

## CIGS Performance Analysis: Alternative Method to Fit the Sandia Array Performance Model

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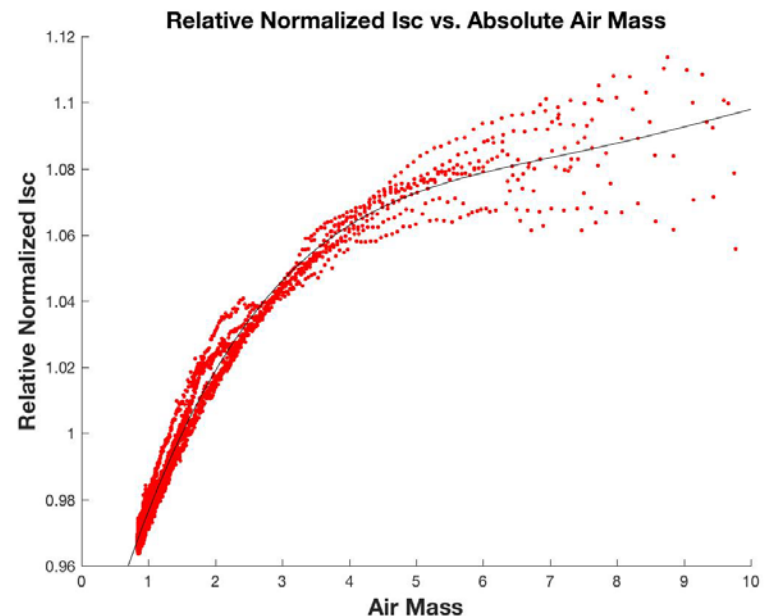
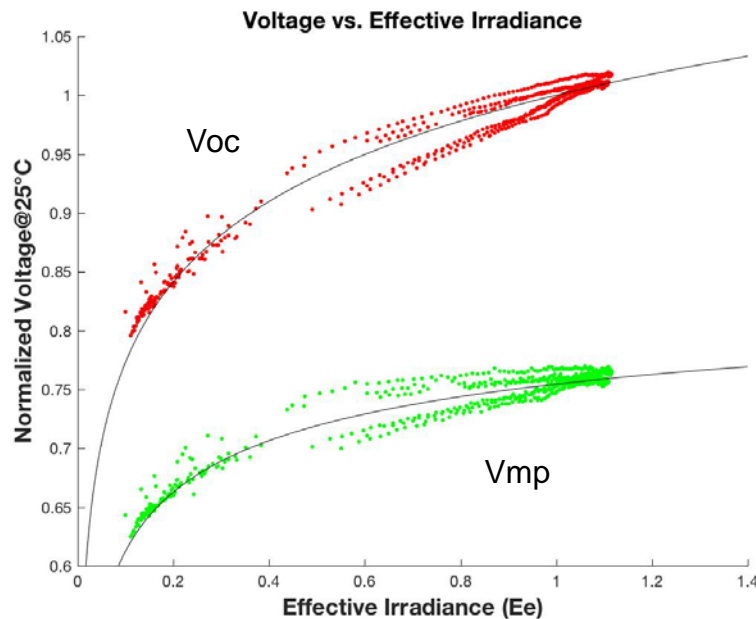
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# Outline

1. Challenges to Measuring and Modeling CIGS Performance
2. Overview of Outdoor Performance Measurements and Sandia Array Performance Model (SAPM)
3. Alternative Method to Fit SAPM
4. Summary

# Challenges to Measuring and Modeling CIGS Performance

- Metastable performance
  - Modules may require 10's of hours of operation at  $1000 \text{ W/m}^2$  to reach steady-state performance conditions
  - May be sensitive to operating temperature
  - Performance stabilization may reverse after storage in the dark (or overnight?)
- Parameters reported to be sensitive to metastability include  $V_{oc}$ ,  $V_{mp}$ , fill factor and temperature coefficients
- Spectral response is not the same as c-Si – accurate performance models need air mass modifiers



# Outdoor Module Characterization at Sandia

Outdoor characterization is performed on a flexible, fully programmable two-axis solar tracker.

Range of Technologies; flat plate, CPV, etc.

