

# Getting more useful information from modelling of iv curves and matrix measurements

**Steve Ransome (SRCL, UK)**

**independent PV consultant**

[www.steveransome.com](http://www.steveransome.com)      [mailto: steve@steveransome.com](mailto:steve@steveransome.com)

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**Salt Lake City, USA..**

Existing modelling methods give reasonable energy yield estimates, but there are simple analysis methods that can be done to

- differentiate PV technologies (from  $r_{series}$ ,  $r_{shunt}$  etc.)
- partition PR losses into separate causes (e.g.  $v_{oc}$ ,  $r_{sc}$ )
- find what may be limiting performance (e.g.  $r_{oc}$  is high)
- calculate degradation rates for each loss factor under different weather conditions (e.g.  $r_{sc}$  fall causes higher degradation at low G)
- be able to suggest optimization targets (e.g. reduce  $r_{series}$ )

This talk suggests some improvements to modelling methods, normalizing of measurements, loss and graphical analysis

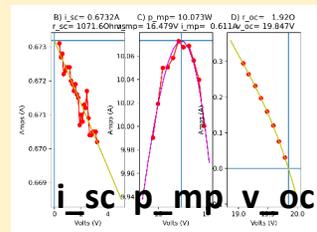
# Outdoor data used for this study

<https://www.nrel.gov/docs/fy14osti/61610.pdf>

- ✓ 11 modules of different technologies (CdTe, CIGS, aSi, 3JaSi, mcSi, scSi, HIT ...)
- ✓ Measured 3 sites FL, CO, OR for >1year
- ✓ ~180 IV points for curves each 5-15 mins
- ✓ Pyranometers for G\_POA, DHI, GHI, BNI
- ✓ Soiling, precipitation, RH (ignored here)
- ✓ Fits to  $i_{sc}$ ,  $i_{mp}$ ,  $v_{mp}$ ,  $v_{oc}$  were given

## However

- ✗ No windspeed
- ✗ No spectrum
- ✗ No  $r_{sc}$  or  $r_{oc}$  fits but calculated here →



## User's Manual for Data for Validating Models for PV Module Performance

W. Marion, A. Anderberg, C. Deline, S. Glick, M. Muller, G. Perrin, J. Rodriguez, S. Rummel, K. Terwilliger, and T.J. Silverman

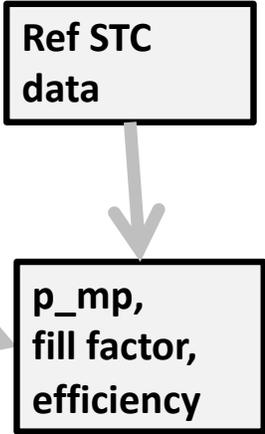
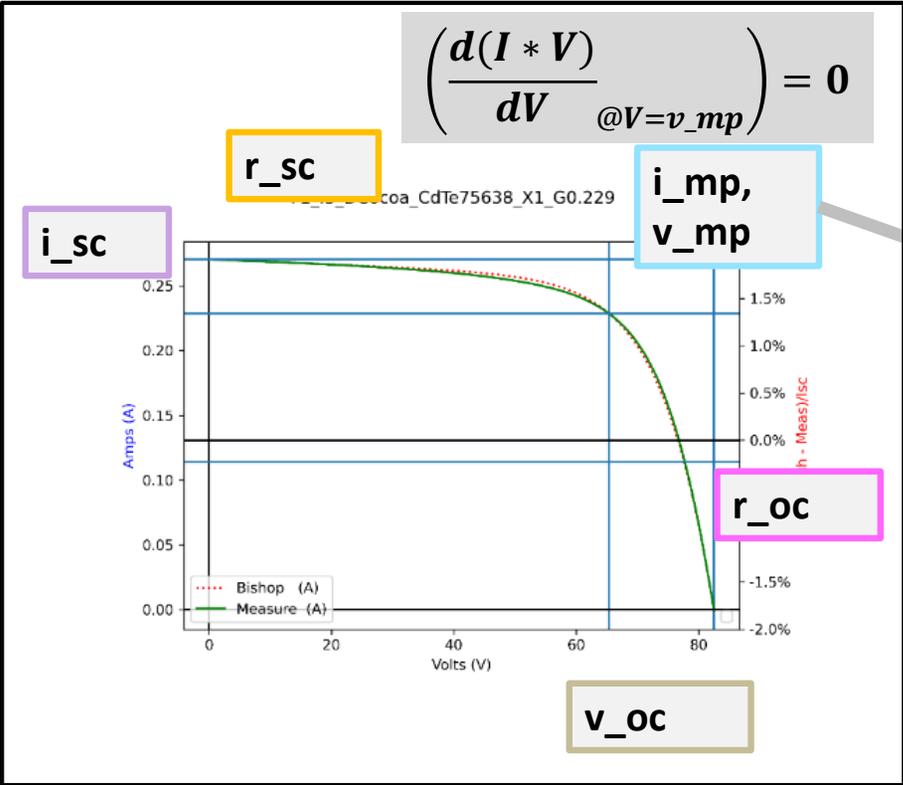
NREL is a national laboratory of the U.S. Department of Energy Office of Energy Efficiency & Renewable Energy Operated by the Alliance for Sustainable Energy, LLC

This report is available at no cost from the National Renewable Energy Laboratory (NREL) at [www.nrel.gov/publications](http://www.nrel.gov/publications).

Technical Report  
NREL/TP-5200-61610  
April 2014

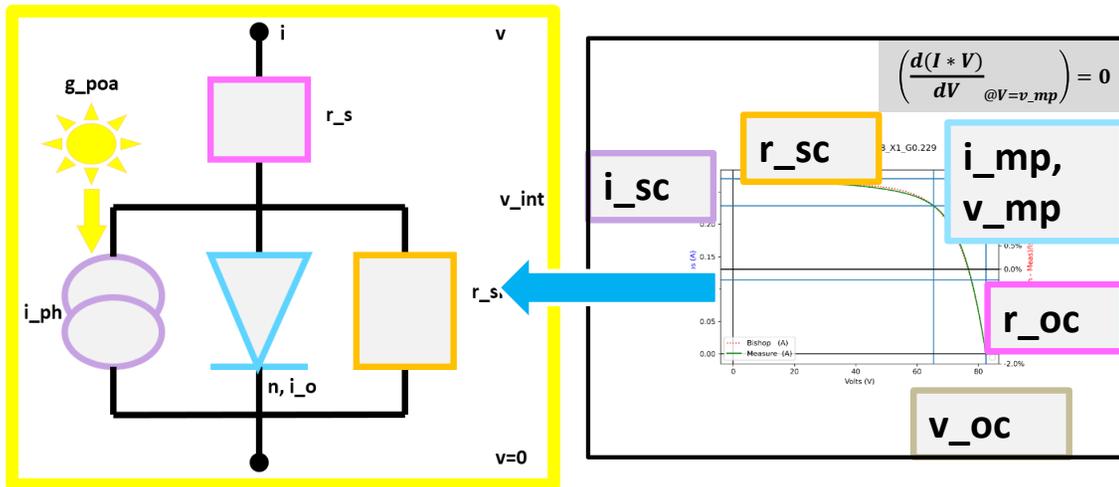
Contract No. DE-AC36-08GO28308

# Typical measured NREL IV curve with some fitted parameters (A, V, Ω, W)



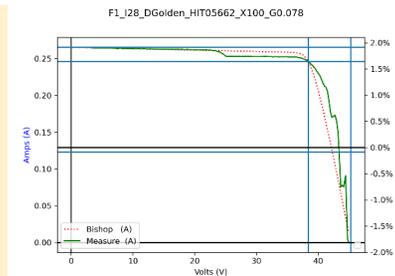
# IV curve → 1-diode model fit with 5 components

color shows which component 'dominates' each fit parameter



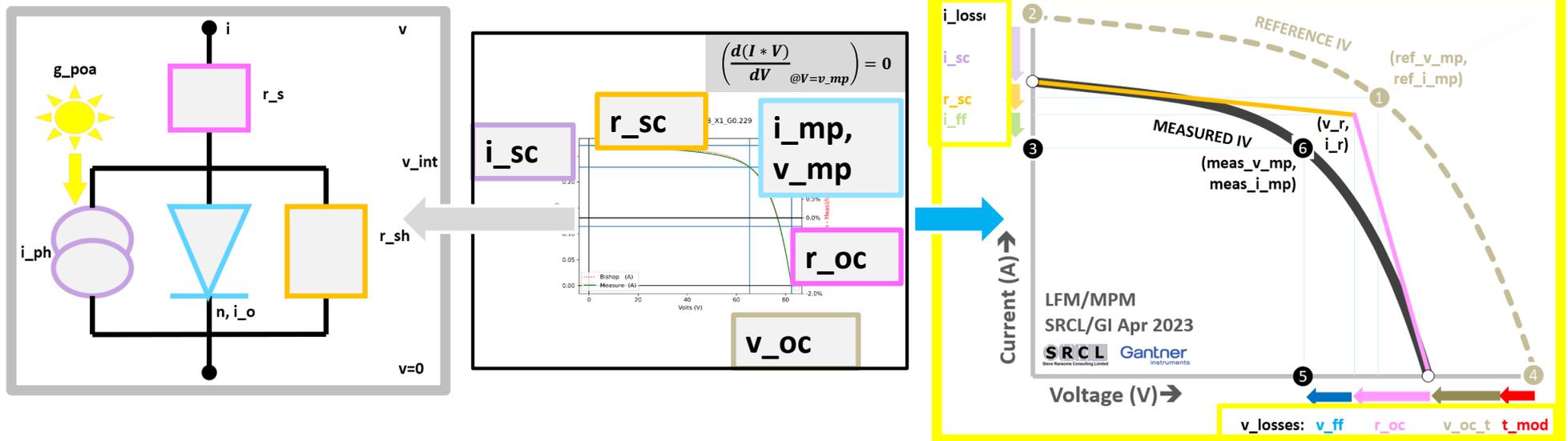
1-diode best fits to IV curves are limited by

