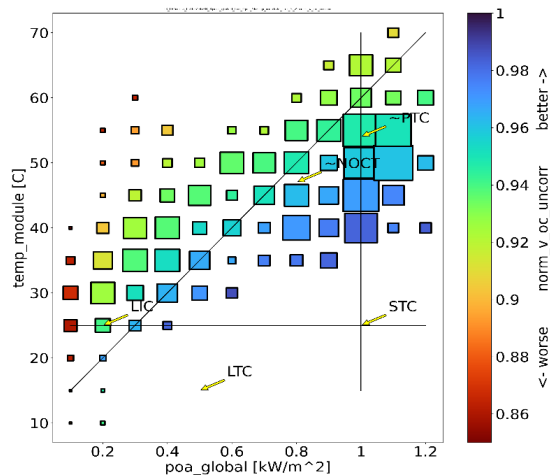
There are reference lines at G=1, T=25 and a pink diagonal from (0.1,15) to (1.2,70)

Lower coldest temperature at Golden than others

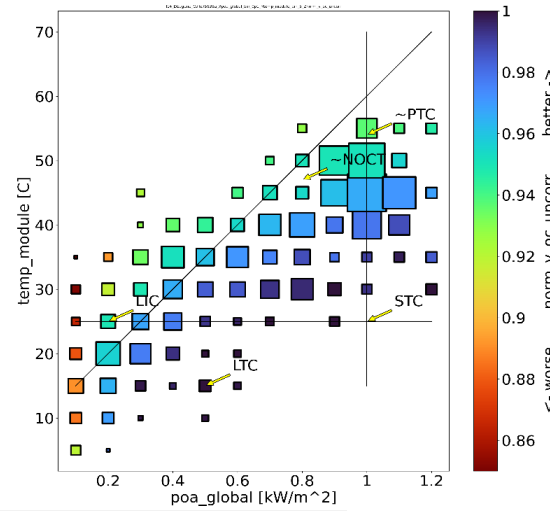
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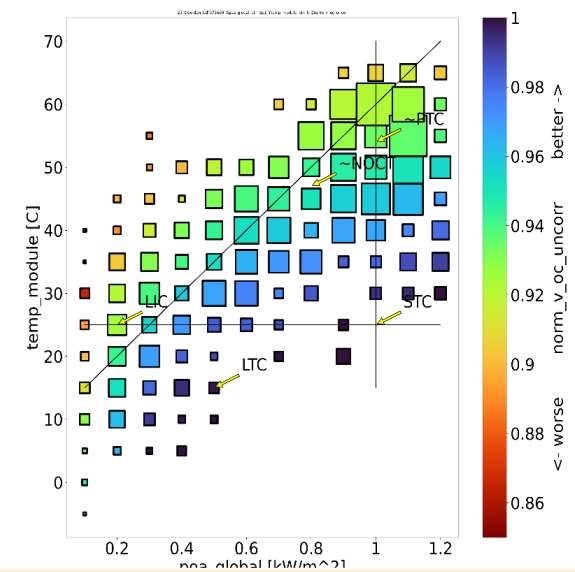
A) COCOA FLORIDA (#1)



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$mlfm\ fit = c_{1c} + c_{2t} * (T - 25) + c_{3lg} * LOG_{10}(G) + c_{4g} * G$

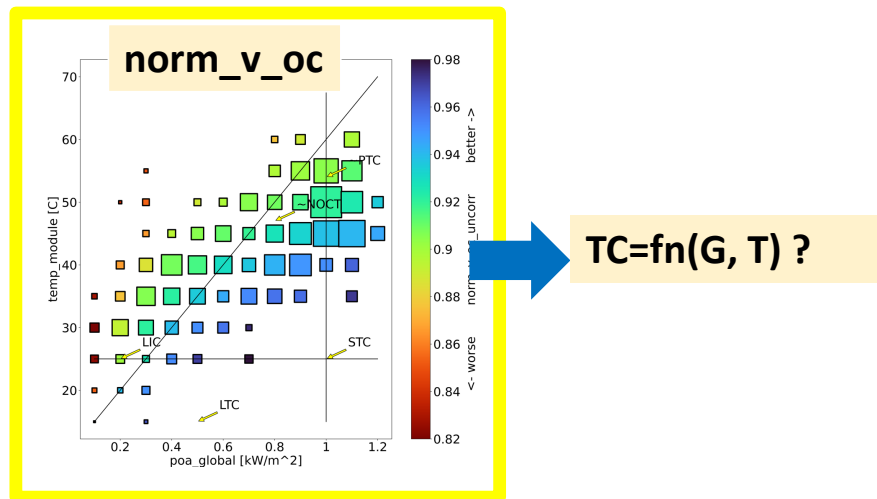
Any performance changes would show up in MLFM fit coefficients and values at given conditions e.g. STC

State	Mod	param	c_1c	c_2t	c_3lg	c_4g	rmse	STC	LIC	NOCT	HTC
FL	CdTe	norm_v_oc	104.9%	-0.27%	14.0%	-3.0%	0.40%	101.9%	94.5%	95.8%	88.6%
CO	CdTe	norm_v_oc	102.3%	-0.25%	11.6%	-1.9%	0.39%	100.4%	93.8%	94.6%	87.9%
OR	CdTe	norm_v_oc	105.1%	-0.28%	13.9%	-3.6%	0.83%	101.5%	94.7%	95.2%	87.4%