## Instrumentation

- Calibrated Silicon Reference Cell
- Calibrated Precision Spectral Pyranometer
- Custom IV sweep hardware and software

Electrical performance test (IV curves) measured at 2 minute intervals

- Sunrise to sunset, multiple days
- Clear and Cloudy conditions
- Approximately 1000 IV curves minimum

Thermal test to determine temperature coefficients for  $I_{sc}$ ,  $I_{mp}$ ,  $V_{oc}$  and  $V_{mp}$

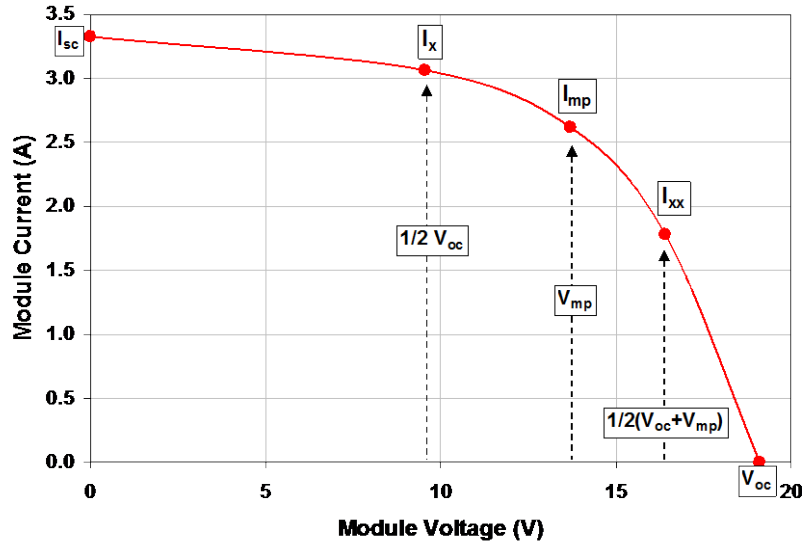
Angle of incidence (AOI) response

Characterization takes approximately two weeks

- Exact length of testing depends on local weather conditions



# Sandia Array Performance Model (SAPM)



$$I_{sc} = I_{sco} f_1(AM) \left[ \frac{E_b f_2(\theta) + f_d E_{diff}}{E_0} \right] [1 + \alpha_{Isc} [T_c - T_0]]$$

$$E_e = \frac{I_{sc}}{I_{sco} [1 + \alpha_{Isc} [T_c - T_0]]}$$

$$I_{mp} = I_{mpo} [C_0 E_e + C_1 E_e^2] [1 + \alpha_{Imp} [T_c - T_0]]$$

$$\delta(T_c) = \frac{nk[T_c + 273.15]}{q}$$

$$V_{oc} = V_{oco} + N_s \delta(T_c) \ln(E_e) + \beta_{Voc} [T_c - T_0]$$

$$V_{mp} = V_{mpo} + C_2 N_s \delta(T_c) \ln(E_e) + C_2 N_s [\delta(T_c) \ln(E_e)]^2 + \beta_{Vmp} [T_c - T_0]$$

$$I_x = I_{xo} [C_4 E_e + C_5 E_e^2] [1 + \alpha_{Isc} [T_c - T_0]]$$

$$I_{xx} = I_{xxo} [C_6 E_e + C_7 E_e^2] [1 + \alpha_{Imp} [T_c - T_0]]$$

Semi-empirical model that defines five points on the IV curve

## Inputs

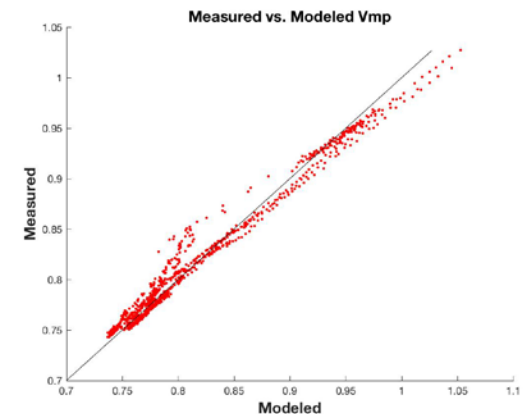
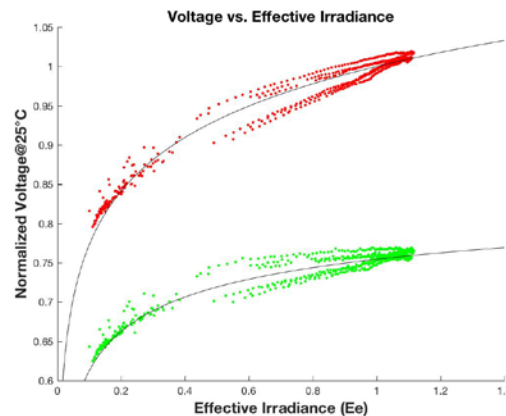
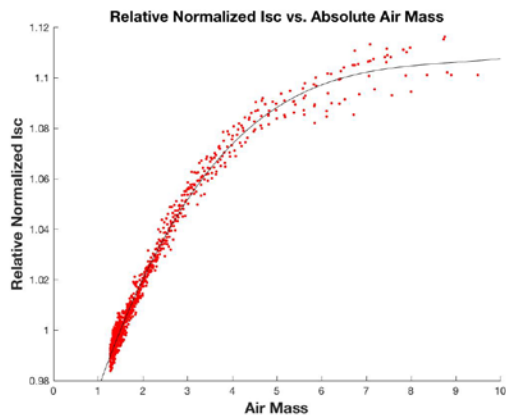
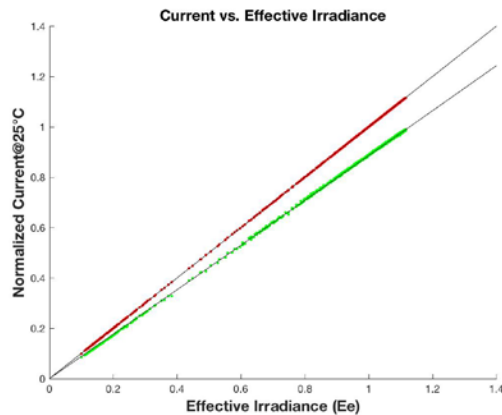
- Measured I-V curves from outdoor testing
- Thermal performance of cell
- Angle of Incidence (AOI) response of module