- Point distribution : e.g. “poor  $r_{sh}$  fit if few near  $i_{sc}$ ”
- Differing fit algorithms, non-unique best fits
- “imperfections” mismatch, rollover, variable cloud during scan
- Note : 5 variables are insufficient to fit all IV curves perfectly



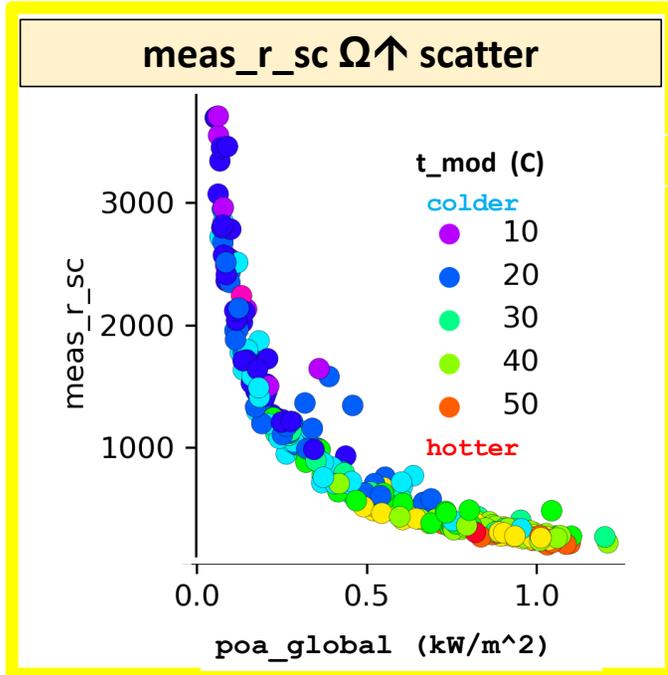
# IV Curve → MLFM\* fit with 6 normalised electrical and 1 temperature correction

\* mechanistic loss factors model

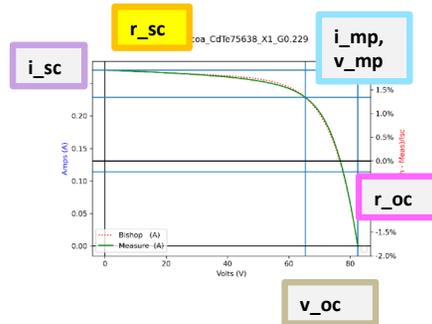


- 6+1 normalised losses from IV curve shape
- Characterise loss parameters vs. G, T and time

## Analysis of $r_{sc}(G, T)$



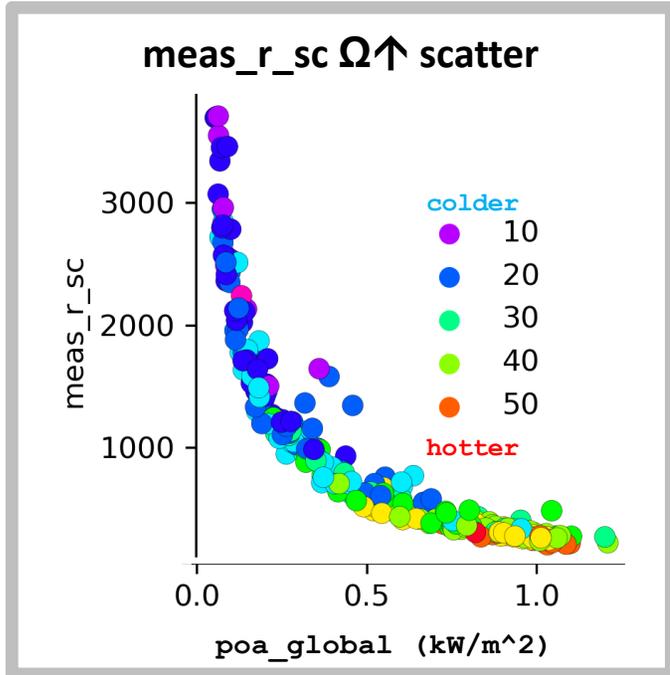
$$r_{sc} = -1 / \left( \frac{dI}{dV}_{@V=0} \right) \sim r_{shunt}$$



$r_{sc}$  vs.  $G$  is curved with a small -ve  $T$  sensitivity.  
 Most models assume  $r_{sc} = \text{constant}$  or  $r_{sc} \sim 1/G$   
 PVSYST has exponential fit

HIT module shown –  
 c-Si and thin films all have similar  
 shapes  
 (but differing values)

## Analysis of $r_{sc}(G, T)$



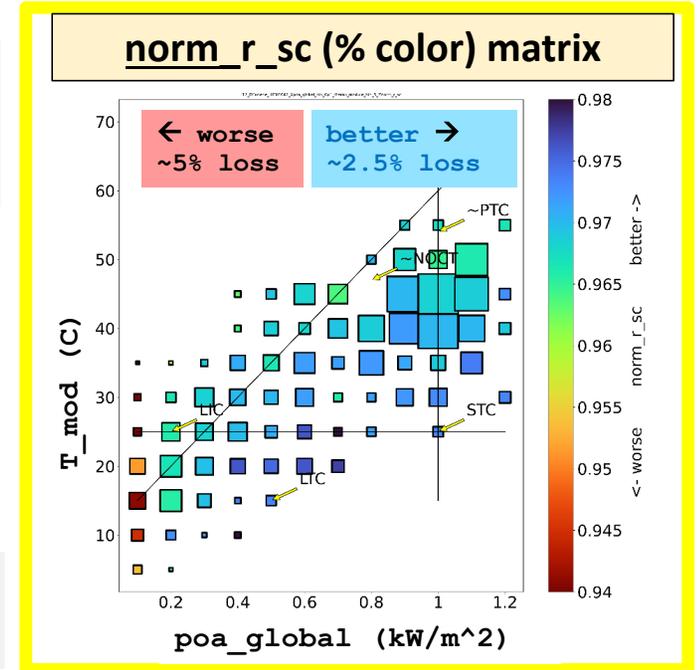
Similar fits can be done for any normalised parameters

Outdoor Matrix : has 50-100 useful G,T points

IEC 61853 (indoor) has ~28 (trying to reduce to ~6 for cost savings)

Square area proportional to Insolation ( $\text{kWh}/\text{m}^2/\text{yr}$ )

## Improved analysis of $r_{sc}(G, T)$



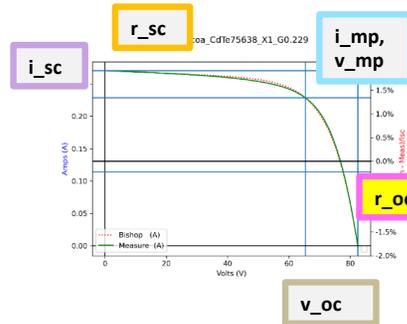
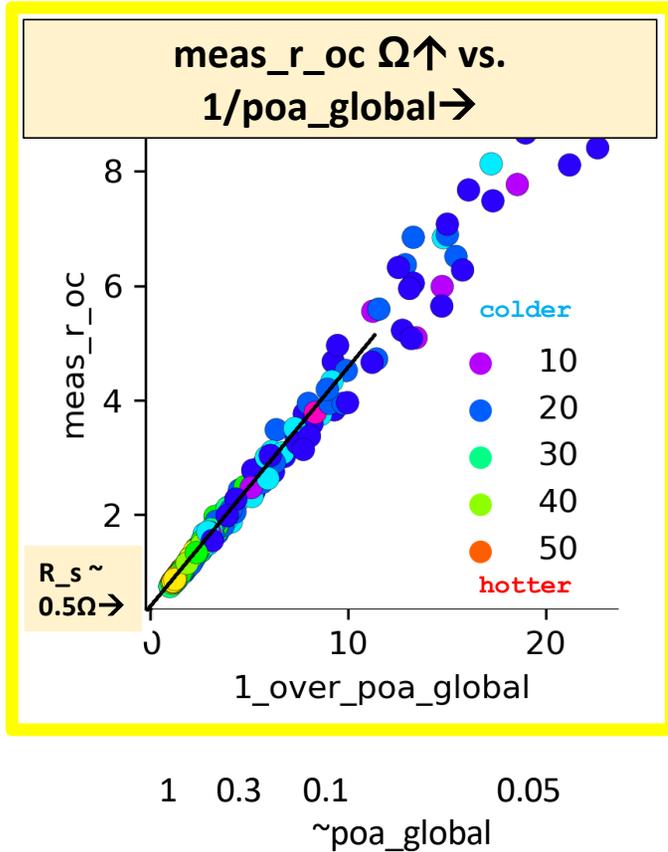
**MLFM Good fit to  $\text{norm}_{r_{sc}}(G, T)$**   
 Temperature coefficient from fit as  $c_{2t} \rightarrow$

$$\text{mlfm fit norm}_{r_{sc}} = c_{1c} + c_{2t} * (T - 25) + c_{3lg} * \text{LOG}_{10}(G) + c_{4g} * G$$

| mlfm      | c_1c  | c_2t   | c_3lg | c_4g  | rmse |
|-----------|-------|--------|-------|-------|------|
| norm_r_sc | 98.3% | -0.07% | 3.0%  | -0.3% | 1.1% |

| MLfm calcs | STC   | LIC   | NOCT  | HTC   |
|------------|-------|-------|-------|-------|
| norm_r_sc  | 97.4% | 95.6% | 96.4% | 95.4% |

