

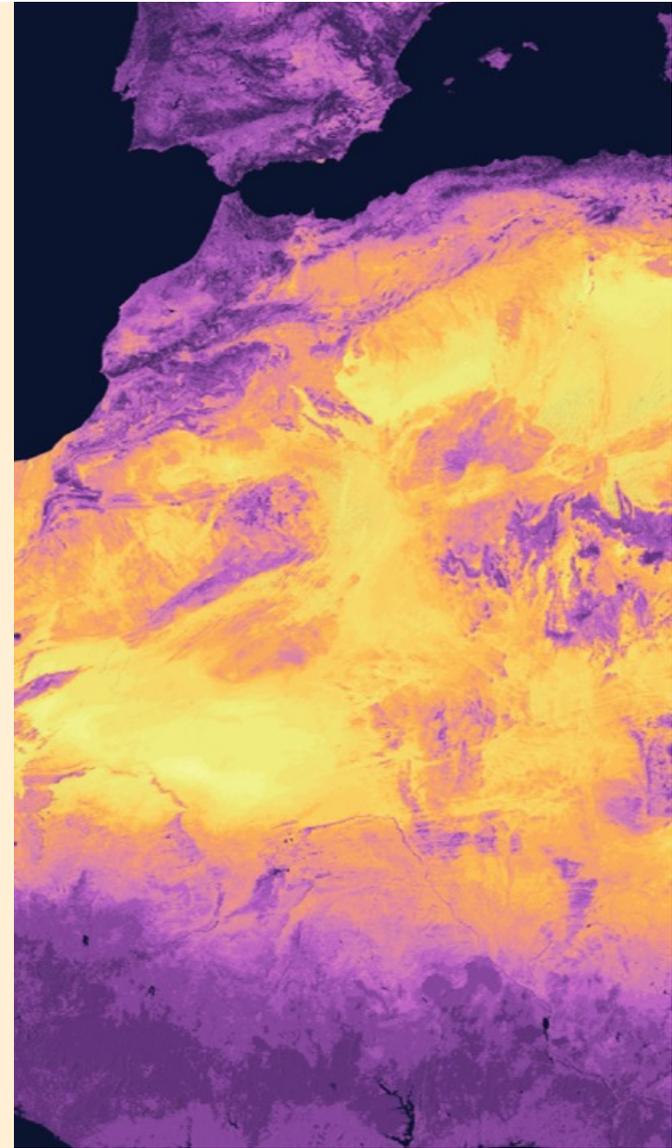
SOLARGIS

A new thermal model for ground and offshore PV installations

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Agenda

- Impact of temperature on PV modules
- Motivation for a new temperature model
- Approach to solution
- Model structure
- Preliminary results and verification
- Proposed next steps

Impact of temperature on PV modules

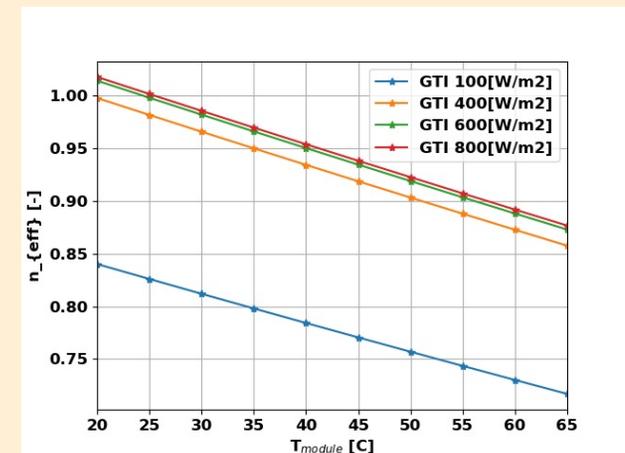
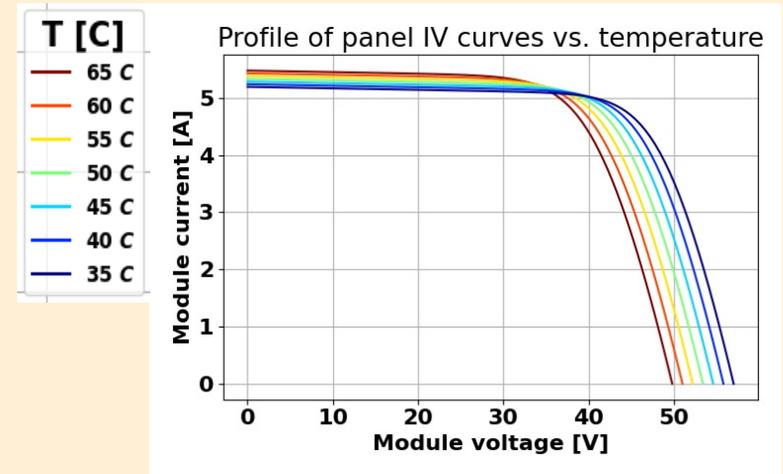
	Environmental effect
1	Global tilt irradiance G [W/m^2]
2	Temperature T [$^{\circ}\text{C}$]
3	Albedo [-]
4	Pollution, Dust