Coefficients can be used with PV\_Lib, SAM and other modeling packages to predict system performance

Standard method of determining coefficients utilizes stepwise filtering and regression analysis to progressively solve each equation

# And the problem.....

- Applied to a prototype CIGS module, the standard analysis method fails
- Calibrated model does not predict measured data used to calibrate the model
- Temperature corrected data appears to “split” between morning and afternoon
- Terms involving current look good, suggests the problem lies with module voltage



# The Suspected Culprit - Temperature Coefficients: Sandia's Method (in use for nearly 2 decades)

- Module is instrumented with temperature sensors and the back of the module is thermally insulated to improve temperature uniformity.
- Module is then covered with an opaque sheet and allowed to cool to ambient temperature.
- Once at ambient, the cover is removed and IV curves and module temperatures are measured rapidly (~ 2 samples per minute) while the module heats up to an equilibrium temperature.
- Temperature coefficients are determined from linear regression analysis
- A typical test requires approximately 30 minutes once the cover has been removed.
- Consistent with international standards (IEC 60891, 61853)
- Inherently transient

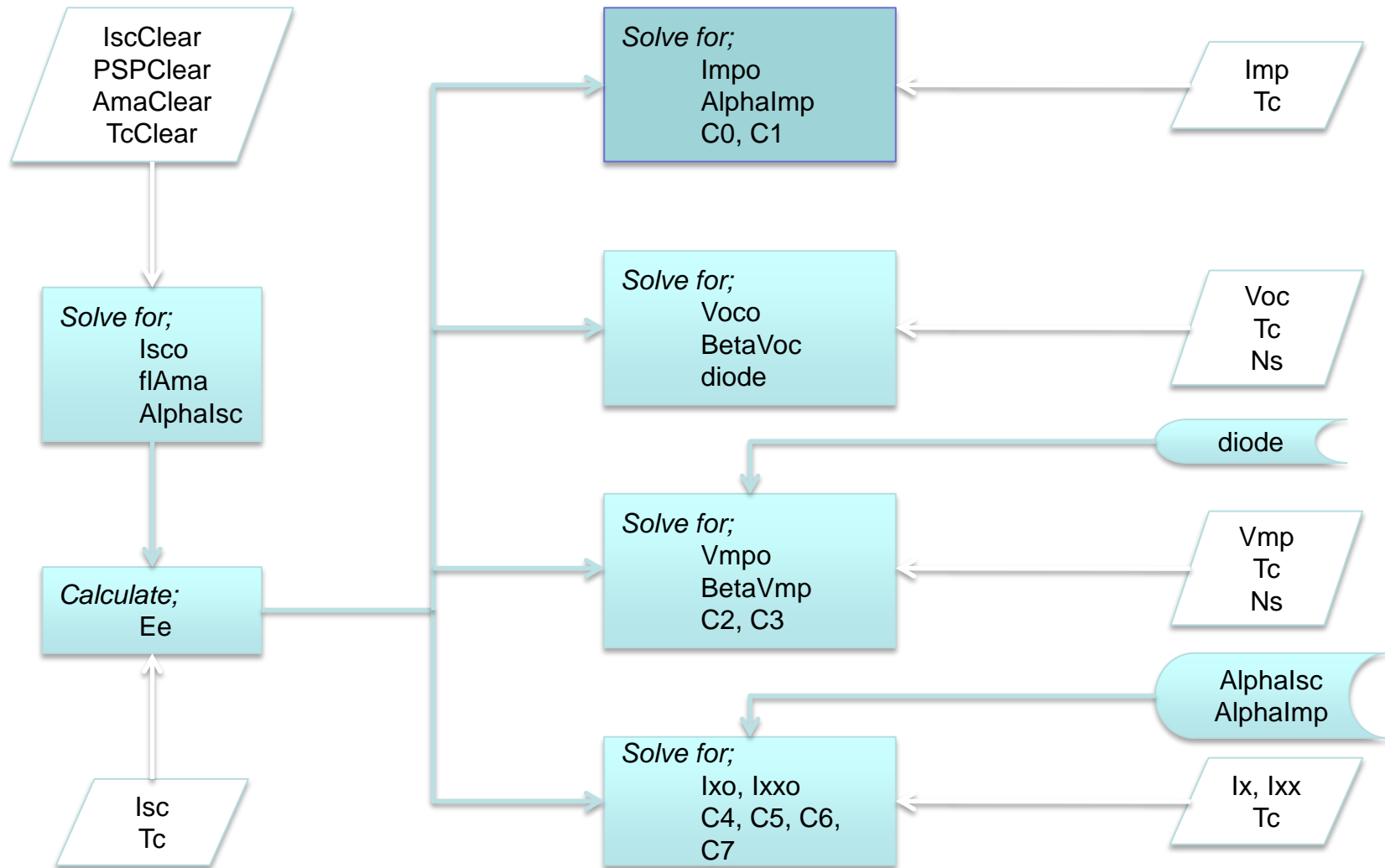


# The Solution - Alternate Method to Determine Model Coefficients

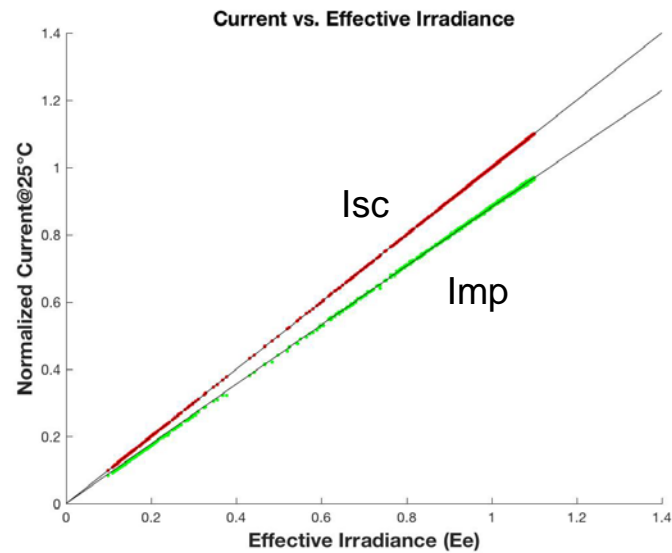
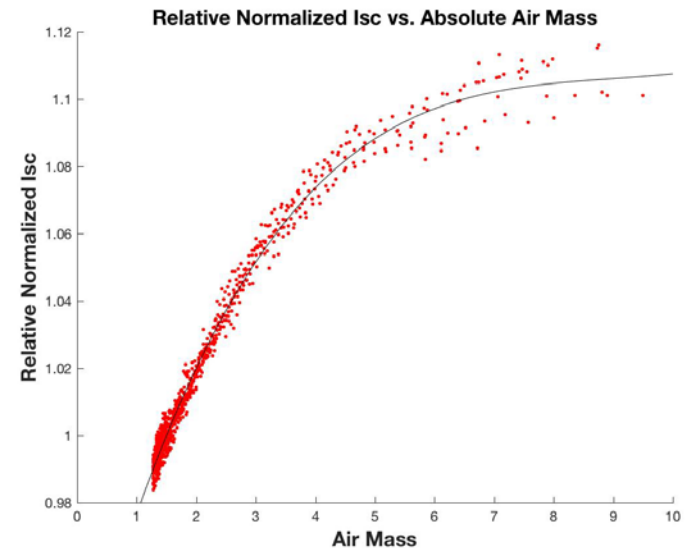
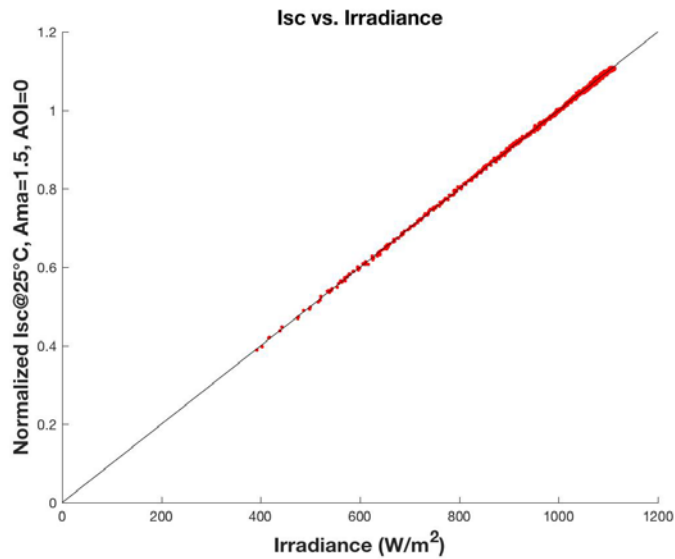
- Simultaneously solve each SAPM constitutive equation for fundamental parameters, e.g. STC electrical parameters, airmass function, temperature coefficients, etc.
- Does not use temperature coefficients from a discrete test
- Uses all IV data collected over a test interval
- Eliminates “piece-wise” model coefficient generation that has been the standard