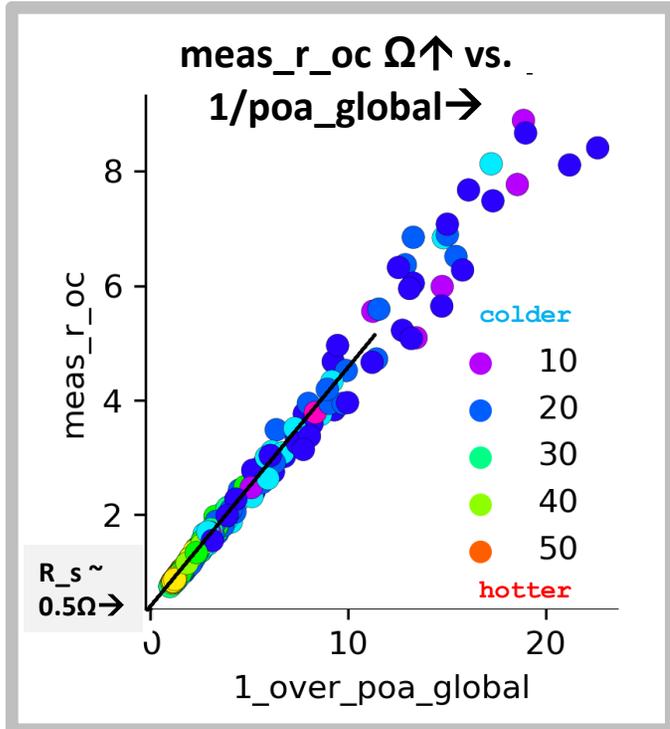
## Analysis of $r_{oc}(G, T)$



$$r_{oc} = -1 / \left( \frac{dI}{dV} \Big|_{I=0} \right) = r_s + fn(1/G)$$

- $r_{oc} \sim$  linear v.s  $1/G$ , extrapolates to  $r_s$  at  $1/G \rightarrow 0$
- Small Temp. coeff. depends on technology, usually
  - $d/dT(\text{norm}_{r_{oc}}) < 0$  for cSi (metal)
  - $d/dT(\text{norm}_{r_{oc}}) > 0$  for Thin films (TCO)
- Most models assume  $r_s(G, T) = \text{constant}$

## Analysis of $r_{oc}(G, T)$



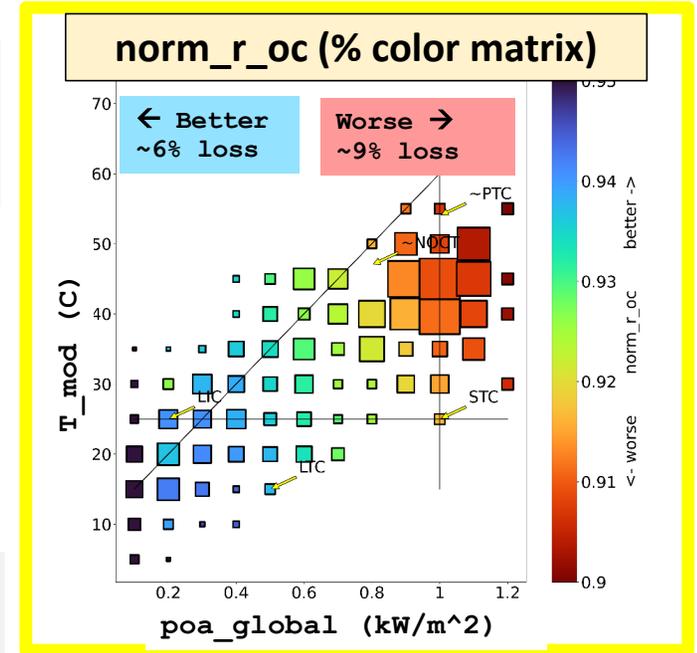
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Square area proportional to Insolation ( $\text{kWh/m}^2/\text{yr}$ )

## Improved analysis of $r_{oc}(G, T)$



**MLFM Good fit to norm  $r_{oc}(G,T)$**   
Temperature coefficient from fit as  $c_{2t}$  →

$$\text{mlfm fit norm}_{r_{oc}} = c_{1c} + c_{2t} * (T - 25) + c_{3lg} * \text{LOG}_{10}(G) + c_{4g} * G$$

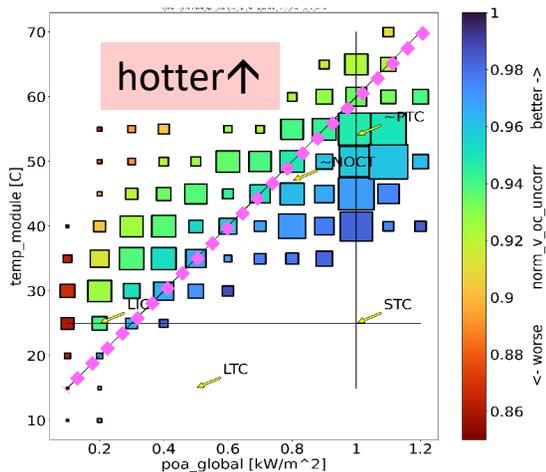
|           |       |        |       |       |      |
|-----------|-------|--------|-------|-------|------|
| mlfm      | c_1c  | c_2t   | c_3lg | c_4g  | rmse |
| norm_r_oc | 97.7% | -0.04% | 3.8%  | -6.3% | 1.5% |

|            |       |       |       |       |
|------------|-------|-------|-------|-------|
| MLfm calcs | STC   | LIC   | NOCT  | HTC   |
| norm_r_oc  | 91.4% | 93.8% | 91.5% | 89.4% |

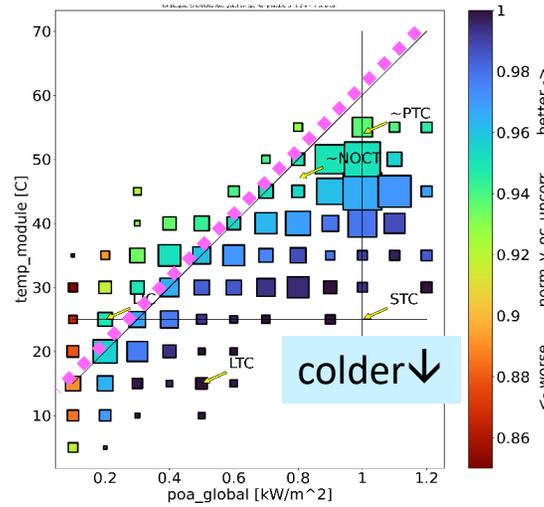
# Performance at different sites or times

(CdTe, norm\_v\_oc = color)

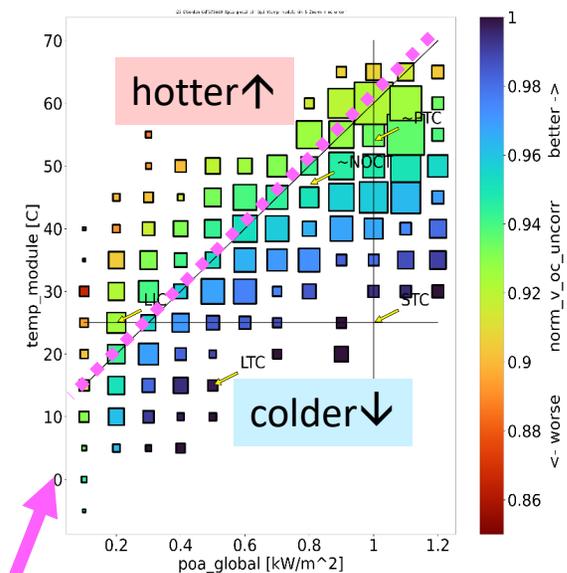
### A) COCOA FLORIDA (#1)



### B) EUGENE OREGON (#1)



### C) GOLDEN COLORADO (#2)



(Note: differing areas of squares from climates, distributions vs. temperature and irradiance)

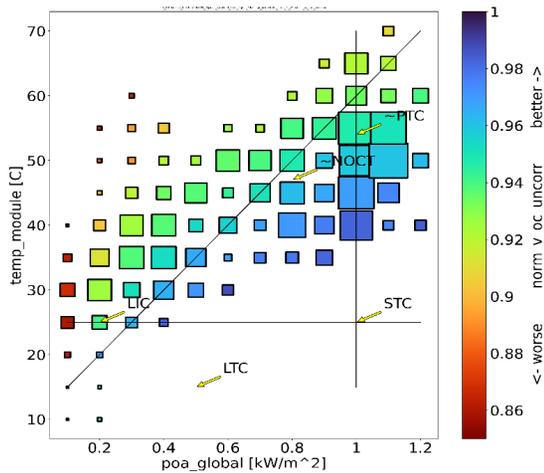
There are reference lines at  $G=1$ ,  $T=25$  and a pink diagonal from (0.1,15) to (1.2,70)