Effects on PV panel

- Open circuit voltage V_{OC} is decreased
- Output DC power and P_{MP} is decreased
- Short circuit current I_{SC} is increased

Models for temperature efficiency μ

- Huld's model – simplified King's model (King et al., 2004)
- Explicit linear models $\mu = \mu_{ref}(1 - \beta_{ref}(T - T_{ref}) + \gamma \ln(I))$



Why new temperature model

SAPM, PVsyst, Faiman and SAM-NOCT

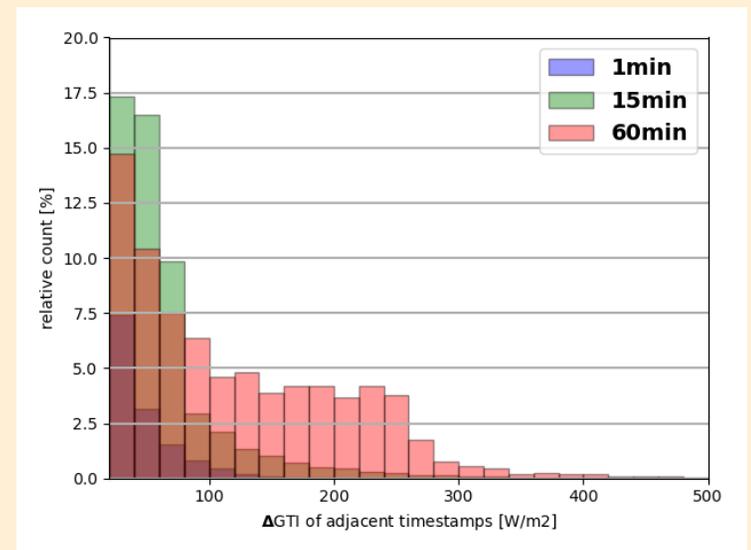
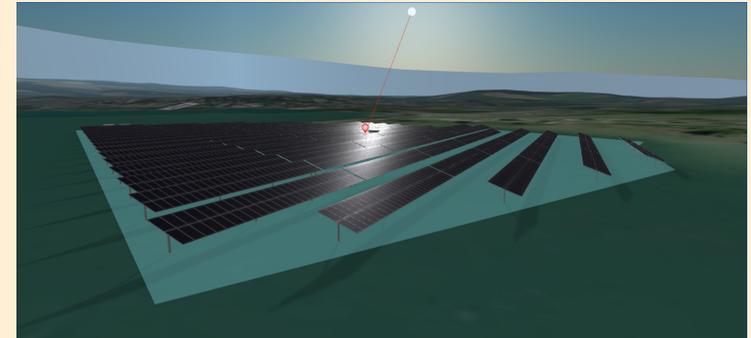
- Based on stationary heat balance equation

$$q_{GTI} - q_{electric} - q_{convection} - q_{conduction} - q_{radiation} = 0$$

- Solution in case of all 4 models is straightforward and explicit formula for module temperature => low calculation costs
- Models are based on a coefficients with constant values for calculated system (even in case of trackers)
- Basic inputs come from fit of ground measured data
- Does not reflect heat capacity of PV modules