Does the temperature coefficient vary $TC=fn(G, T)$?

e.g. $\beta_{v_{oc}}(G, T) = 1/v_{oc_STC} * \Delta v_{oc}/\Delta T$

- Most models assume Temperature Coefficients $TC(G, T) = \text{constant}$
- Some manufacturers may provide valid ranges if they vary e.g. ">25C"
- This method with 50-100 points allows us to easily map a $TC(G,T)$ from a normalised loss matrix

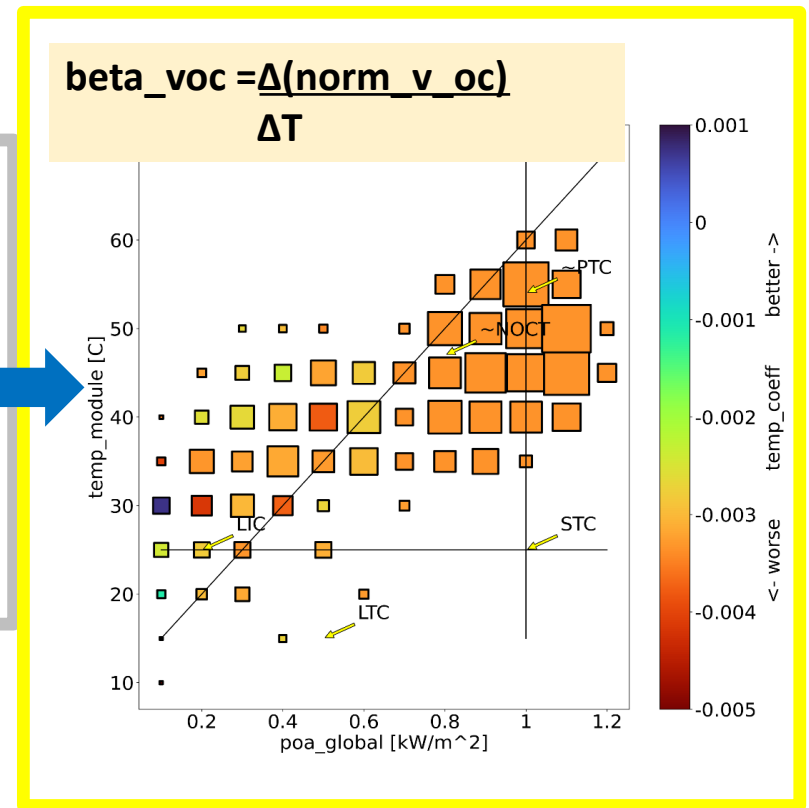
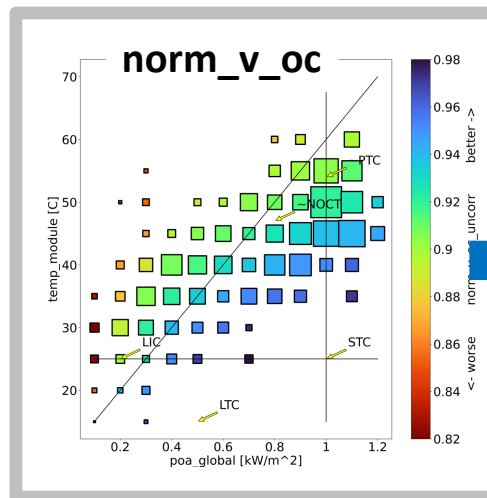


Calculated Temperature coefficient $TC = f_n(G, T)$

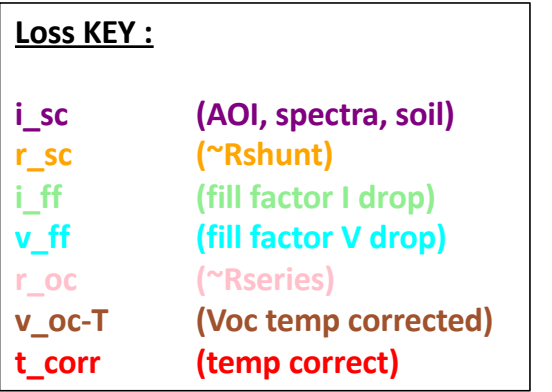
$TC(G, T)$ = difference between adjacent temperature points \updownarrow
mc-Si beta $v_{oc} \sim -0.35\%/K$

Some astable thin films have “non-constant temp coeffs” where warm autumn performance (after high temperatures) differs from cool spring (after cool weather)

