

# Shading mismatch loss calculation in PVsyst 6 

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## Near shadings: shading factor

"Near shadings" definition: the obstacles draw visible shades on the array


Definition of the Shading Factor :
Ratio of the Shaded area to the total sensitive area
(for a given sun's position)
Acts on the beam component

## PVsyst creates a

Table of shading factors for any direction of the space

| Shading factor table (linear), for the beam component |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Azimuth <br> Height | -180* | -160 | -140 | -120 | -100 ${ }^{\circ}$ | -80 | -60 | -40* | -20 ${ }^{\circ}$ | $0^{\circ}$ | $20^{\circ}$ | $40^{\circ}$ | $60^{\circ}$ | $80^{\circ}$ | $100^{*}$ | $120^{\circ}$ | $140^{\circ}$ | $160^{*}$ | $180^{*}$ |
| $90^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $80^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $70^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $60^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $50^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $40^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $30^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.008 | 0.003 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $20^{\circ}$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.088 | 0.057 | 0.070 | 0.026 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| $10^{\circ}$ | Behind | Behind | Behind | Behind | 0.000 | 0.000 | 0.033 | 0.471 | 0.314 | 0.191 | 0.172 | 0.071 | 0.017 | 0.057 | 0.083 | 0.083 | 0.000 | Behind | Behind |
| $2^{\circ}$ | Behind | Behind | Behind | Behind | Behind | 0.000 | 0.033 | 0.479 | 0.335 | 0.195 | 0.172 | 0.217 | 0.498 | 0.719 | 0.759 | 0.165 | Behind | Behind | Behind |

## Shading factor on diffuse

If we assume that the diffuse is isotropic
i.e. the received irradiance is identical whatever the direction of the space
(This is a reasonable hypothesis when considering the diffuse all over the year,
i.e. including covered weathers )
$\Rightarrow$ The shading factor for diffuse is calculated as an integral of the shading factor over all sky directions "seen" by the plane of the array (orange slice between the horizontal and collector planes)

This is independent on the sun's position and therefore:
$>$ constant over the year
(to be applied to the diffuse component at each simulation time step)
$>$ characteristic of the geometry of the system itself (not the latitude)
NB: This integral is computed using the shading factor table

## Shading factor on albedo

- Hypothesis: the albedo is from far ground reflexions $\Rightarrow$ if an obstacle is on the ground, no albedo from this direction
- By analogy to transposition models : albedo is proportionnal to the incidence angle of the ground for this given direction,
$\Rightarrow$ Shading factor on albedo = integral of this "ground shading factor" over the portion of sphere between the ground and the prolongation of the collector plane below ground

As for diffuse factor, this is independent on the sun's position, therefore:
> constant over the year
(to be applied to the albedo component at each simulation time step)
$>$ characteristic of the geometry of the system

NB: For rows arrangement the SF on albedo is $(n-1) / n \quad(n=n b$ of rows)

## Shading factor "according to strings"

Strong Hypothesis: when one cell of a string is shaded, the whole string becomes electrically inactive


Shading Factor "according to strings"
The array is partitioned into rectangles, each rectangle represents a full string (yellow)
SF according to strings = yellow + grey areas / total area
Acts on the beam component
"Linear" or "irradiance" losses: effect of grey areas Electrical losses:
effect of yellow areas (weighted by a parameter "Fraction for electrical shadings")

## Shading on one cell in a module

One cell shaded at $80 \% \Rightarrow$ the Isc of the cell drops by $80 \%$


By-pass diodes: derive the current in this sub-module
The I/V characteristics is about the same for 1 or several shaded cells

When the current exceeds Isc:
$\Rightarrow$ the cell is reverse-biased
$\Rightarrow$ the absorbed power becomes very high (hot spot)

$\Rightarrow$ We should treat each I/V curve at the sub-module level

## Shading on one cell in an array

One cell shaded in an array of 5 modules in series and 3 modules in parallel: 900 cells

Partial shadings on one cell - for an array of 3 strings of 5 modules


1 shaded cell : 0.09\% of cells => 3.5\% loss on Pmpp !

The Pmpp operating point is chosen by the inverter

The reverse current in the submodule may be very high

The string resulting I/V depends on the number of shaded sub-modules

## Module Layout definition

Calculation requires
positioning all modules (sub-modules)
on all shading areas defined in the 3D part

Modules may be automatically positioned:
in portrait/landscape orientation

- with specified spacing
- specified nb. of diodes in each module
- specify orientation of submodules



## "Irradiance" or "Linear" shading factor

The 3D calculation identifies the shading state of each corner of each sub-module
Sub-modules with 1 corner shaded: $25 \%$ shaded 2 corners shaded: 50\% shaded 3 corners shaded: $75 \%$ shaded
NB: $\Rightarrow$ little uncertainty on sub-modules of the shade border Resolution: with 6 " cells, 1 sub-module $\approx 0.5 \mathrm{~m}^{2}$


Linear Shading Factor $=\mathrm{Nb}$ of shaded sub-modules $/$ Total nb. of sub-modules