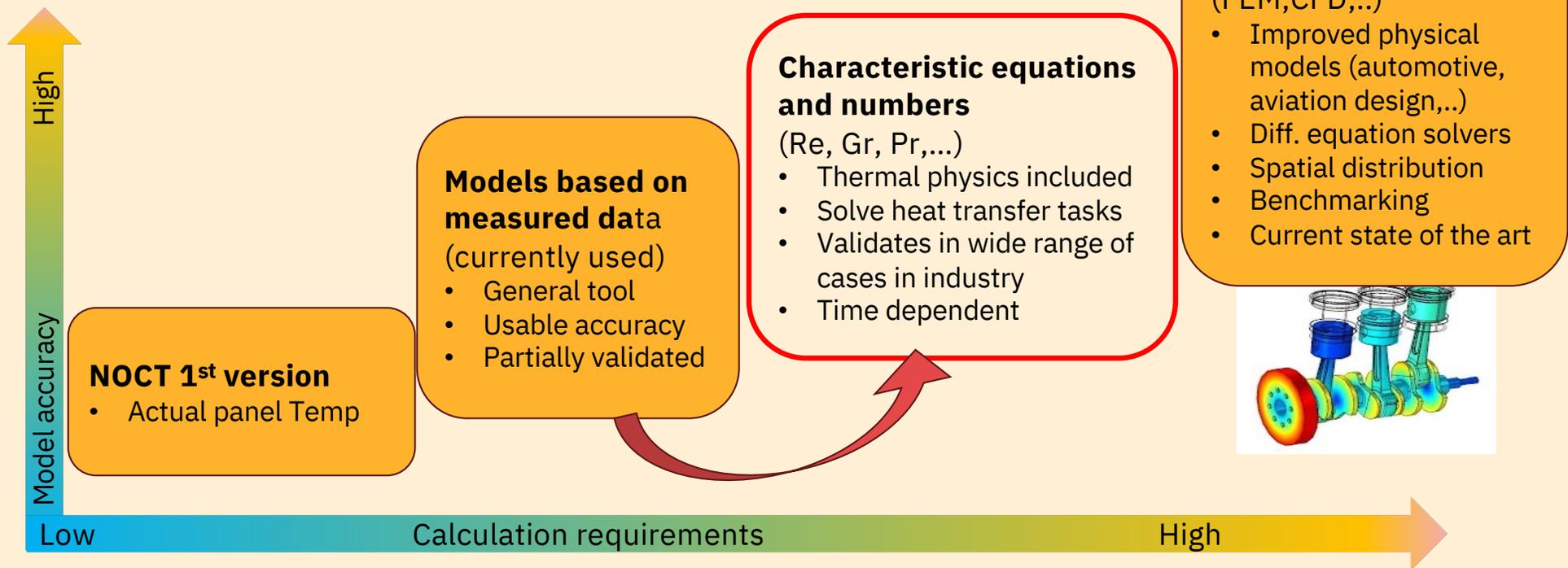
Transient weight moving average model (Prilliman et al., 2020)

- Previous module temperature is considered via moving average



New temperature model approach

- Work package in SERENDI-PV project – Floating simulation improvements
- Heat transfer is a more general issue than PV industry covers
- Approach motivated by (Choi et al., 2021)



Basic model structure

- As simple as the solution of heat balance equation (time dependent)
- Explicit or straightforward calculation except the h value.

h – convective heat transfer coefficient

- Involves differences between laminar and turbulent flow
- Depends on material properties of air
- Semi empirical method for h .