Not yet tested on OPV, perovskite, dye or novel tandem



1/ff_ref
↓
PRdc

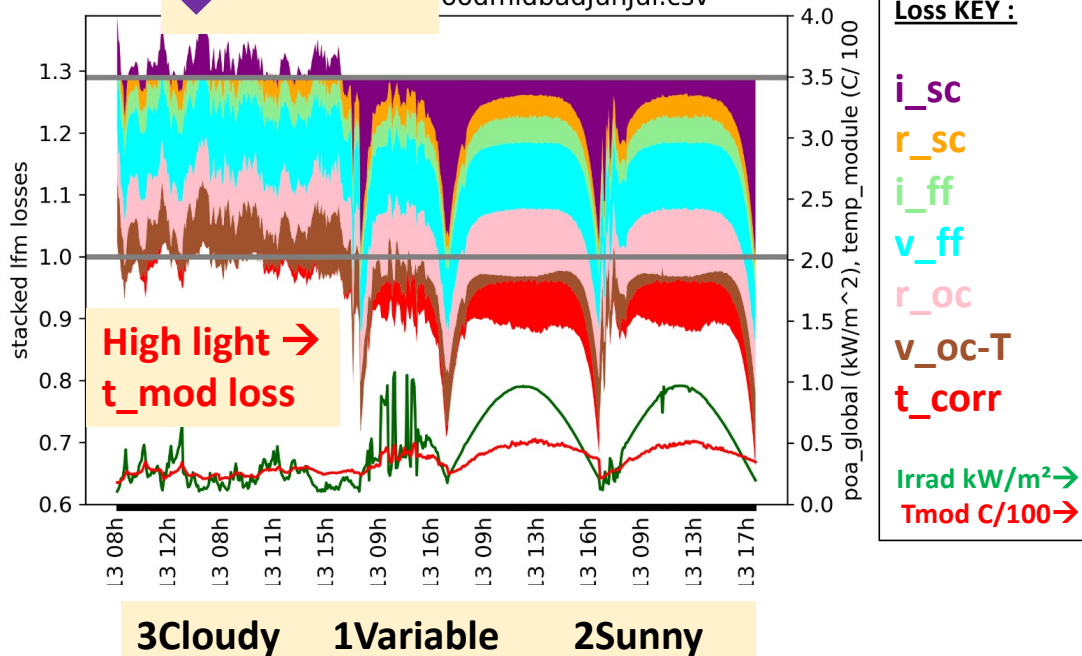


Stacked losses under different weather conditions (no correction for reflectivity or spectral response from pyranometer)

HIT 2010

Low light
Spectral gains
↓

oodmidbadJunJul.csv

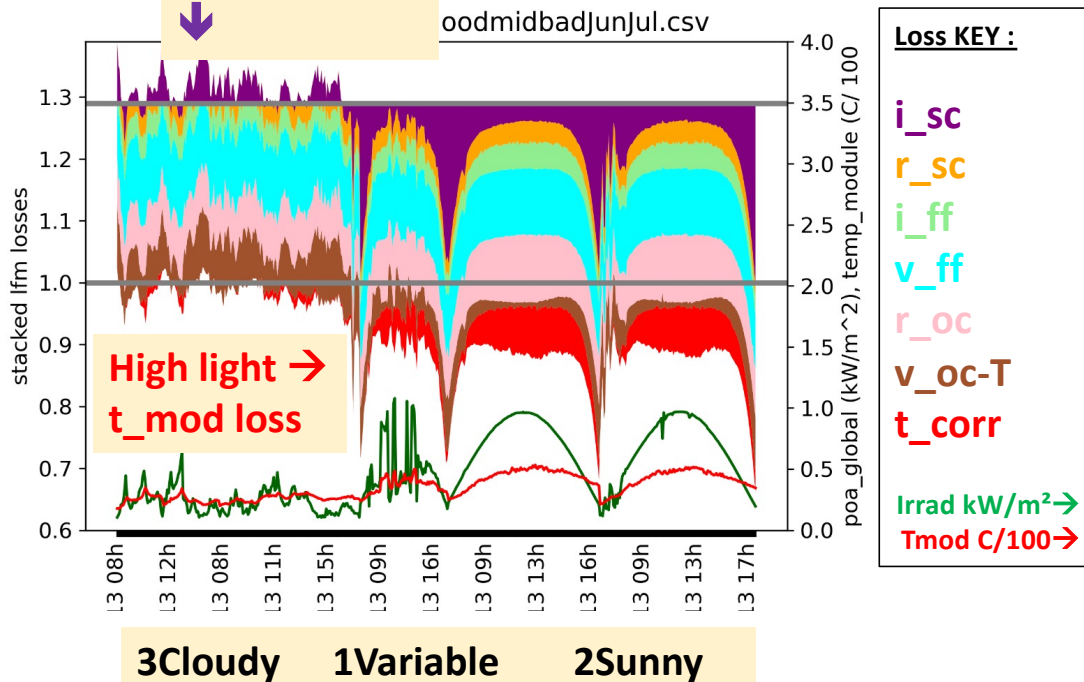


Stacked losses under different weather conditions

(no correction for reflectivity or spectral response from pyranometer)