Lower coldest temperature at Golden than others

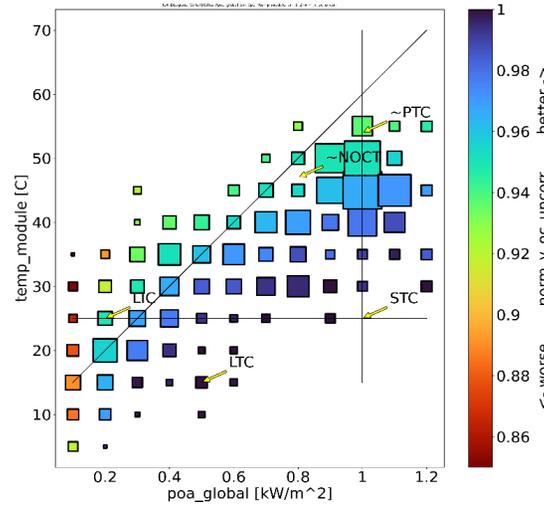
# Performance at different sites or times

(CdTe, norm\_v\_oc = color)

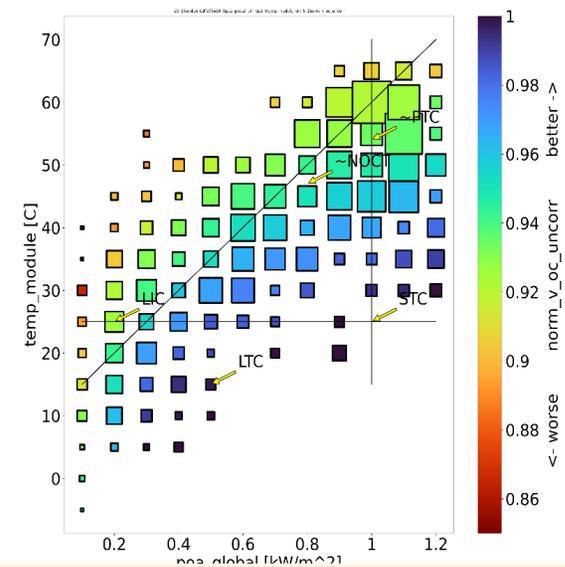
## A) COCOA FLORIDA (#1)



## B) EUGENE OREGON (#1)



## C) GOLDEN COLORADO (#2)



$$mlfm\ fit = c_{1c} + c_{2t} * (T - 25) + c_{3lg} * LOG_{10}(G) + c_{4g} * G$$

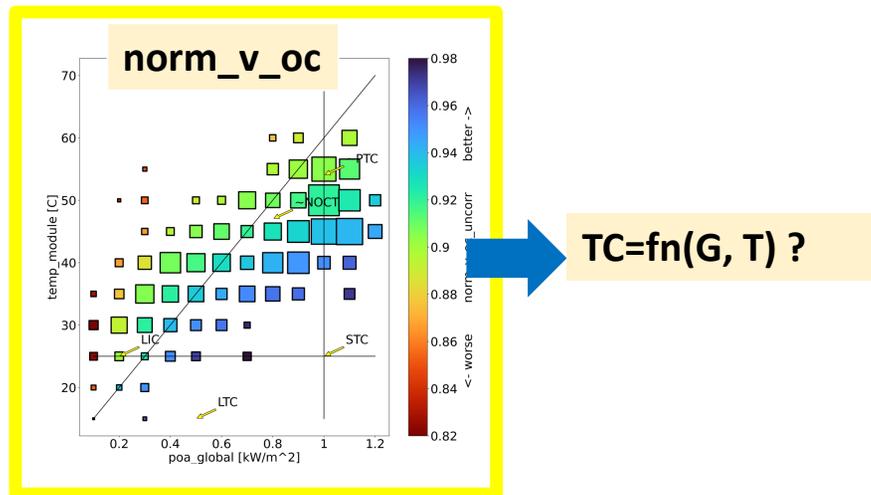
Any performance changes would show up in MLFM fit coefficients and values at given conditions e.g. STC

| State | Mod  | param     | c_1c   | c_2t   | c_3lg | c_4g  | rmse  | STC    | LIC   | NOCT  | HTC   |
|-------|------|-----------|--------|--------|-------|-------|-------|--------|-------|-------|-------|
| FL    | CdTe | norm_v_oc | 104.9% | -0.27% | 14.0% | -3.0% | 0.40% | 101.9% | 94.5% | 95.8% | 88.6% |
| CO    | CdTe | norm_v_oc | 102.3% | -0.25% | 11.6% | -1.9% | 0.39% | 100.4% | 93.8% | 94.6% | 87.9% |
| OR    | CdTe | norm_v_oc | 105.1% | -0.28% | 13.9% | -3.6% | 0.83% | 101.5% | 94.7% | 95.2% | 87.4% |

## Does the temperature coefficient vary $TC=fn(G, T)$ ?

e.g.  $\beta_{v_{oc}}(G, T) = 1/v_{oc\_STC} * \Delta v_{oc}/\Delta T$

- Most models assume Temperature Coefficients  $TC(G, T) = \text{constant}$
- Some manufacturers may provide valid ranges if they vary e.g. ">25C"
- This method with 50-100 points allows us to easily map a  $TC(G,T)$  from a normalised loss matrix

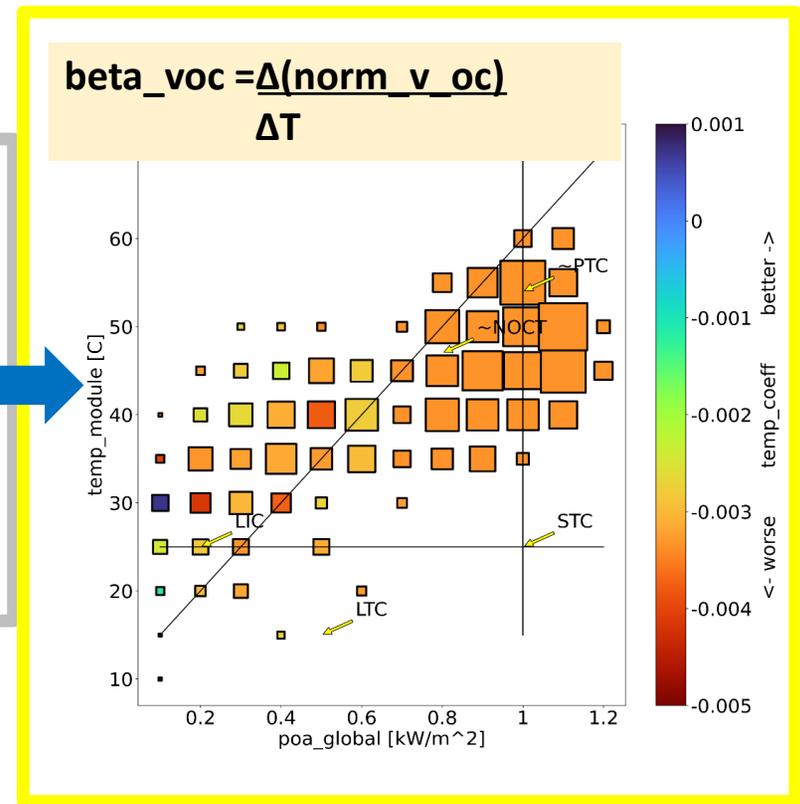
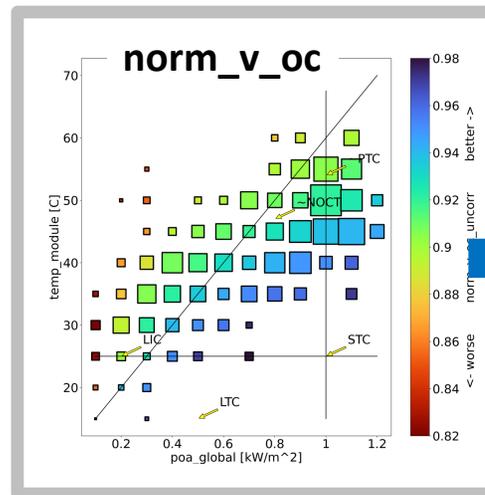


## Calculated Temperature coefficient $TC = f_n(G, T)$

$TC(G, T)$  = difference between adjacent temperature points  $\updownarrow$   
 mc-Si beta  $v_{oc} \sim -0.35\%/K$