- Panel tilt
- Panel temperature
- Panel dimensions

- Air viscosity
- Air density
- Air thermal conductivity
- Air temperature
- Wind speed

$$C \frac{dT_{module}}{dt} = P_{in} - P_{electr} - P_{convect} - P_{rad}$$

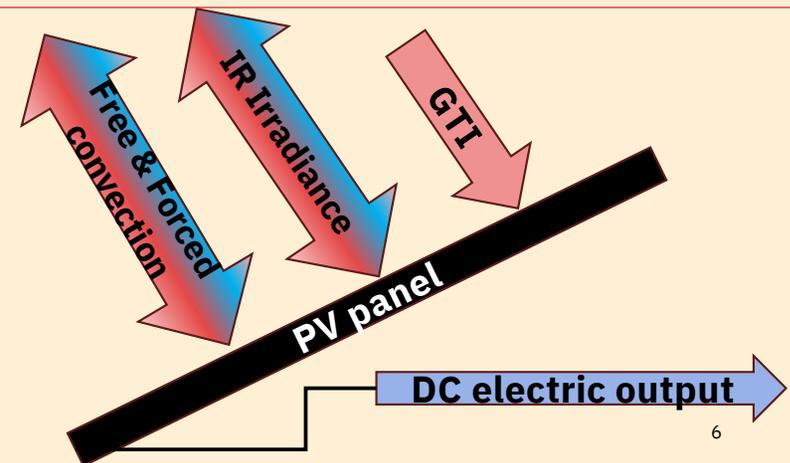
$P_{in} = A * G * \mu$ [W] – Power to module surface

$P_{electr} = U * I$ [W] – Outflow DC power

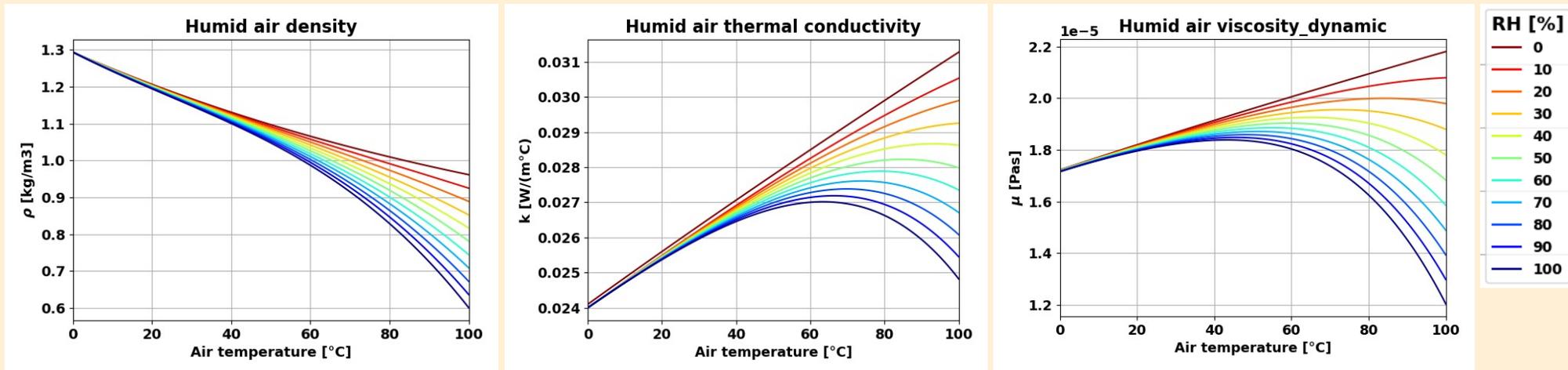
$P_{convect} = A * h * (T_{mod} - T_{air})$ [W] – (Frank P. Incropera, 2007)

$P_{rad} = F * A * \varepsilon * \sigma * (T_{mod}^4 - T_{sky}^4)$ [W] – (Driesse et al., 2022)

A [m²] – Panel surface => **separate for top and bottom site**



Material properties of humid air



(Tsilingiris, 2018)

- Floating panel does not “see” the water below mounting, but interacts with ambient air via air properties (specific heat, density, viscosity, temperature conductivity)
- Rate of convective heat transfer strongly depends on fluid properties
- Remarkable change in humid air properties starts at $T \sim 40$ °C
- Ambiguous shape of curves for elevated humidity
- Relative humidity close to water level: **RH > 80%**

h calculation

ISO 80000-11:2019(E)		
Characteristic number	Simple description	Formula
Reynolds number (Re)	$\frac{\text{inertial force}}{\text{viscous force}}$	$Re = \frac{\rho \cdot v \cdot L}{\mu}$
Prandtl number (Pr)	$\frac{\text{momentum diffusivity}}{\text{thermal diffusivity}}$	$Pr = \frac{c_p \mu}{k}$
Grashof number (Gr) (vertical surface)	$\frac{\text{bouyancy force}}{\text{viscous force}}$	$Gr = \frac{g \cdot \beta \cdot \rho^2 (T_{panel} - T_{air}) L^3}{\mu^2}$