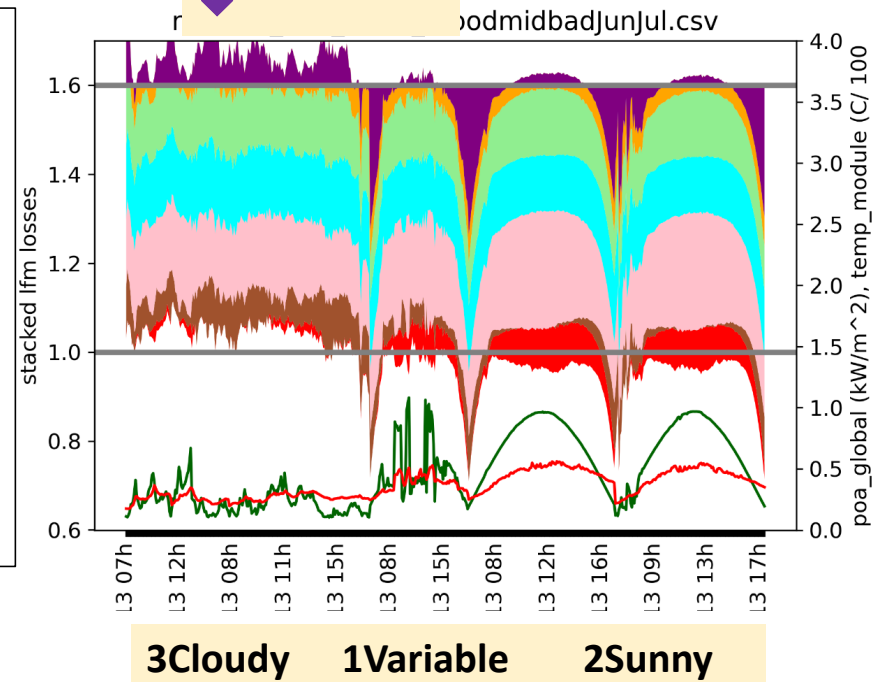
HIT 2010

Low light
Spectral gains
↓



CdTe 2010

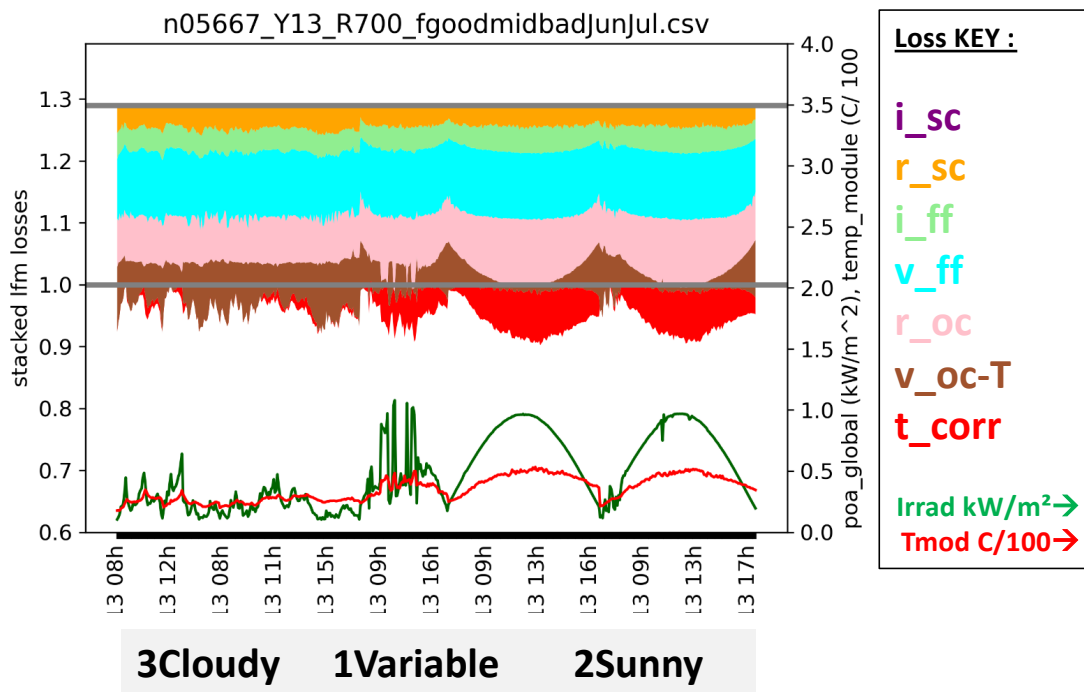
Low light
Spectral gains
↓



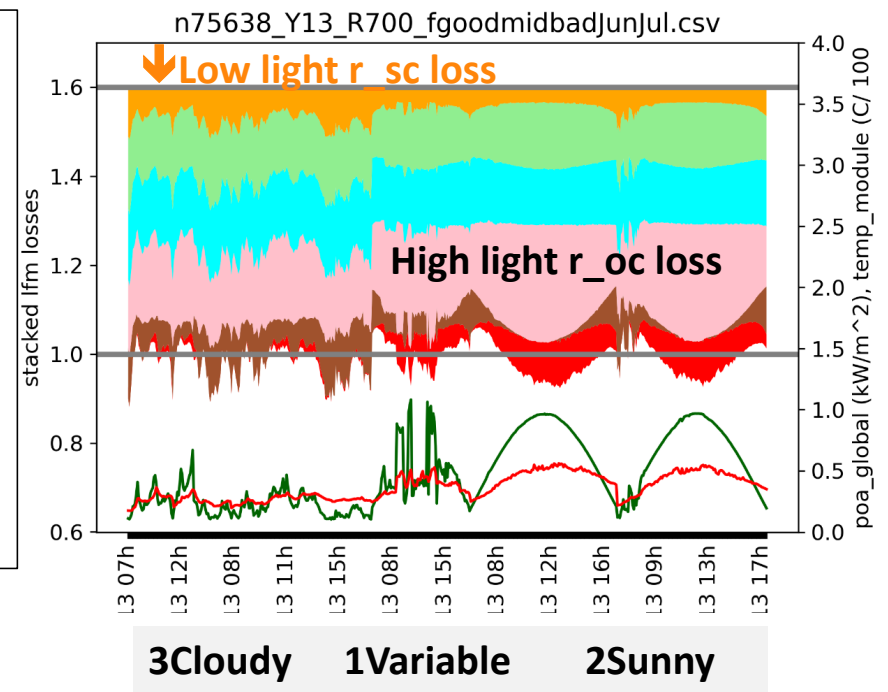
Stacked losses under different weather conditions