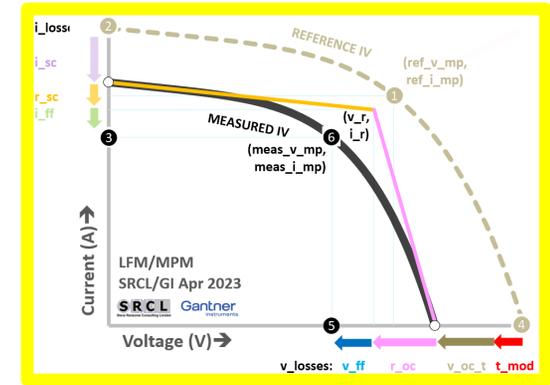
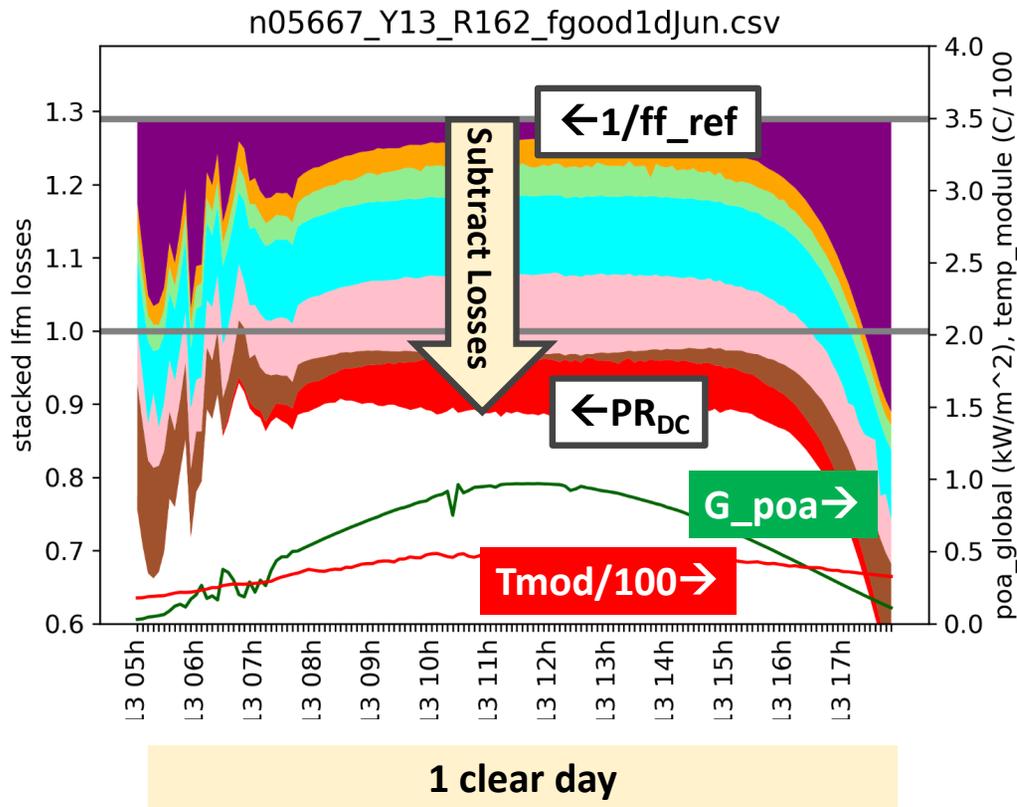
Some stable thin films have “non-constant temp coeffs” where warm autumn performance (after high temperatures) differs from cool spring (after cool weather)

Not yet tested on OPV, perovskite, dye or novel tandem



# What are the performance losses by type vs. G and T?

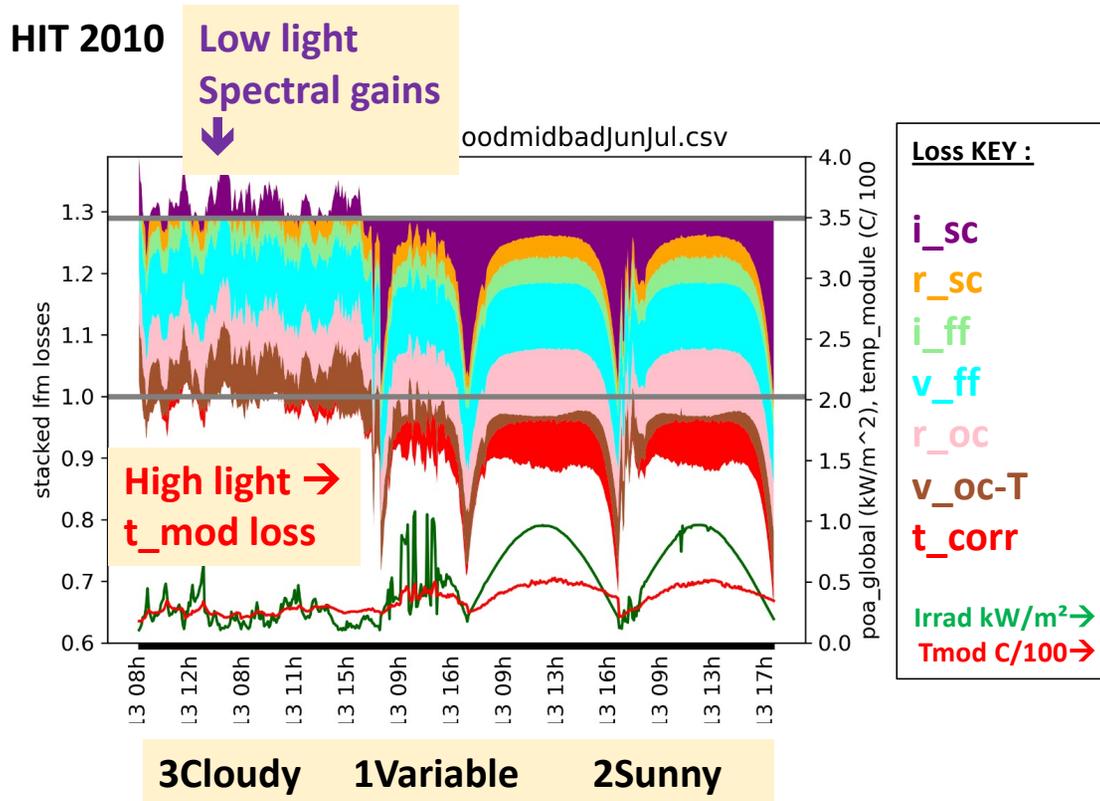
Subtract all 7 losses in turn from  $1/ff\_ref$  ↓ PR<sub>dc</sub>



**Loss KEY :**

|                    |                      |
|--------------------|----------------------|
| i <sub>sc</sub>    | (AOI, spectra, soil) |
| r <sub>sc</sub>    | (~Rshunt)            |
| i <sub>ff</sub>    | (fill factor I drop) |
| v <sub>ff</sub>    | (fill factor V drop) |
| r <sub>oc</sub>    | (~Rseries)           |
| v <sub>oc</sub> -T | (Voc temp corrected) |
| t <sub>corr</sub>  | (temp correct)       |

# Stacked losses under different weather conditions (no correction for reflectivity or spectral response from pyranometer)

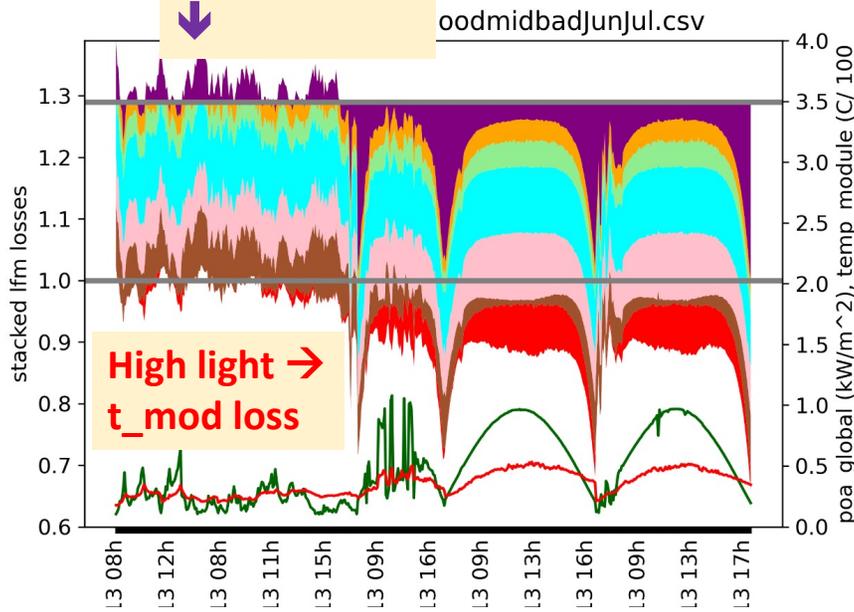


# Stacked losses under different weather conditions

(no correction for reflectivity or spectral response from pyranometer)