(Frank P. Incropera, 2007;
Hideaki Imura, 1972)

Semiempirical, non intuitive, complex,
but still in use

$$h_{forced} = f(Pr, Re)$$

$$h_{free} = f(Pr, Gr)$$

$$h = \sqrt[3]{h_{free}^3 + h_{forced}^3}$$

$f(Pr, Re)$ differs for:

- laminar/turbulent flow

$f(Pr, Gr)$ differs for:

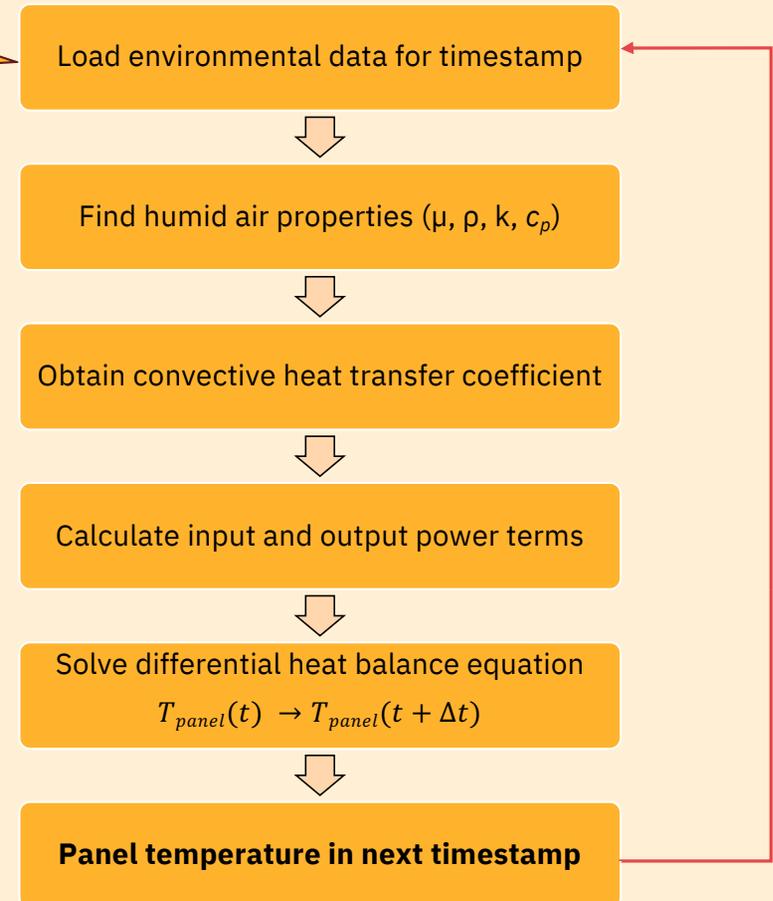
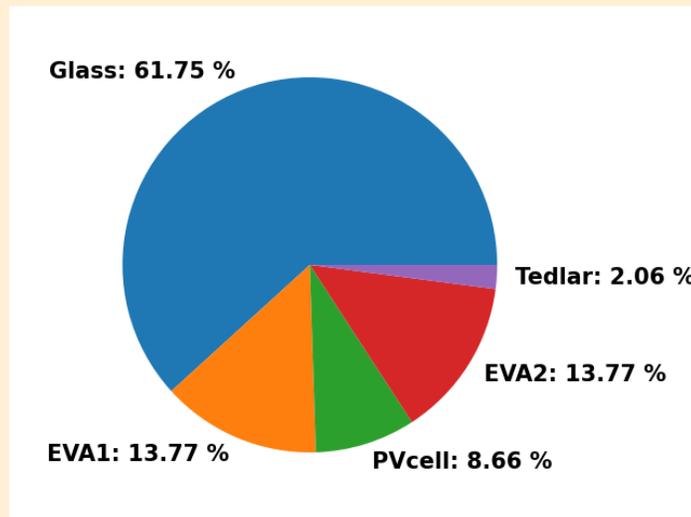
- laminar/turbulent air flow
- surface orientation top/bottom
- panel hotter/cooler than ambient air