– self referenced so easier to quantify other losses without i_{sc} errors

HIT 2010



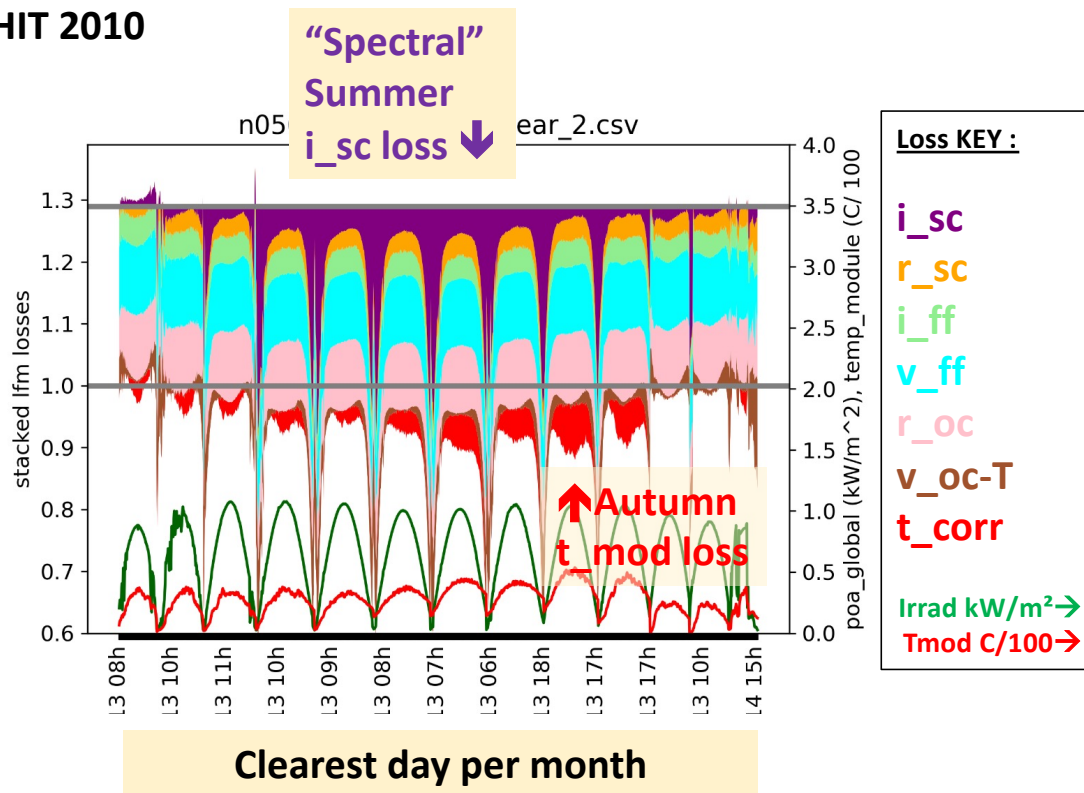
CdTe 2010



Stacked losses “clearest day per month Dec – Dec” “stable modules”

- can show stepwise or continuous changes, seasonal instability or maybe sensor problems