HIT 2010

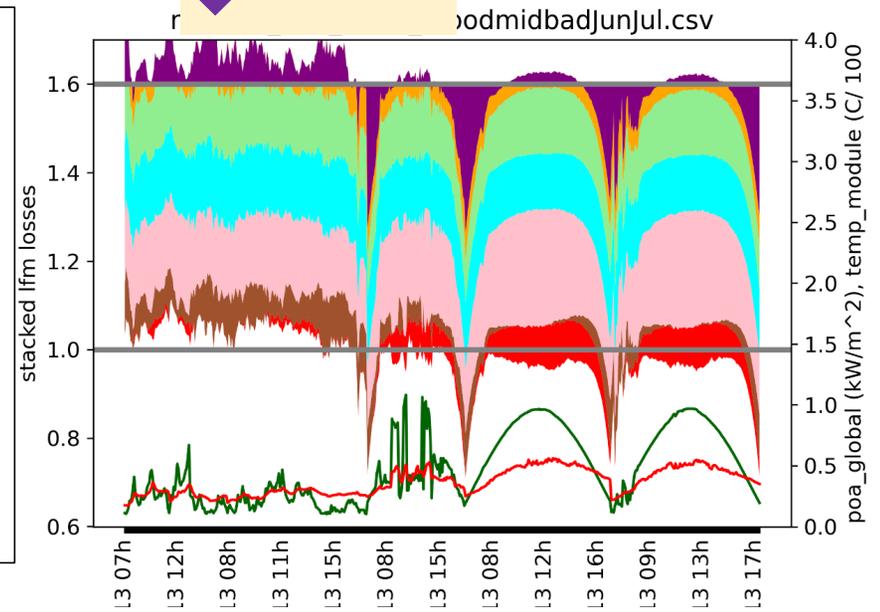
Low light  
Spectral gains  
↓



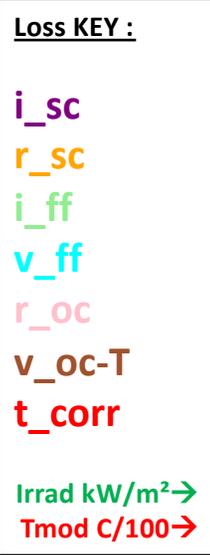
3Cloudy 1Variable 2Sunny

CdTe 2010

Low light  
Spectral gains  
↓



3Cloudy 1Variable 2Sunny

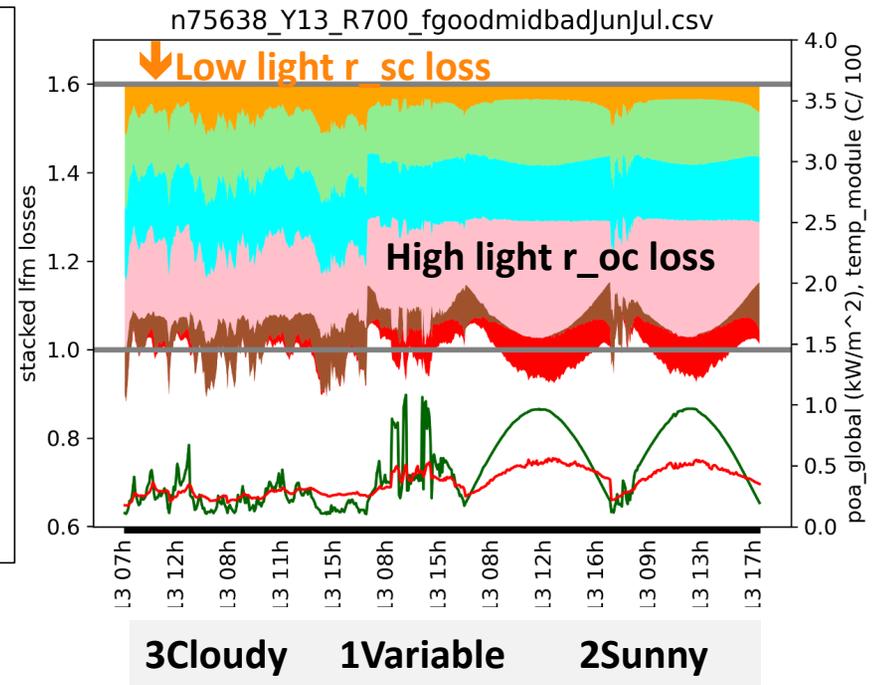
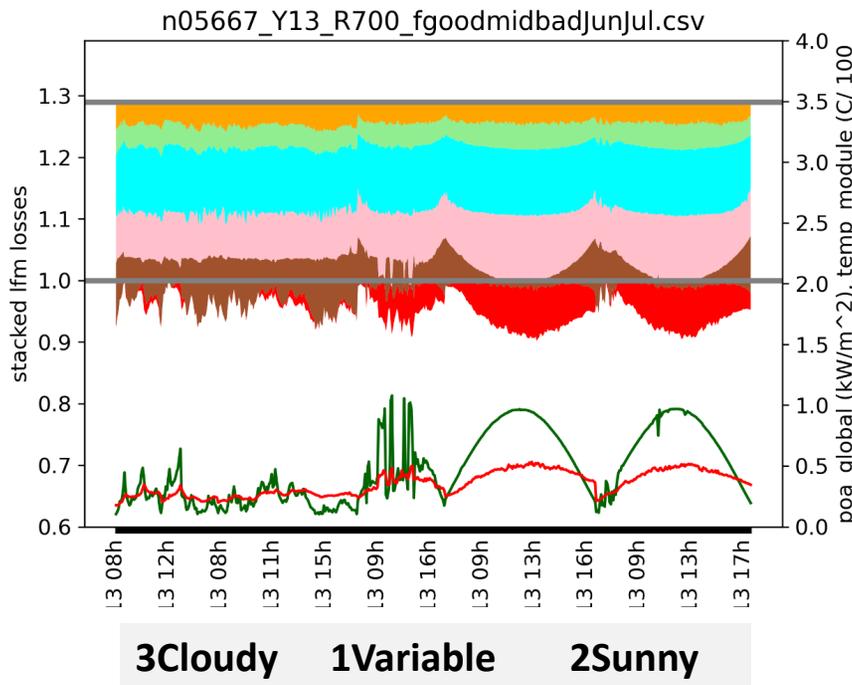


# Stacked losses under different weather conditions

– self referenced so easier to quantify other losses without  $i_{sc}$  errors

HIT 2010

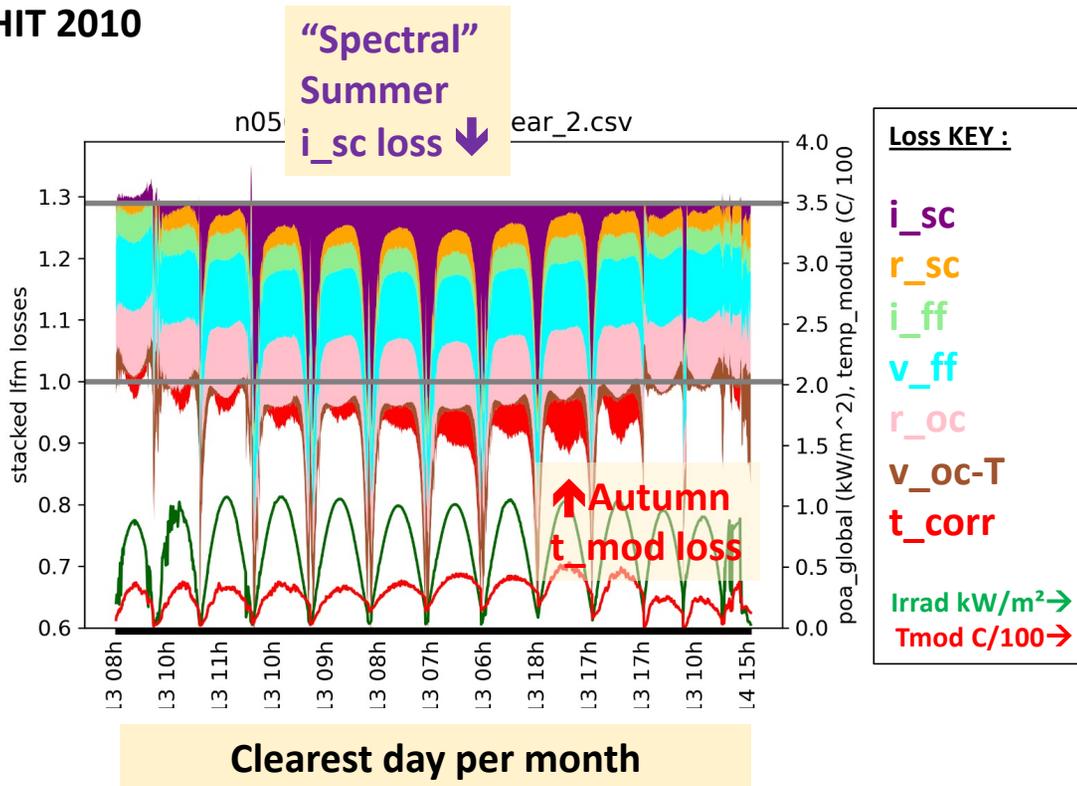
CdTe 2010



# Stacked losses “clearest day per month Dec – Dec” “stable modules”

- can show stepwise or continuous changes, seasonal astability or maybe sensor problems