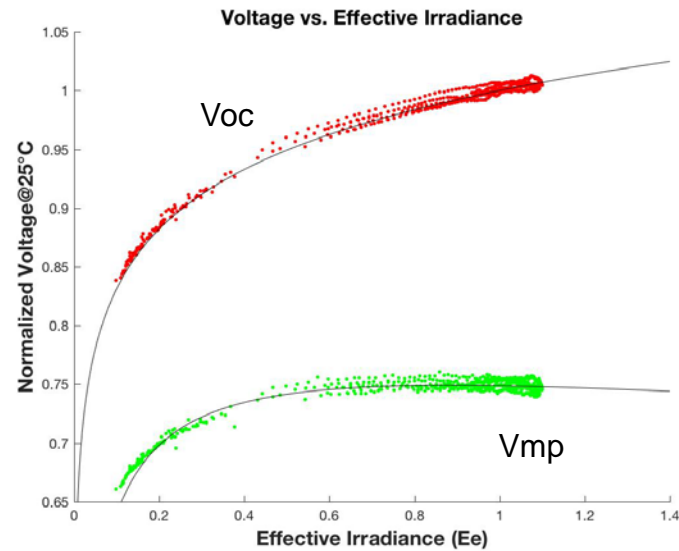
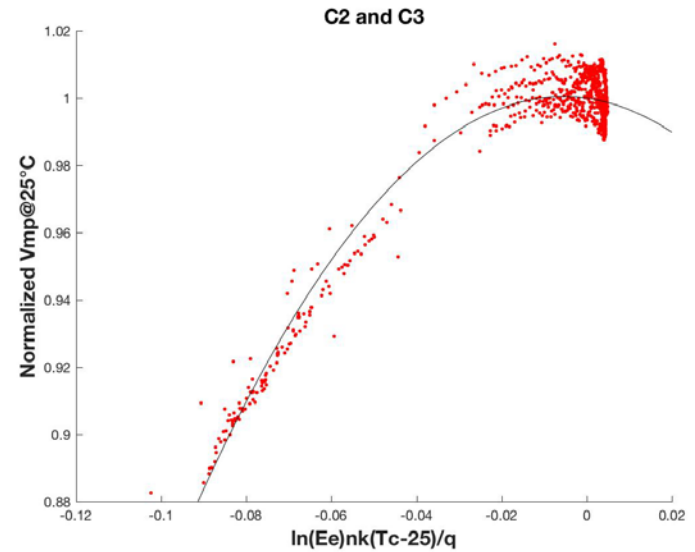
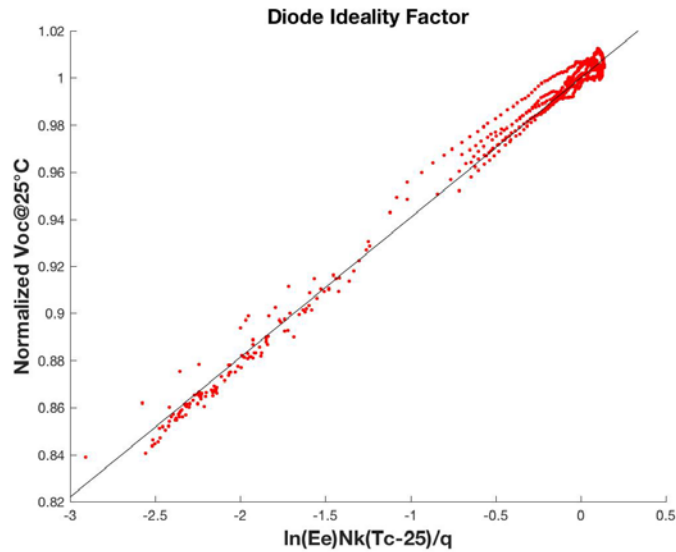
# Alternate Method – Simultaneous Solution