Model flow

- Model setting
- length, width
- Emissivity for top and bottom face
- Specific heat per area (IEC 61215-1:2021)

(Syafiqah et al., 2017)

- Temperature
- Wind speed
- Global tilt irradiance
- **Relative humidity**



Model comparison with site-measured data

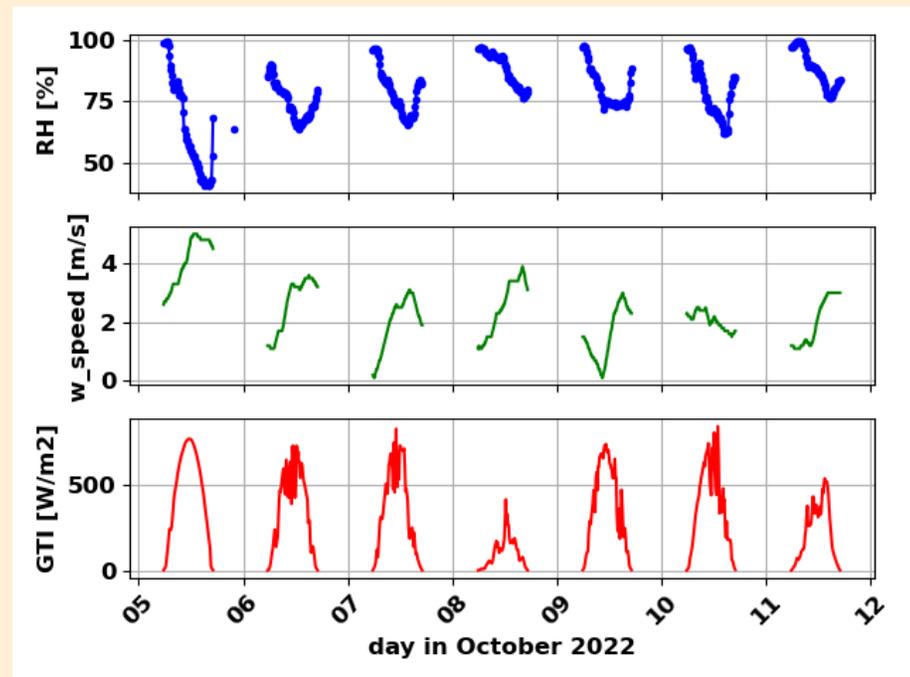
- Validation and tuning on ground measured data (Not allowed to present)
- First verification on floating PV measurements
 - Site (Western Europe)
 - Fixed tilt
 - Water dam
 - 5-min time resolution (only several days available)