HIT 2010

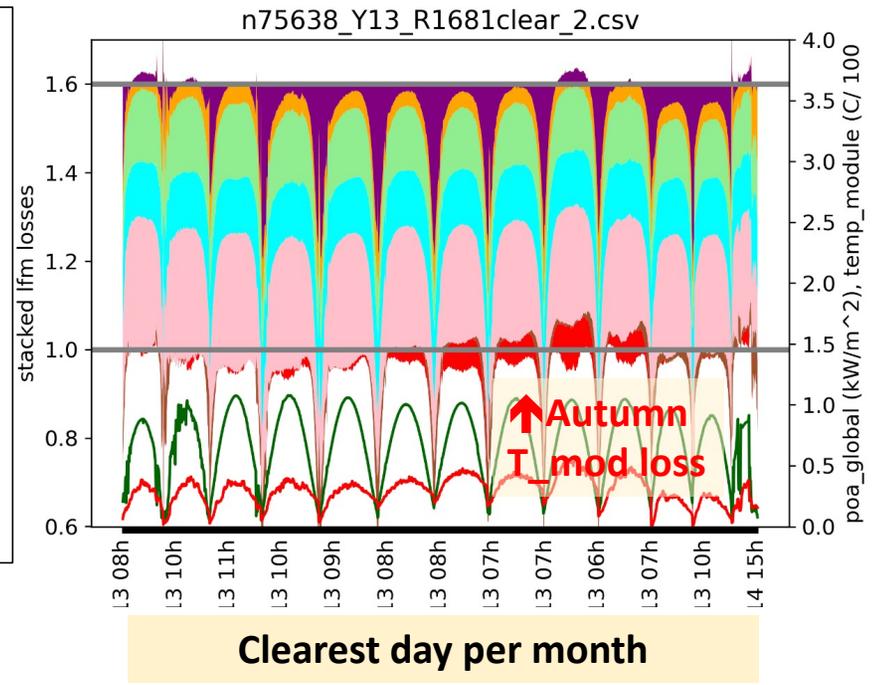
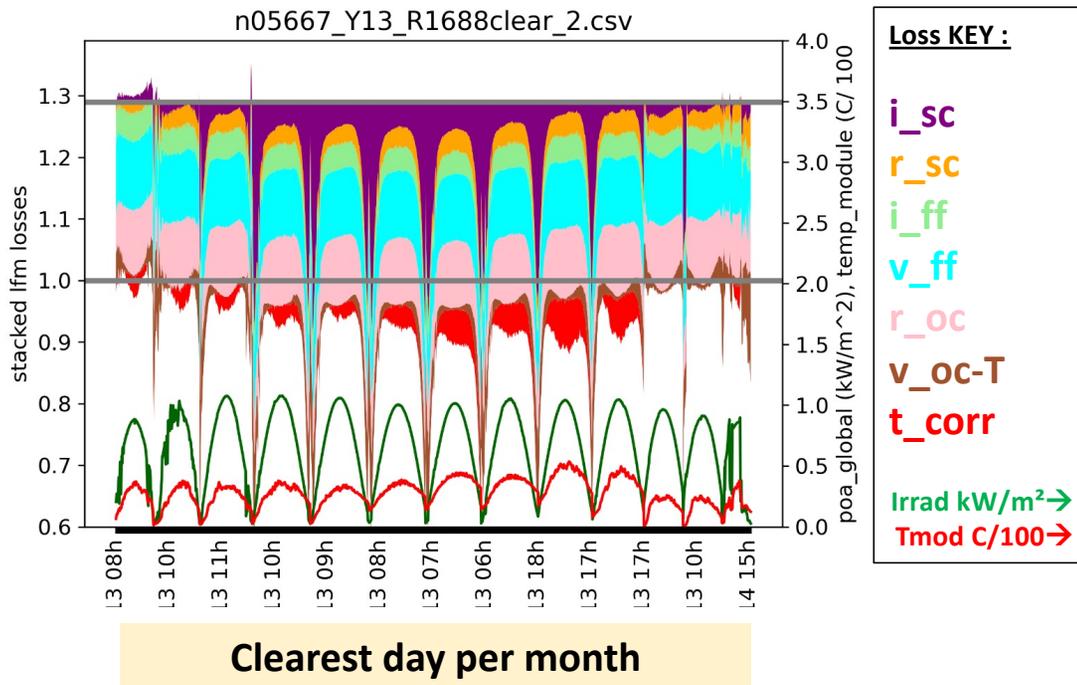


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HIT 2010

CdTe 2010

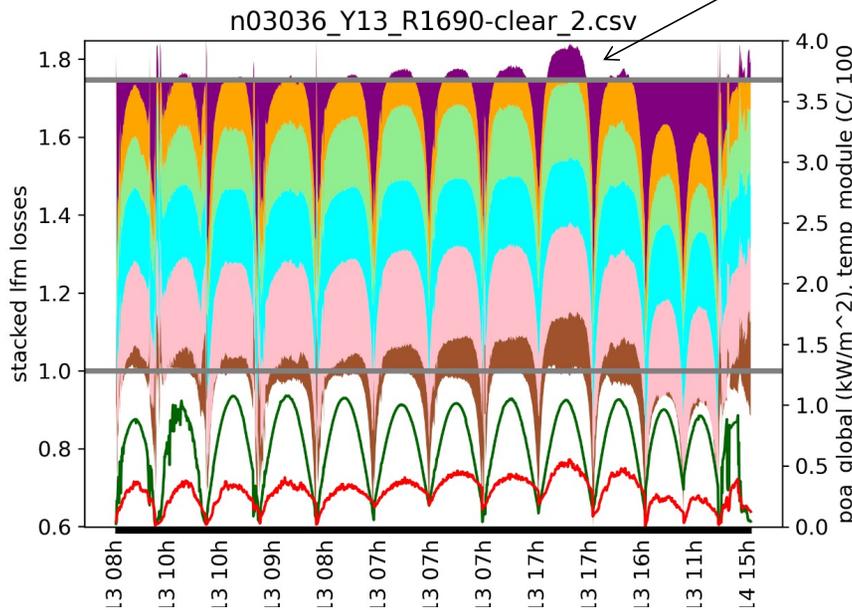


# Stacked losses “clearest day per month Dec – Dec” “unstable modules”

- show changes, seasonal astability, thermal annealing or maybe sensor problems

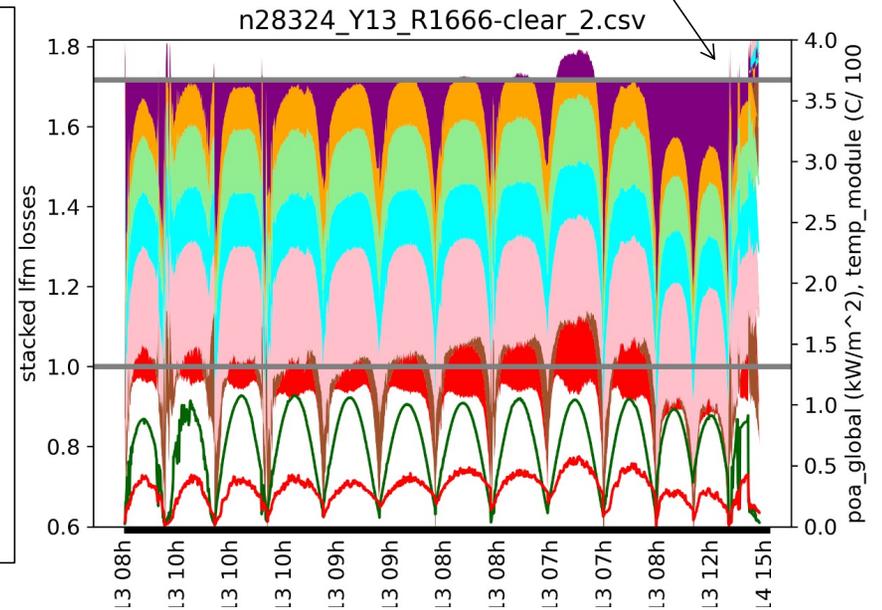
Atypical weather days? Thermal annealing? Spectrum?  
Soiling or sensor problems?  $i_{sc}$  worse but  $v_{oc}$  is better than other days

CIGS? 2010 Missing beta\_v\_oc



Clearest day per month

3J aSi? 2010 Beta\_v\_oc



Clearest day per month

**Loss KEY :**

- $i_{sc}$
- $r_{sc}$
- $i_{ff}$
- $v_{ff}$
- $r_{oc}$
- $v_{oc}-T$
- $t_{corr}$

Irrad kW/m<sup>2</sup> →  
Tmod C/100 →

# Conclusions

New methods have been shown using normalised loss factors to improve IV curve and matrix fits finding temperature and performance coefficients

Matrix plots (with areas ~ Insolation) are easiest to visualize and fit

Losses and causes help understand the behaviour vs. G,T and time

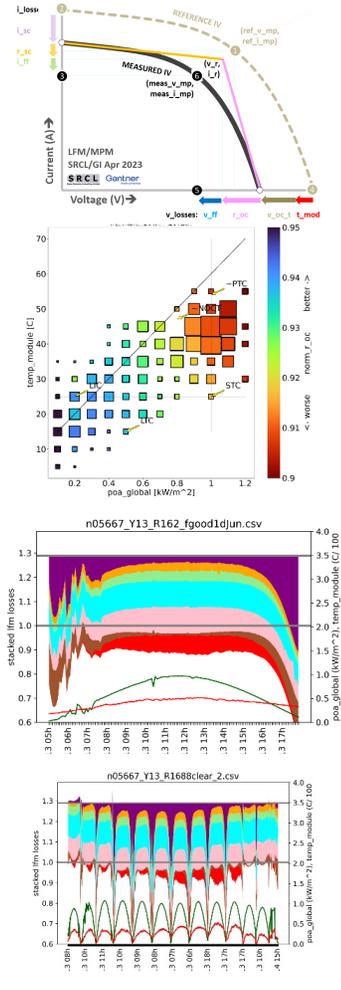
Relative performance of different PV technologies has been contrasted

Please contact me for more information [steve@steveransome.com](mailto:steve@steveransome.com)

Thank you for your attention!