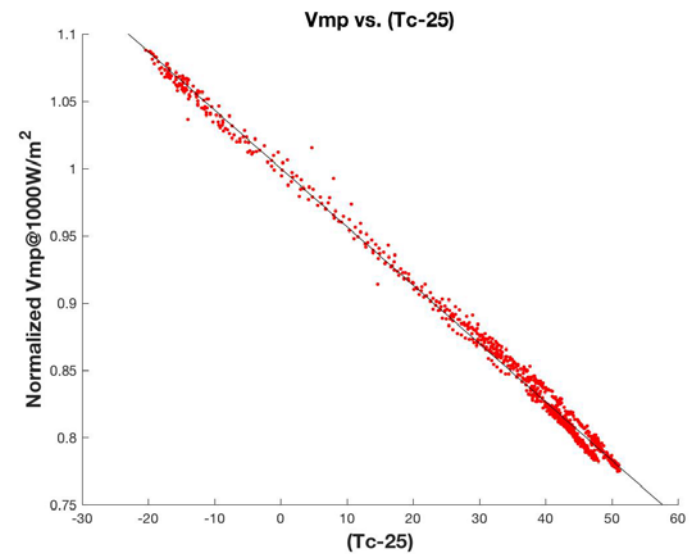
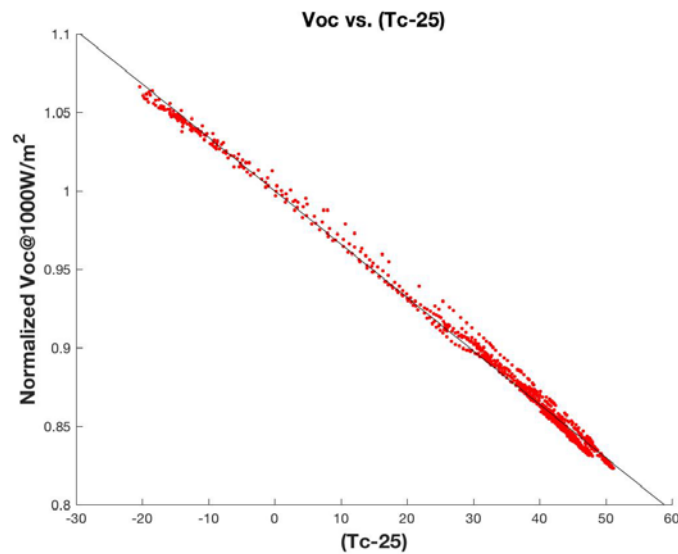
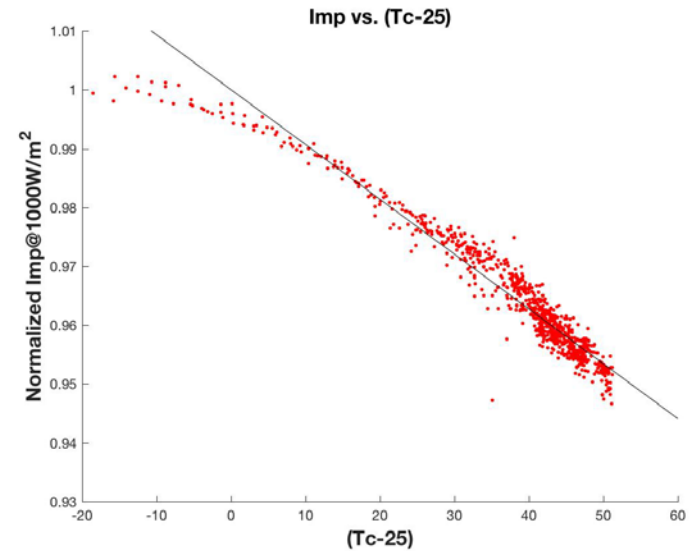
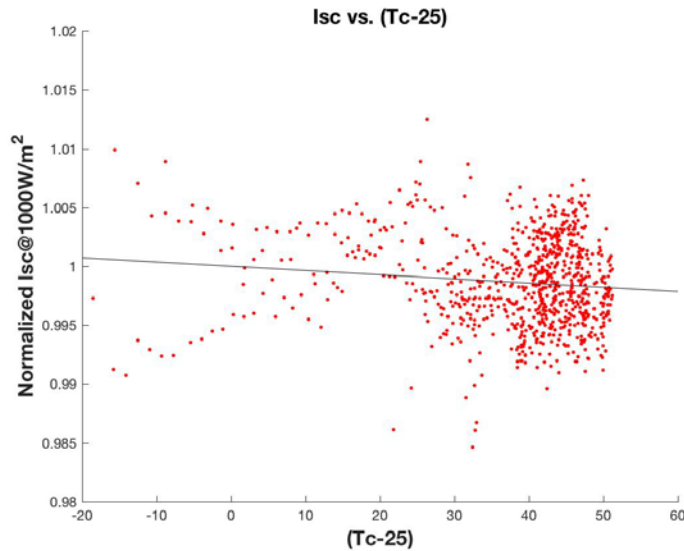
# Output – Currents