Inputs

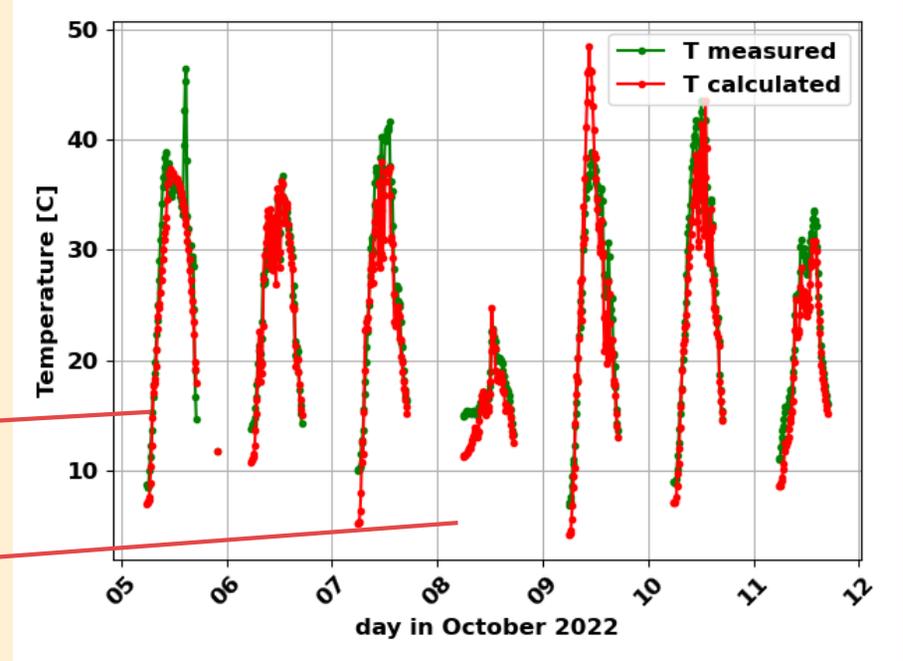
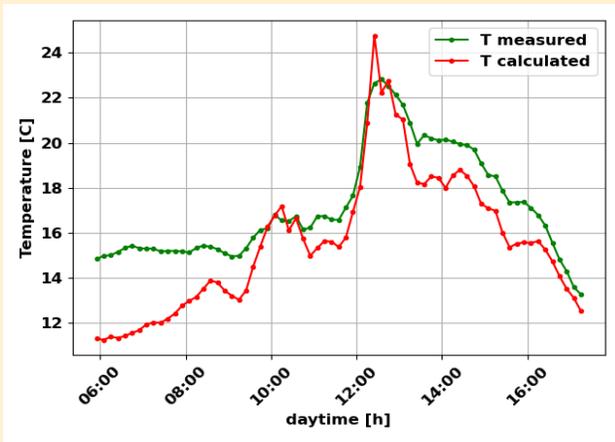
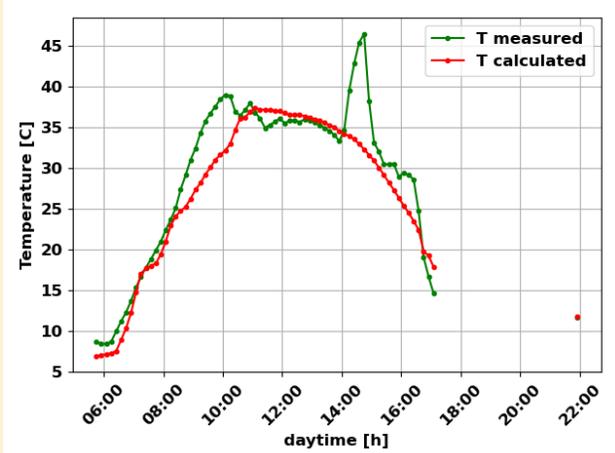
- Temperature
- **Wind speed (ERA-5)** (Hersbach et al., 2020)
- Global tilt irradiance
- Relative humidity