Link to temporary version until it's published by SANDIA

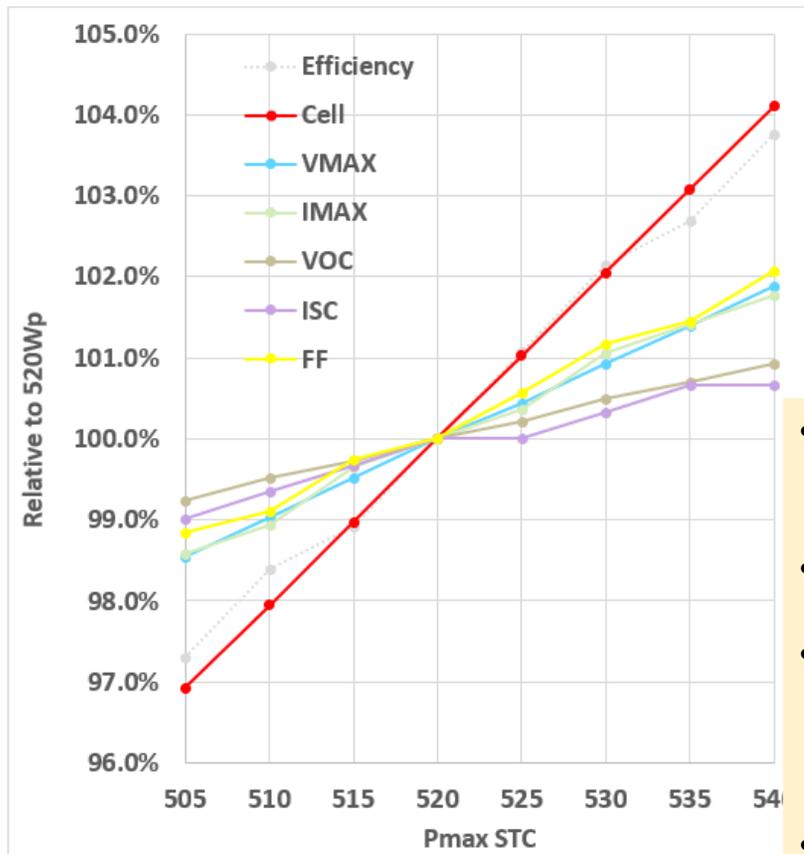
[www.steveransome.com/pvpmc23.pdf](http://www.steveransome.com/pvpmc23.pdf)



- SPARE

# Why it's better to use normalised fit coefficients rather than measured

<https://www.firstsolar.com/-/media/First-Solar/Technical-Documents/Series-7/Series-7-TR1-Datasheet.ashx>



TYPES: FS-7XXXXA-TR1 (XXX = NOMINAL POWER) RATINGS AT STANDARD TEST CONDITIONS (1000W/m<sup>2</sup>, AM 1.5, 25°C)2 Nom

TYPES: FS-7XXXXA (XXX = NOMINAL POWER)

| AT     | STANDAR TEST | CONDITIC (1000W/m <sup>2</sup> |         |        |         |         |        |         |         |        |
|--------|--------------|--------------------------------|---------|--------|---------|---------|--------|---------|---------|--------|
| AM     | 1.5,         | 25°C)2                         |         |        |         |         |        |         |         |        |
| Power3 | (-0/+5%)     | PMAX (W)                       | 505     | 510    | 515     | 520     | 525    | 530     | 535     | 540    |
|        |              | Efficiency %                   | 18.1    | 18.3   | 18.4    | 18.6    | 18.8   | 19      | 19.1    | 19.3   |
|        |              | Cell %                         | 18.9    | 19.1   | 19.3    | 19.5    | 19.7   | 19.9    | 20.1    | 20.3   |
|        |              | VMAX (V)                       | 182.5   | 183.4  | 184.3   | 185.2   | 186    | 186.9   | 187.8   | 188.7  |
|        |              | IMAX (A)                       | 2.77    | 2.78   | 2.8     | 2.81    | 2.82   | 2.84    | 2.85    | 2.86   |
|        |              | VOC (V)                        | 223.9   | 224.5  | 225     | 225.6   | 226.1  | 226.7   | 227.2   | 227.7  |
|        |              | ISC (A)                        | 3.01    | 3.02   | 3.03    | 3.04    | 3.04   | 3.05    | 3.06    | 3.06   |
|        |              |                                | 100.10% | 99.97% | 100.20% | 100.08% | 99.91% | 100.15% | 100.04% | 99.94% |

- PV production modules are put in power bins, e.g. First Solar with 8 bins from 505-540Wp.
- These have steadily increasing  $i_{sc}$ ,  $i_{mp}$ ,  $v_{mp}$  and  $v_{oc}$
- One normalised coefficient algorithm can be fitted to all bins then extrapolated to new bins rather than needing separate coefficients each bin.
- Normalised coeffs are in a narrow range, so are easy to check.

[steve@steveransome.com](mailto:steve@steveransome.com) ; [www.steveransome.com](http://www.steveransome.com)

**IEC 61853 1-4** : <https://webstore.iec.ch/publication/6035>

**MPM 1** : “Accurate module performance characterisation using novel outdoor matrix methods PVSC-48, 2021” [http://www.steveransome.com/PUBS/2021\\_06\\_PVSC48\\_Florida\\_Ransome\\_210617t10\\_submitted.pdf%20VIRTUAL%20PVSC%2048%202021](http://www.steveransome.com/PUBS/2021_06_PVSC48_Florida_Ransome_210617t10_submitted.pdf%20VIRTUAL%20PVSC%2048%202021)

**MPM 2** : “Checking the new IEC 61853.1-4 with high quality 3rd party data to benchmark its practical relevance in energy yield prediction" PVSC-46, 2019” [http://www.steveransome.com/PUBS/1906\\_PVSC46\\_Chicago\\_Ransome.pdf](http://www.steveransome.com/PUBS/1906_PVSC46_Chicago_Ransome.pdf)

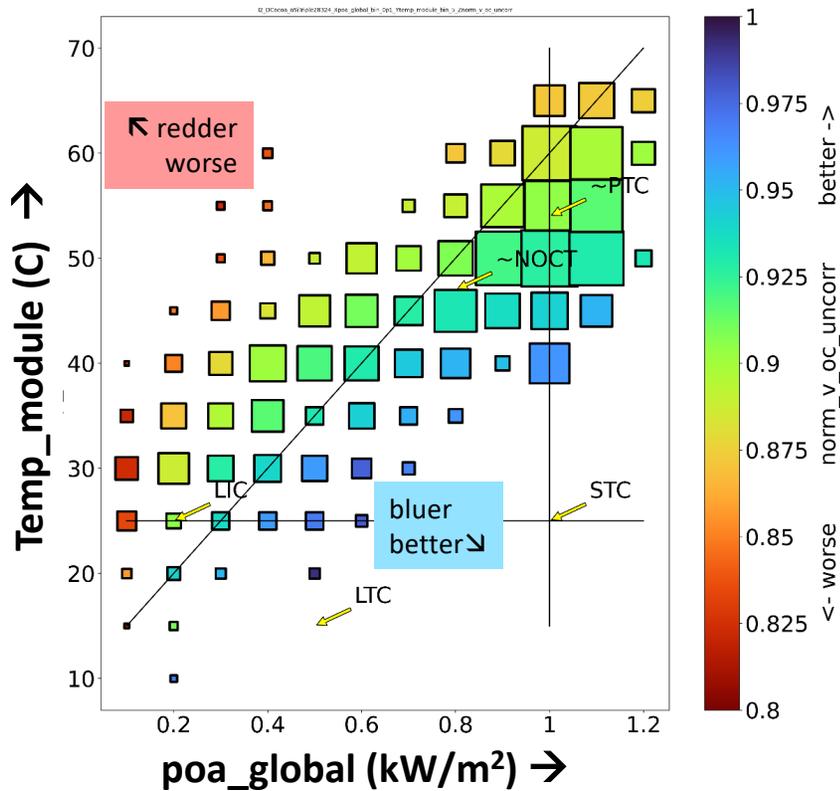
**1-diode** : W. De Soto et al., “Improvement and validation of a model for photovoltaic array performance”, Solar Energy, vol 80, pp. 78-88, (2006)

**PVPMC** : Holmgren, W. C. Hansen and M. Mikofski (2018).

“pvlib Python: A python package for modeling solar energy systems.” Journal of Open Source Software 3(29):884.

[https://www.researchgate.net/publication/327525177\\_pvlib\\_python\\_a\\_python\\_package\\_for\\_modeling\\_solar\\_energy\\_systems](https://www.researchgate.net/publication/327525177_pvlib_python_a_python_package_for_modeling_solar_energy_systems)

## Improved matrix performance plot (with four independent parameters)



color = chosen parameter

blue = best performance

green = middle

red = worst performance

Area of squares :

$\alpha$  insolation H (kWh/m<sup>2</sup>/y)

- Some standard conditions are marked e.g. STC, NOCT
- Area shows most important (large) vs. insignificant (very small) which may be outliers

# Effects that determine shape of measurement matrix Module #5 c-Si

$$pr\_dc = meas\_eff / stc\_eff = meas\_p\_max / stc\_p\_max / g\_kW\_m2$$

Performance at matrix points is dominated by 5 separate effects