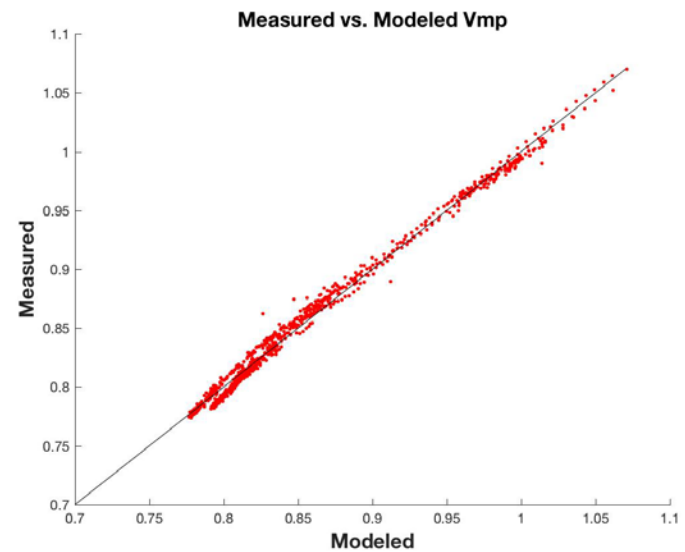
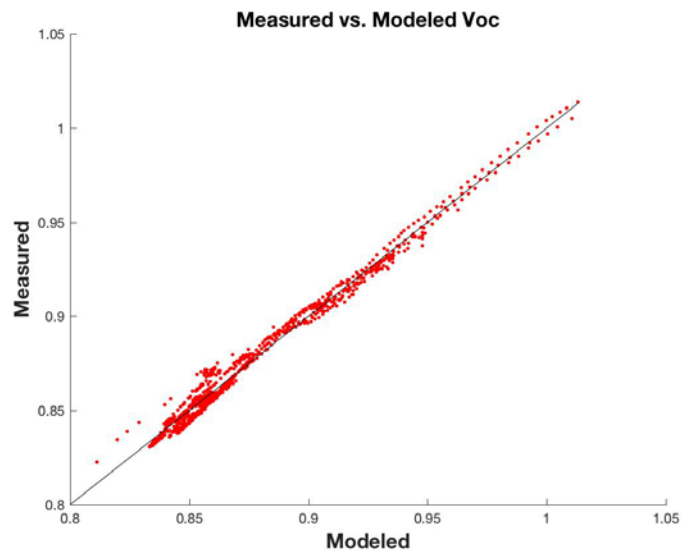
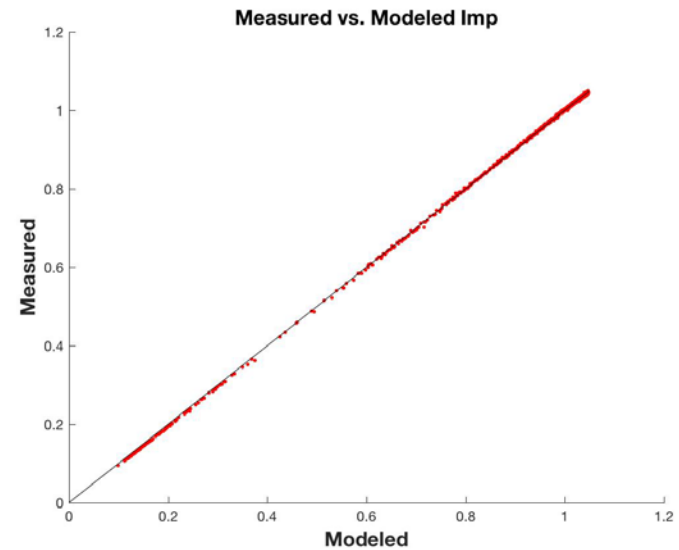
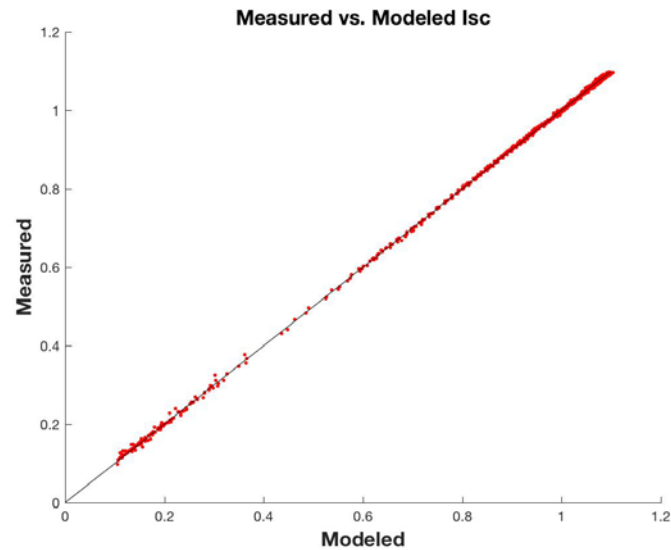
# Output - Voltages