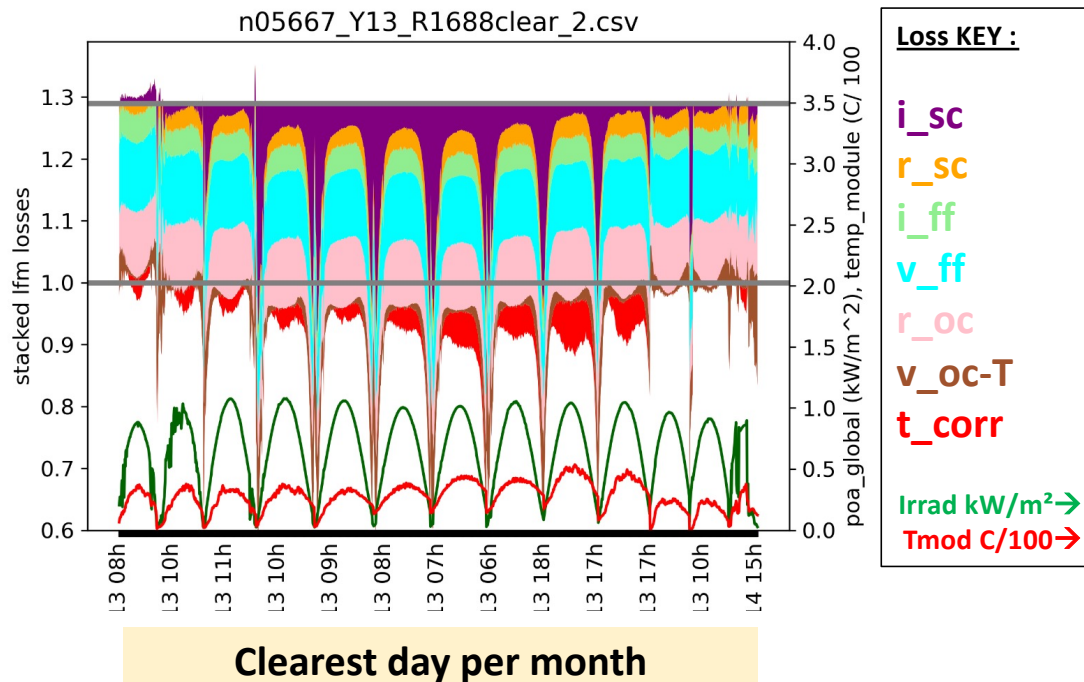
HIT 2010



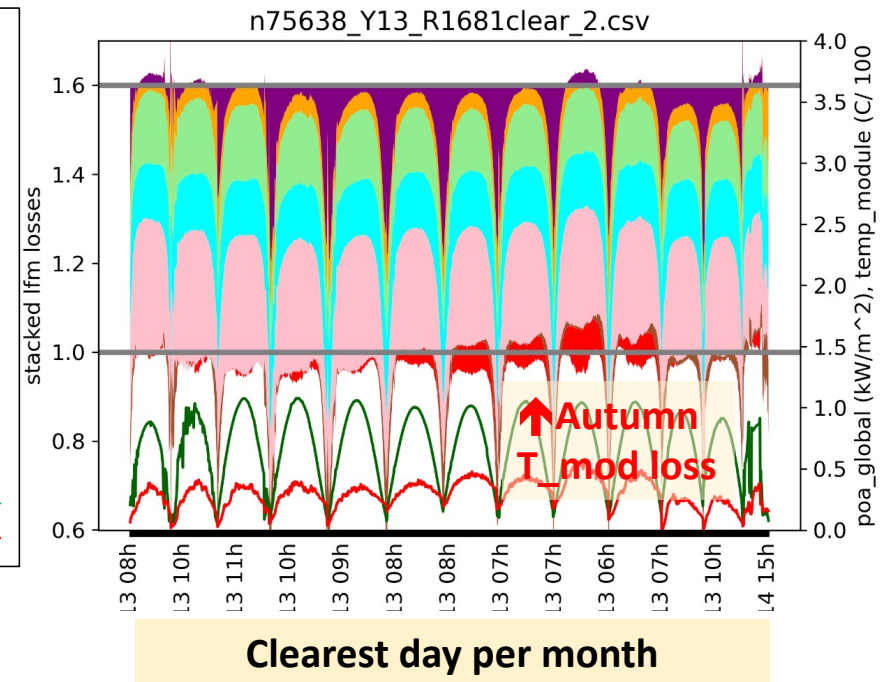
Stacked losses “clearest day per month Dec – Dec” “stable modules”

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HIT 2010



CdTe 2010

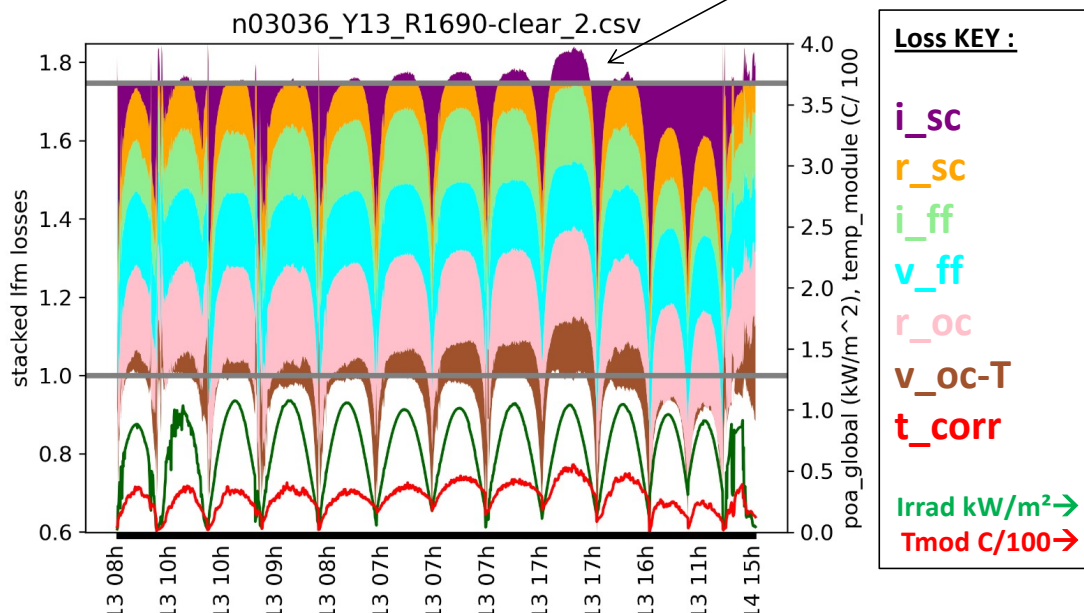


Stacked losses “clearest day per month Dec – Dec” “unstable modules”