Model

Selected environmental conditions



Model validation with site-measured data

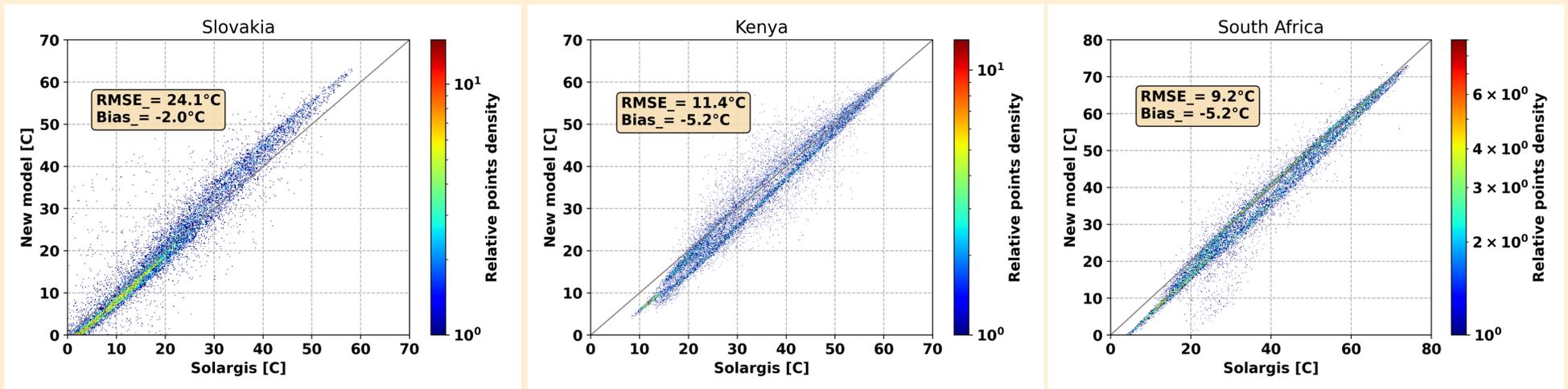


Comparison with Solargis temperature model

Country	Lat., Lon. [°]	Panel tilt [°]	Climate
Slovakia	49.258, 19.968	39	Continental, No dry season, Warm summer
Kenya	0.000, 37.210	4	Temperate, Dry and Warm summer
South Africa	-33.095, 19.038	29	Temperate, Dry and Warm summer

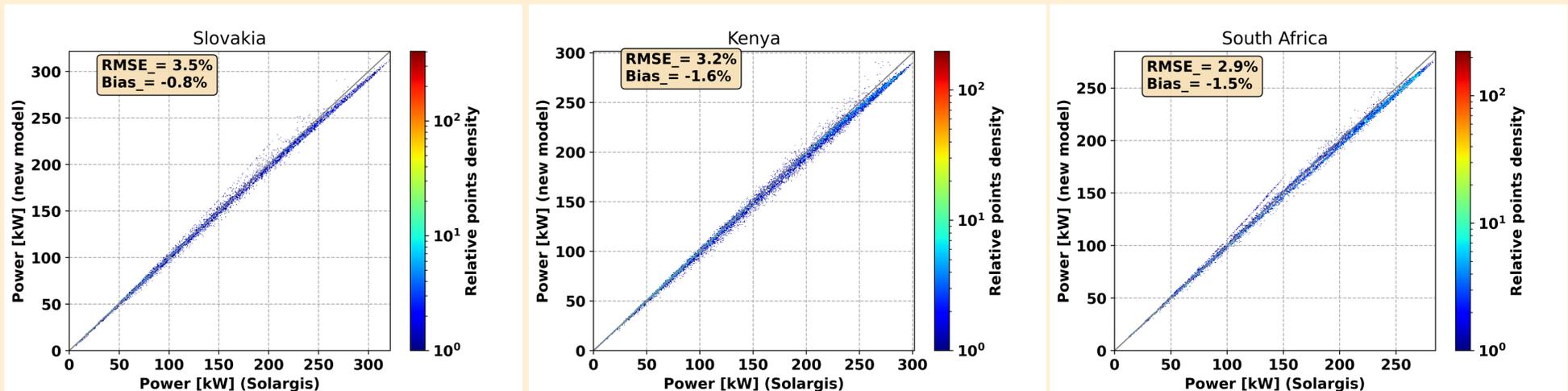
- Solargis time series 15-min resolution, year 2022
- Monofacial, ground mounted, fixed-tilt installation, OPTA calculated using Solargis tools
- Installed power = 300 kW
- Relative row spacing 2.5 m
- Modified NOCT temperature model is used as standard in Solargis calculation

Comparison with Solargis temperature model



Country	RMSE [°C]	Bias [°C]
Slovakia	24.1	-2.0
Kenya	11.4	-5.2
South Africa	9.2	-5.2

Comparison with Solargis PV simulation



Country	RMSE [%]	Bias [%]
Slovakia	3.5	-0.8
Kenya	3.2	-1.6
South Africa	3.5	-0.8

Conclusions and further work

- New approach to the modeling of panel temperature was introduced
- The first but not the last step has been done
- Preliminary results with promising model accuracy

- Suggested solutions for open issues (radiation, model speed up,...)
- Besides site measurements, the FEM, FVM software is going to be involved as verification tool