## Electrical shading calculation

Attribute each module to an electrical string
（i．e．to an inverter input）

| S Ster | ：S䝯： | ：St\＃ | $\because$ Ster | ：S斯： | S S ${ }^{\text {H }}$ | ：S ${ }^{\text {H }}$ | $\cdots$ S\＃ 6 | OS\＃ | S斯 | S严5． |  | ：S ${ }^{\text {Hef }}$ | S斯： | S斯： |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S Stu： | S斯： | －Still |  | S䢒了： | S Stus | S St4： | ： 5 \＃4： | S Ste | ：St4： | 澵4： | S\＃4： | S St⿱⿴⿱卄一二八斤5： |  | ：S斯： |
|  | ：S斯： | －Still |  | ：Stin： | $\cdots$ S期 | ：Stur | $\cdots$ ： \＃4：$^{\text {a }}$ | $\cdots$ ：St 4 | －544 1 | S農4． | 1st4： | $\cdots$ Ster | ：S | －St |
|  | St： | STIT | St | Stit： | St． | St． | $\cdots \mathrm{Sm}{ }^{\text {a }}$ | ：S\＃\＃ | 放2：1 | ：S\＃\＃： | S\＃2： | ：S\＃\＃？ | ： 5 \＃5］： | S\＃\＃ 5 |
|  | S其！ | S其！ | S其！ | Stit： | ST | ST | －S\＃2： | ［S\＃2． | Is\＃2： | ：S\＃\＃： | 䍻2： | －SH？ | －S\＃5 | －5\＃5： |
|  |  | 5 |  |  | 1 |  |  | 1 |  |  | 20 |  |  | 25 |

Here：Inv． 1
S\＃1，S\＃2，S\＃3
Inv． 2 S\＃4，S\＃5，S\＃6

Calculate the I／V curve for each input of each inverter：
－Add the voltage of each sub－module ＝＞I／V curve of each string
－Add the current of each string
＝＞inverter input＇s I／V curve
Calculate the Pmpp
Compare to unshaded Pmpp


## Detailed Shading Loss calculation

The calculation and interpretation involves the irradiance components in different ways :


Linear or Irradiance loss = Diffuse + Albedo + Beam losses (grey contributions)
Electrical shading loss = calculated as the balance of all these losses

## Simulation results



The "Module Layout" approach is suited for little systems ( say, < 50 kWp)
The shading calculation "according to strings" should be used for big systems. (It will produce an array "electrical loss" contribution in the same way).

Comparing results of both methods allows a determination of the "Fraction for electrical shadings" involved in the strings approach

## Application: Sheds (rows) arrangement

Relevant parameters:

- plane tilt
- Limit Angle
- GCR = Width / Pitch



Shading factor on diffuse: depends on the geometry only!

Factor independent on Latitude Loss = Diffuse • Factor dependent on the climate (due to Diffuse/Global ratio)

## Losses contributions in Sevilla

Example: Sevilla (Spain) :
Glob $_{\text {horiz }}=1750 \mathrm{kWh} / \mathrm{m}^{2} /$ year
$D / G$ ratio $=36 \%$

Albedo: prop. to $(1-\cos$ Ta) / 2 $\approx$ Completely lost: $\mathrm{SF}=(\mathrm{n}-1) / \mathrm{n}$

Diffuse : SF applies on D/G


"Linear" on beam: low contribution < 10\%
Electrical loss (applies on beam):
2 strings in width: low contribution

## Electrical loss in sheds

Different string layouts with 4 modules in width :

Case A


Case B


Case D


As soon as $1 / 3$ of sub-modules shaded $\Rightarrow$ the string is electrically inactive $\Rightarrow$ "Fraction for electrical loss" $=100 \%$


|  |  | Calculation mode |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{\|c\|} \hline \text { Linear } \\ \text { shadings } \end{array}$ | "Acc to strings" | Module layout | Submod bottom |
| Case A | 3.40\% | 0.43\% | 0.41\% | 33\% |
| Case B | 3.40\% | 0.92\% | 0.69\% | 17\% |
| Case C | 3.40\% | 1.50\% | 0.61\% | 8\% |
| Case D | 3.40\% | 0.92\% | 1.04\% | 100\% |

Calculation in "Module strings" mode:

- Case A and D: fits correctly
- Case B and C: not all submodules shaded at a time => Fractions for electrical loss < 100\%


## Conclusions

- The shading calculation is based on a geometrical calculation for Beam
- Model for applying to Diffuse and Albedo components ( $\Rightarrow$ assumptions)
- Electrical mismatch only applied to the Beam component
- Module Layout: calculation at the sub-module level, for each inverter input
- 2 ways of calculating the electrical loss:

According to String to be used for big systems
Module layout suited for "little" systems (< $\approx 50 \mathrm{kWp}$ )

- "Fraction for electrical loss" may be estimated on little parts of the system
- Model uncertainties: more important on diffuse/albedo estimation than on the electrical calculations