- show changes, seasonal astability, thermal annealing or maybe sensor problems

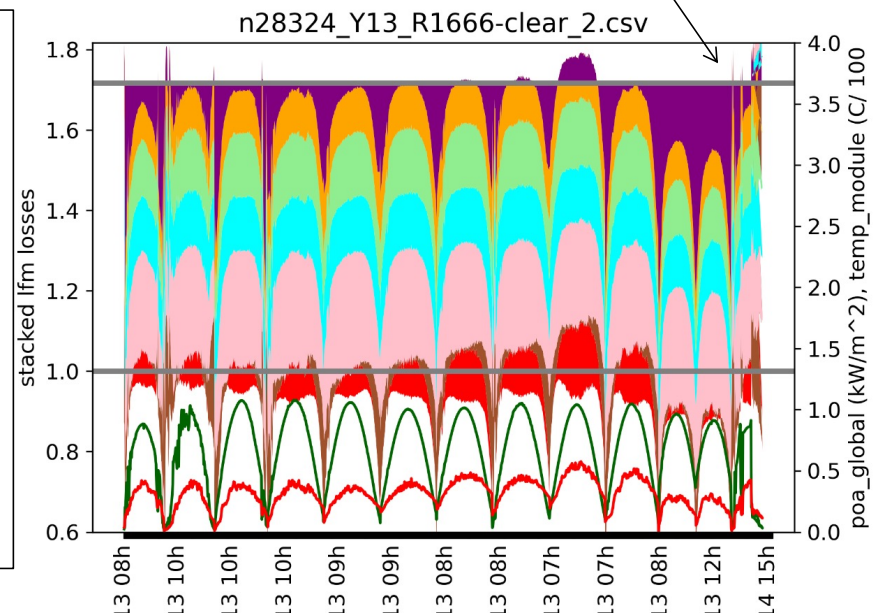
Atypical weather days? Thermal annealing? Spectrum?
Soiling or sensor problems? i_{sc} worse but v_{oc} is better than other days

CIGS? 2010 Missing $\beta_{v_{oc}}$



Clearest day per month

3J aSi? 2010 Beta_v_oc



Clearest day per month

Conclusions

New methods have been shown using normalised loss factors to improve IV curve and matrix fits finding temperature and performance coefficients

Matrix plots (with areas ~ Insolation) are easiest to visualize and fit

Losses and causes help understand the behaviour vs. G,T and time

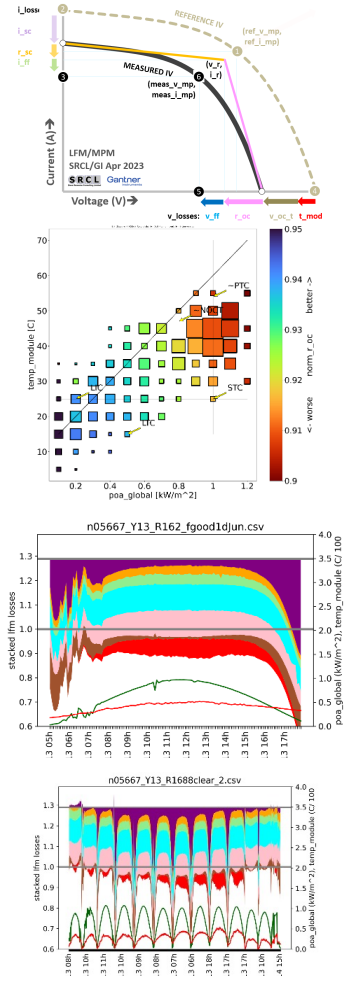
Relative performance of different PV technologies has been contrasted

Please contact me for more information steve@steveransome.com

Thank you for your attention!

Link to temporary version until it's published by SANDIA

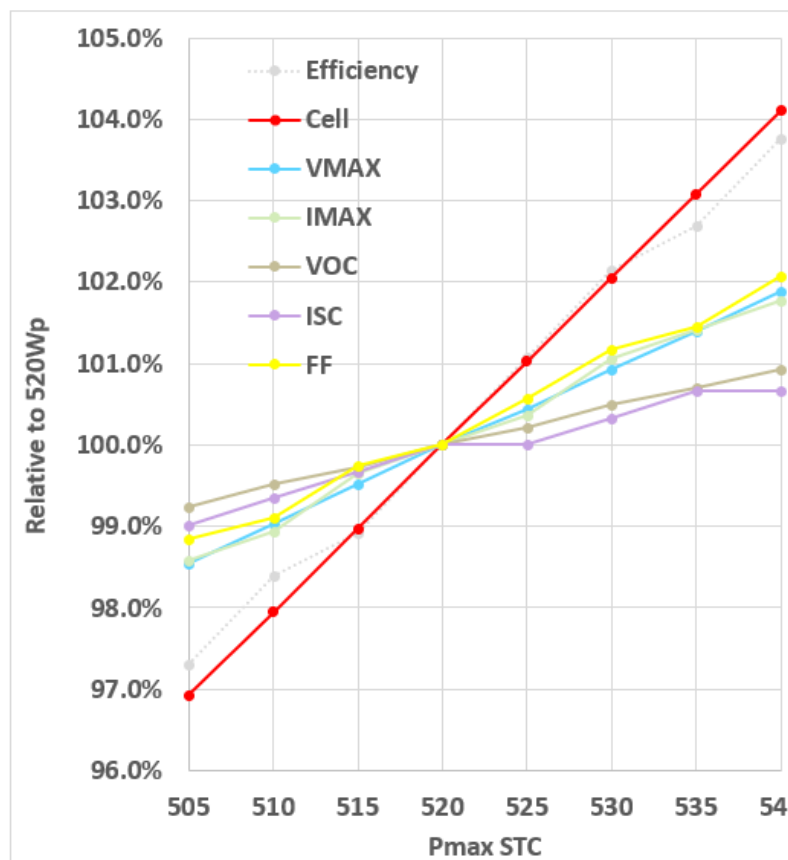
www.steveransome.com/pvpmc23.pdf



- SPARE

Why it's better to use normalised fit coefficients rather than measured

<https://www.firstsolar.com/-/media/First-Solar/Technical-Documents/Series-7/Series-7-TR1-Datasheet.ashx>