# Temperature Coefficients



# Measured vs Modeled

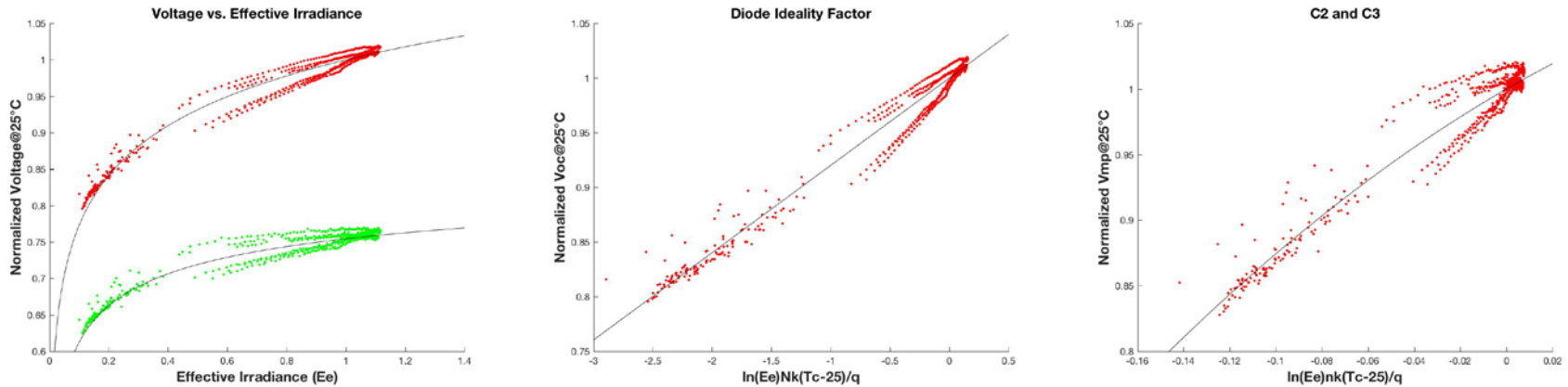


# Select Parameters (Normalized)

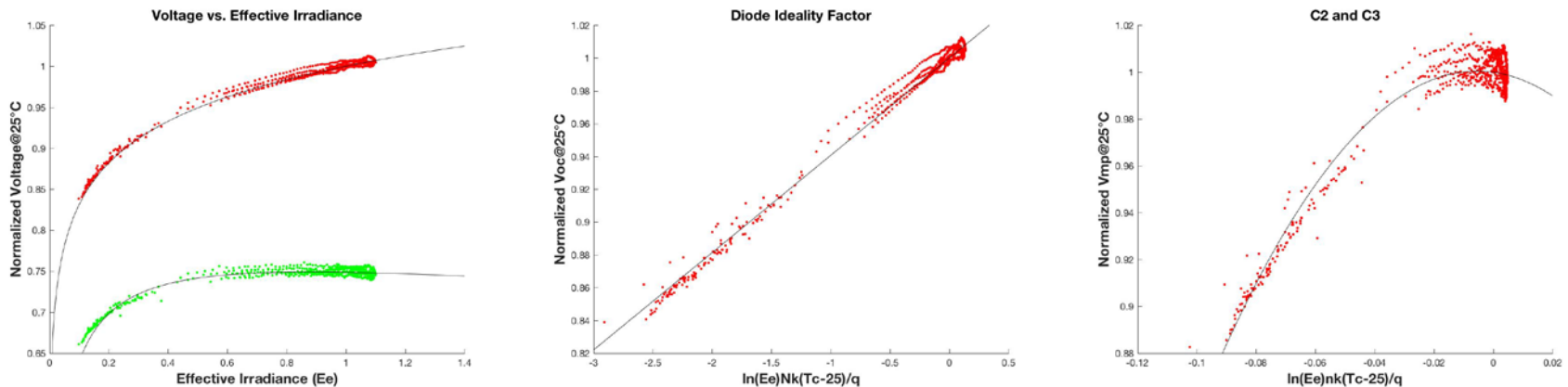
	Alternate Method	Standard Method	Lab Estimates
Pmpo	1.02	1.05	1
Isc	1.02	1.01	1
Voc	1.01	1.05	1
Alpha-Isc (%/°C)	-0.0036	-0.0036	-0.0034
Alpha-Imp (%/°C)	-0.100	-0.107	-0.066
Beta-Voc (V/°C)	-0.097	-0.123	-0.095
Beta-Vmp V/°C)	-0.093	-0.117	-0.086
Gamma-Pmp (%/°C)	-0.534	-0.636	-(0.45 - 0.50)
Diode factor	1.69	2.35	-

# Example Improvement

## Standard Method



## Alternate Method



# Summary

- CIGS Modules present challenges to measurement and modeling due to metastable behavior
- Standard outdoor methods for measuring temperature coefficients may produce values that are not representative of a CIGS module's behavior during normal, steady state operation
- An alternate analysis method was developed to determine temperature coefficients simultaneously with the solution of all other model parameters
- The alternate method resulted in a more accurate model for the test case
- Validation against historical data sets indicates the method is applicable to other technologies and possibly produces a more accurate model in general
- This method may eliminate the need to perform separate thermal tests