TYPES: FS-7XXXXA-TR1 (XXX = NOMINAL POWER) RATINGS AT STANDARD TEST CONDITIONS (1000W/m², AM 1.5, 25°C)2 Nom

TYPES: FS-7XXXXA (XXX = NOMINAL POWER)

AT	STANDAR TEST	CONDITIC (1000W/m ²								
AM	1.5,	25°C)2								
Power3	(-0/+5%)	PMAX	(W)	505	510	515	520	525	530	535
		Efficiency %		18.1	18.3	18.4	18.6	18.8	19	19.1
		Cell %		18.9	19.1	19.3	19.5	19.7	19.9	20.1
		VMAX (V)		182.5	183.4	184.3	185.2	186	186.9	187.8
		IMAX (A)		2.77	2.78	2.8	2.81	2.82	2.84	2.85
		VOC (V)		223.9	224.5	225	225.6	226.1	226.7	227.2
		ISC (A)		3.01	3.02	3.03	3.04	3.04	3.05	3.06
				100.10%	99.97%	100.20%	100.08%	99.91%	100.15%	100.04%
										99.94%

- PV production modules are put in power bins, e.g. First Solar with 8 bins from 505-540Wp.
- These have steadily increasing i_{sc} , i_{mp} , v_{mp} and v_{oc}
- One normalised coefficient algorithm can be fitted to all bins then extrapolated to new bins rather than needing separate coefficients each bin.
- Normalised coeffs are in a narrow range, so are easy to check.

steve@steveransome.com ; www.steveransome.com

IEC 61853 1-4 : <https://webstore.iec.ch/publication/6035>

MPM 1 : “Accurate module performance characterisation using novel outdoor matrix methods PVSC-48, 2021” http://www.steveransome.com/PUBS/2021_06_PVSC48_Florida_Ransome_210617t10_submitted.pdf%20VIRTUAL%20PVSC%2048%202021

MPM 2 : “Checking the new IEC 61853.1-4 with high quality 3rd party data to benchmark its practical relevance in energy yield prediction" PVSC-46, 2019” http://www.steveransome.com/PUBS/1906_PVSC46_Chicago_Ransome.pdf

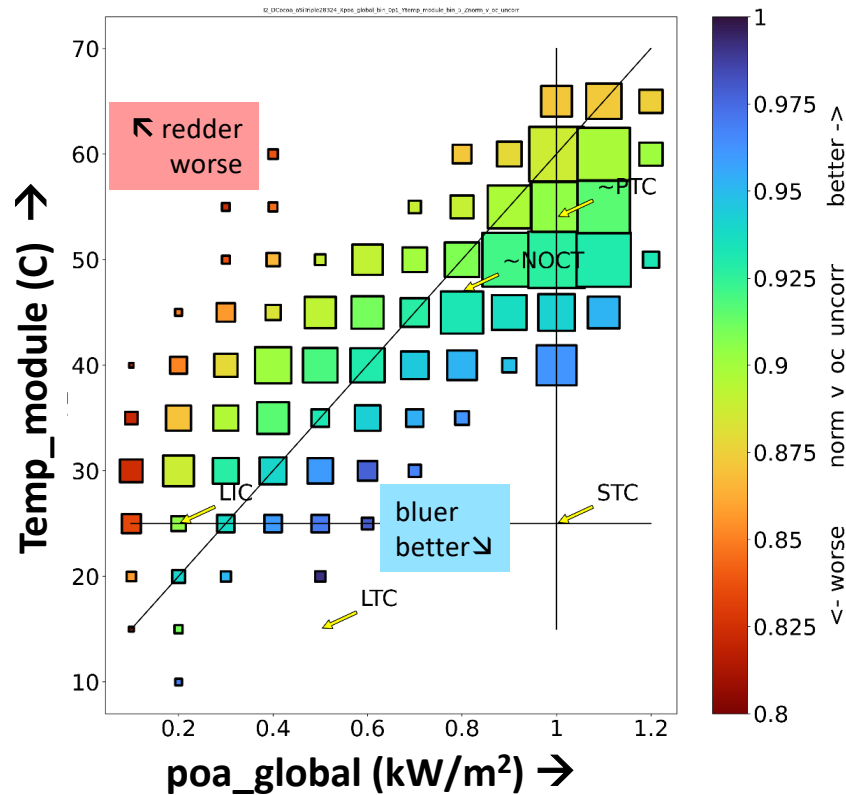
1-diode : W. De Soto et al., “Improvement and validation of a model for photovoltaic array performance”, Solar Energy, vol 80, pp. 78-88, (2006)

PVPMC : Holmgren, W. C. Hansen and M. Mikofski (2018).

“pvlib Python: A python package for modeling solar energy systems.” Journal of Open Source Software 3(29):884.

https://www.researchgate.net/publication/327525177_pvlib_python_a_python_package_for_modeling_solar_energy_systems

Improved matrix performance plot (with four independent parameters)



color = chosen parameter

blue=best performance

green = middle

red=worst performance

Area of squares :

α insolation H (kWh/m²/y)

- Some standard conditions are marked e.g. STC, NOCT
- Area shows most important (large) vs. insignificant (very small) which may be outliers

Effects that determine shape of measurement matrix Module #5 c-Si

$$pr_dc = meas_eff / stc_eff = meas_p_max / stc_p_max / g_kW_m2$$

Performance at matrix points is dominated by 5 separate effects

